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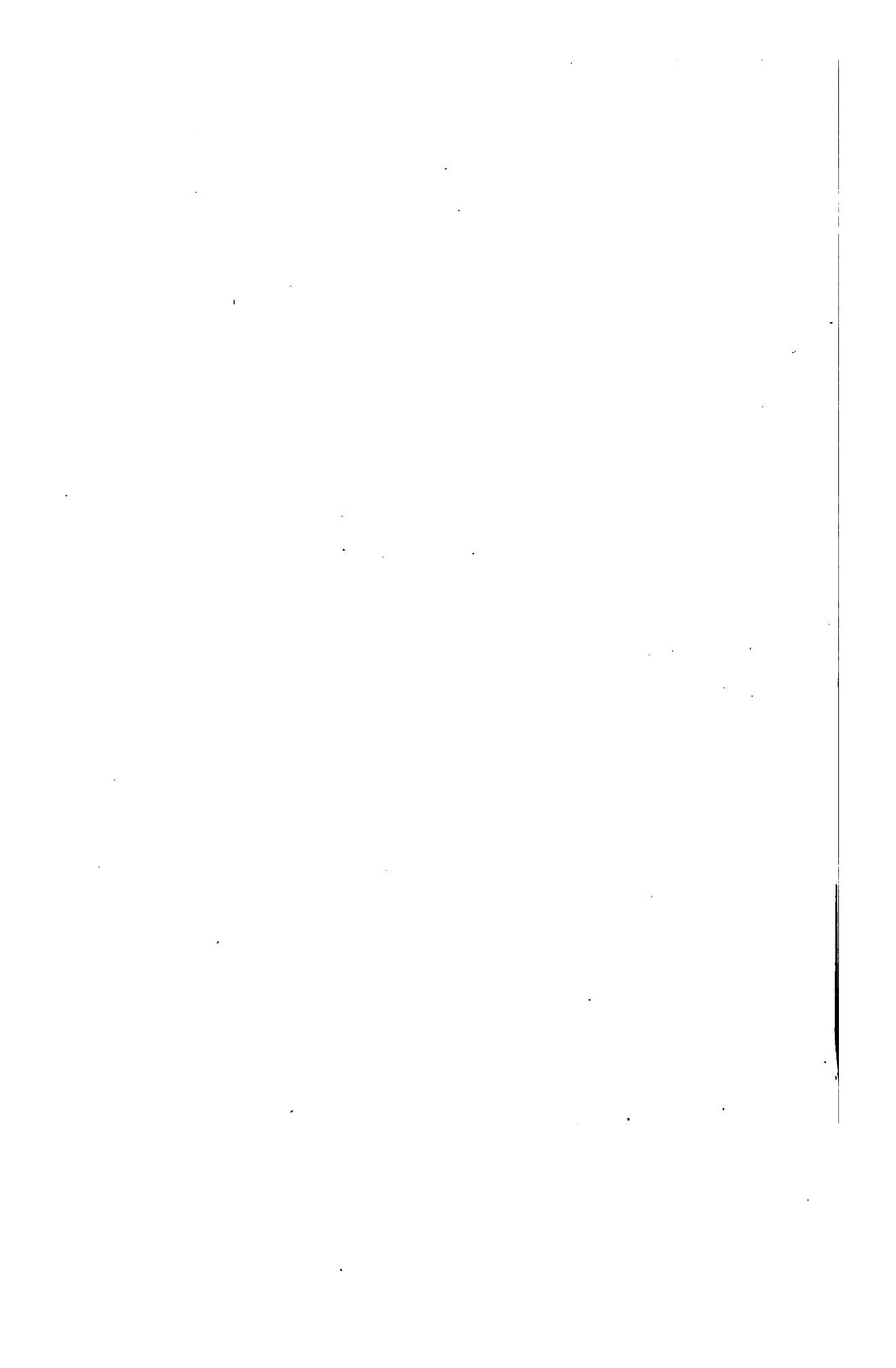
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## **HAULAGE AND WINDING APPLIANCES**



# HAULAGE AND WINDING APPLIANCES USED IN MINES

BY

CARL VOLK

INSTRUCTOR AT THE COLOGNE MUNICIPAL SCHOOL OF MACHINE CONSTRUCTION

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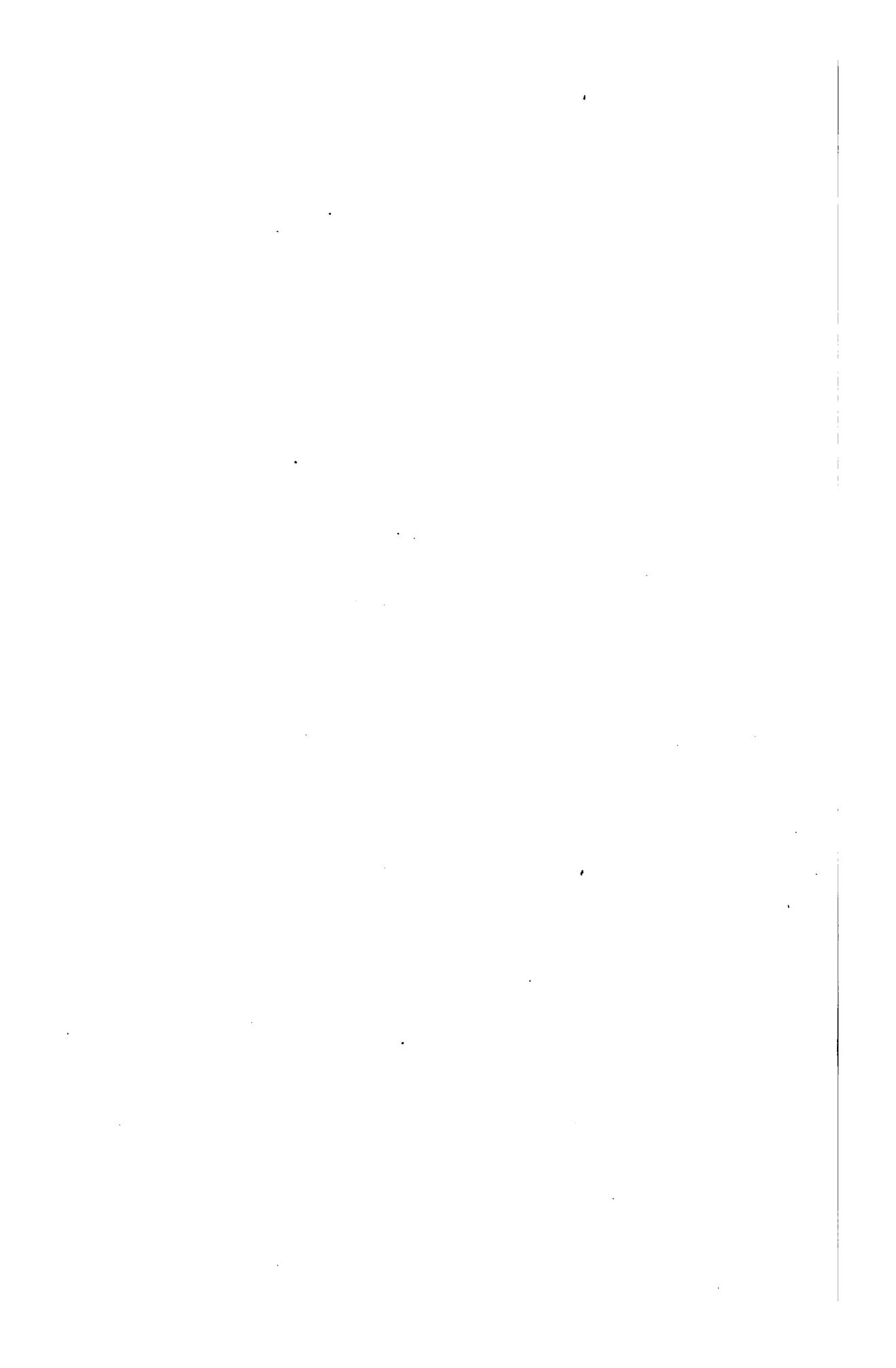
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## P R E F A C E.

DURING the period when the Author filled a position on the teaching staff at the Imperial and Royal Mining Academy, Leoben, he for several years enjoyed the advantage of serving under Julius von Hauer, whose great skill as a teacher was shown by the excellent manner in which he succeeded in making his listeners well acquainted with the extensive field of mining machinery by his succinct method of instruction.

At the time the Author was imbued with the idea of treating in a brief manner the subjects dealt with in Von Hauer's large work on winding engines; and the present work is the outcome of that idea, though its purpose is of a more modest character than that of the master.

The present work is intended for students in mining schools, young technicists desiring to extend their knowledge in this special direction, for the mine manager wishing to gain a comprehensive view of the complex subject, and so on. In all cases, however, a certain general knowledge of machinery is pre-supposed; extensive descriptions are avoided, and the drawings

merely briefly explained. The constructive side of the question has naturally had to be omitted altogether, though the special requirements entailed by the conditions of pits and shafts are always brought into prominence.

CARL VOLK.

COLOGNE, GERMANY,  
1901.

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## CHAPTER I.

### ROPES.

THREE classes of ropes are used in mine haulage, namely, wire, hemp, and aloe-fibre rope.

#### I. WIRE ROPE,

or cable, is used for raising loads, for transmitting movement in underground haulage, as the carrier in rope tramways, as guiding rope for pit cages, etc. Some wire ropes are of circular section, others rectangular (flat ropes).

(a) **Round Ropes.**—In the manufacture of winding ropes a suitable number of wires are laid together to form a ply, and several of these are then plaited together to make a rope. For specially flexible cables and lift ropes the plies are first united into strands and these again into the rope. The number of wires used is 36-180, or, for ropes to be used in conjunction with very small pulleys, 120-294. A core of hempen cord, or annealed iron of circular or oval section, is often placed in the centre of the plies and of the rope; and such ropes are far more flexible than usual, though on the other hand they are much more bulky, and are easily crushed when several layers of the rope are wound one on the other. In cross-laid ropes the twist of the plies forming the rope is in the opposite direction to that of the wires in the plies themselves; hence, if the plies show a left-handed spiral twist, the spiral position they assume in the rope is right handed. This arrangement renders the rope more flexible, and diminishes its tendency to axial rotation under the influence of a load. On the other hand, the wires form numerous ridges on the periphery of the rope, and are there sub-

jected to strong flexion, so that for certain purposes, where the rope is exposed to mechanical wear by surface friction and abrasion (underground haulage, wire tramways, etc.), it is preferable to have the twist of the separate wires and plies running in the same direction. A somewhat different arrangement is that shown in Fig. 1, representing the Felton & Guilleaume "patent closed" rope that has latterly come into use for haulage and wire tramway purposes. As can be seen from the drawing, this rope consists of a wire core surrounded by several concentric layers of shaped wire, wound alternately right and left handed, the section of the wires being such that no interstitial spaces are left between them. The wires in the outer layer fit into each other, and, by a special arrangement of the spinning machine, are given a greater tension than those inside, the result being that any fracture, arising in use, becomes apparent in

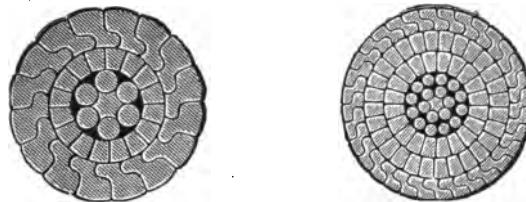


FIG. 1.

the outer layer first, and not in the inner, unseen portion. By the abolition of the hempen core and the useless interstitial spaces, this rope is lighter and much thinner than others of equal strength; consequently, a greater length of rope can be wound on the same drum, and greater depths can be attained without necessitating any alteration of the drum. On the other hand, these ropes are more susceptible to injury from kinking in the tail rope, defective coiling and winding; and as the closed construction prevents the protrusion of broken ends at the surface, incipient damage is more difficult of detection, and the rope therefore requires far more careful inspection.

*Tapered Rope.*—In very deep shafts the weight of the rope itself lays a heavy strain on the upper portions; but as the influence of this weight decreases downwards, the rope can be reduced in sectional area in the lower portion (tapered), preferably, in the case of round ropes, by decreasing the number of wires used. These

ropes are much lighter than those of constant section, but are by no means extensively used, although they have been found to answer well in certain cases.

*Kind of Wire Used.*—Charcoal iron and Bessemer steel are seldom employed, except for tramway and guide ropes, or in cases where heavy underground haulage ropes are required. The most usual material is crucible steel, with a breaking strain of 170,000 to 250,000 lb. per sq. in., greater strength being required only in cases of very deep pits and heavy loads. The extensibility of this wire is smaller, it is more susceptible, and requires a large coiling radius.

*Calculating the Strength of Rope Required.*—The permissible amount of strain on ropes is generally fixed by administrative regulations. The usual plan of selecting rope is by taking the tensile strength quoted in the makers' catalogues and allowing a margin of safety, 6- to 8-fold in the case of goods and 10-fold when passengers (*e.g.*, miners) are in question; the weight of the rope itself must also be taken into consideration, and the winding drum should be of larger diameter than given in the makers' tables. It should be noted that, in consequence of dynamic influences, the strain on the rope is occasionally far higher than that corresponding to the weight of the load.

*Attaching Rope to Load.*—For the purpose of attaching the rope to the load, the former must be looped at the end. Where the strain is comparatively small, as in the case of horizontal haulage, a simple loop will be sufficient, the end of the rope being turned back on itself for a distance of 12-20 ins., and fastened by tightly lapping it with wire, or by means of a clamp. A suitably curved iron ring is inserted in the loop to protect the wire.

Fig. 2 shows the Felton & Guilleaume friction clamp, in which the loop is enclosed by strong iron plates at each side, and the ends held by additional clamps. The strong flexion of the rope in forming the loop always sets up unequal tension in the end parts of the rope; and, on this account, it is preferable to form the support for the load by loosening and bending the individual wires, or spreading the end out conically by driving in a dowel, the whole being then fixed in a previously superimposed conical bush,

by means of a hard lead casting. The remaining connections are attached to the bush in question (Fig. 37). This method, however, is attended with the risk of the wire getting loose in the lead, and the whole rope drawing out of the bush. (In Fig. 37 the steel sleeve is made in two parts for convenience in mounting.)

For attaching loads otherwise than at the end of the rope the Baumann clamp (Fig. 3) can be recommended. In this case a steel bush, divided into three parts and filled with a cast metallic

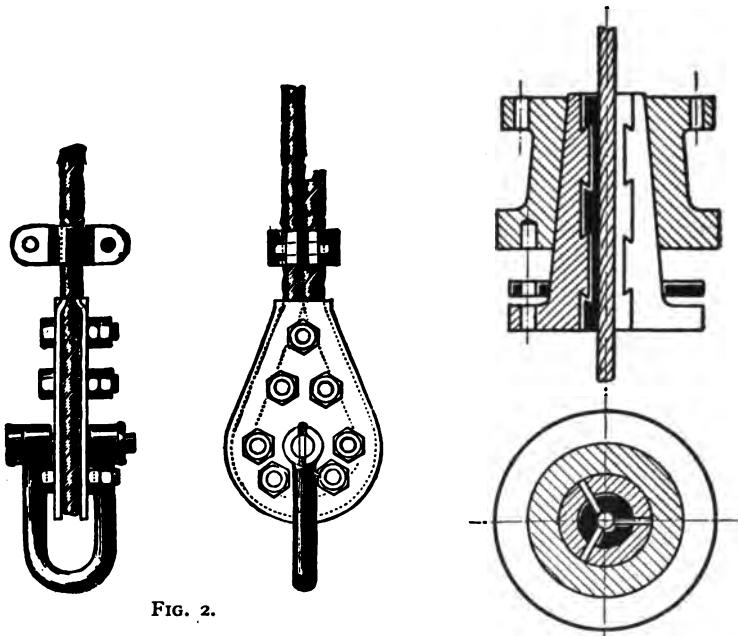


FIG. 2.

FIG. 3.

alloy, is pressed tight against the rope by an outer collar with tapered bore. The cage is supported on the collar, either direct or by means of chains, the narrow flange being utilised for mounting.

(b) **Flat Ropes.**—These consist of several (6-8 or 10) strands of round rope placed side by side and connected together by rivets of lenticular section, or, better still, by interwoven wires. The individual strands are usually four-ply, and alternately of right- and left-handed twist. Being thinner than round ropes of equal strength, they allow of a smaller radius of curvature in winding. Their advantages and

defects will be detailed when we come to speak of drums. The loop can be formed as in Fig. 4, or as in Fig. 2, the rope being laid round a pear-shaped pulley, and the end clamped to the main portion.

Since the practice of conveying the miners to and from the pit in cages has become the almost universal custom, greater attention than ever has to be bestowed on the careful testing of winding ropes, and in many parts is rendered obligatory by law. To detect broken wires the rope is allowed to pay out very slowly, and a wisp of

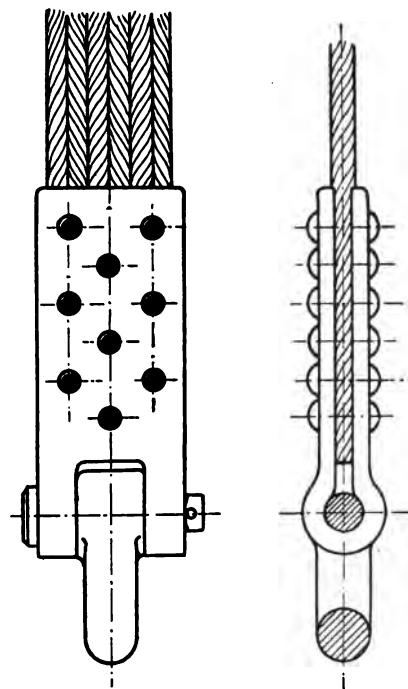


FIG. 4.

hemp is held against it; and every three or four months a length of two to three yards is cut off the tail end of the rope, and the individual wires tested for breaking strain, extensibility and flexibility.<sup>1</sup> The latter test is particularly important, since, while there is little alteration in the tensile strength, the brittleness increases and causes breakages. It is also good to grease the rope well,

<sup>1</sup> In tying the end up again, this length is drawn from the reserve coils on the drum (see p. 56). This proceeding is advantageous, as changing the part of the rope exposed to prejudicial strain on the drum at the commencement of winding.

especially when exposed to acid pit water; also the loop and that part of the rope which is between the head pulley and the drum when the cage is in its lowest position. The grease used—mixtures of tar, pitch, tallow, oil, etc.—must be free from acid, and sufficiently consistent to refrain from dripping under the influence of the (often high) temperature of the shaft.

## 2. ROPES OF ALOE FIBRE.

Flat ropes are made from the fibre of *Agave Americana* to carry loads not exceeding 1000-1140 lb. per sq. in., and to wind on drums of a diameter 20-40 times the thickness of the rope. As these drums are far smaller than can be used for wire rope, aloe ropes are preferred (especially in Belgium) for many purposes, e.g., moderate depths, compensating pulleys, etc. For depths exceeding about 1,000 ft. these ropes must be tapered.

## CHAPTER II.

### HAULAGE TUBS AND TRACKS.

#### (a) THE TRACK.

THE track consists of rails and sleepers; the former, of the Vignol type, being made of ingot steel; the sleepers (mostly transverse) of oak, or, where this is difficult to procure, of beech, larch, pine, etc., iron sleepers being more rare. Longitudinal sleepers are only used in exceptional cases, for instance, where the rope has to be carried long distances on the floor of a haulage road and below the level of the track.

**Dimensions of Rails.**—For convenience in lowering into the pit and handling there the length should not exceed 16-22 ft. The sectional area is calculated in the same manner as for girders on two supports, but with a larger margin of safety, since, apart from any accidental excess over the contemplated load, heavy rails are advantageous, as enabling the load to be increased. Stronger and firmer connections are used, the track is more durable, wears less and requires less repair. The dimensions of the rails are: height,  $2\frac{1}{2}$ - $3\frac{1}{4}$  ins.; weight, 11-25 lb. Rails over  $17\frac{1}{2}$  lb. are strong enough for light locomotives.

**Wooden Sleepers.**—These measure  $3\frac{1}{2}$  x 4 to  $4\frac{1}{2}$  x 6 ins., and are laid at distances of 24-32 ins. apart. They are usually steeped (impregnated) with zinc chloride, oil of creosote, or by the Hasselmann process. This treatment, however, does not increase their life to such an extent as in surface railways. On the other hand, it is found highly advantageous to bed the sleepers in broken stone, gravel or slag. To fasten the rails in position hooked spikes are used, three to each sleeper (two outside, and one inside, the rail). In power haulage these spikes are occasionally replaced by screw-

bolts, and bed-plates are laid under the rails at the curves, up-grades and switches. The joints are placed between the sleepers (Fig. 5). Rabbetting the sleepers below the rail foot, in order to give the rail an inward pitch, shortens the life and is better omitted.

**Iron Sleepers.**—These are still seldom used, though very little

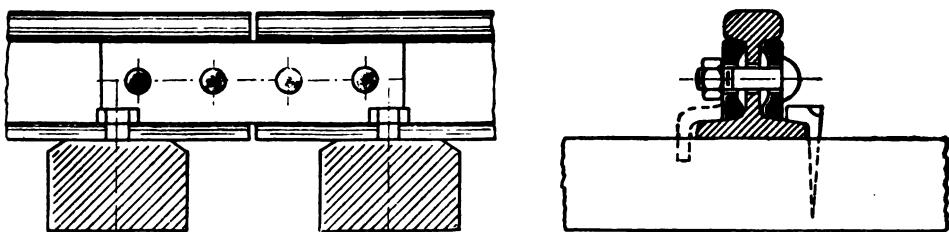


FIG. 5.

dearer than good wooden ones ; but it is only when they are of the best quality and well looked after that they are preferable to the latter. The usual profiles for iron sleepers are shown in Fig. 7, and the method of fastening the rails on them is illustrated in Fig. 6.

Rail tracks should be laid with care, templets being provided for setting the rails the proper distance apart, etc. ; the roads must

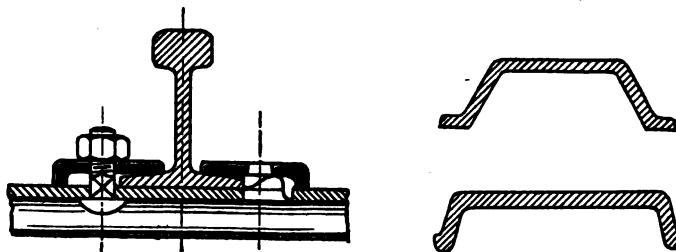


FIG. 6.

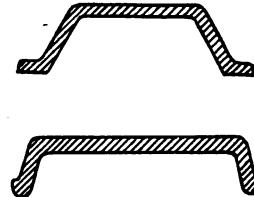


FIG. 7.

be carefully inspected and cleared, especially with a floor inclined to creep ; and water must be drained off in serviceable gutters. The width (gauge) of the track, measured inside the rail heads, is 18-32 ins., and the outside measurement on the flanges of the tub wheels must be  $\frac{1}{2}$ - $\frac{3}{4}$  of an inch less. With narrow gauge smaller radii of curvature, turn-tables, etc., may be used, but the stability of the tubs is low.

In curves the track must be widened a little by setting the inner rail  $\frac{1}{2}$ - $\frac{3}{4}$  in. farther out, and at the same time the outer rail must be raised by one-tenth to one-twentieth the width of the track; the higher the speed and the sharper the curve, the more will the outer rail need raising. In mechanical haulage, guide rails are frequently provided at the curves to prevent the tubs running off the line.

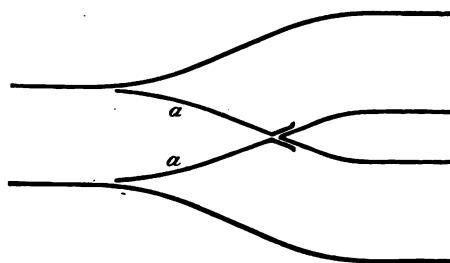


FIG. 8.

Since in running round curves the outer and inner wheels have different distances to travel, various methods have been proposed for the prevention of attrition:—

1. *Loose Wheels on a Stationary Axle* (Fig. 17).—This arrangement entails a great deal of wear in the hub journals.
2. *Loose Axle with One Loose Wheel*.—In this case the wear

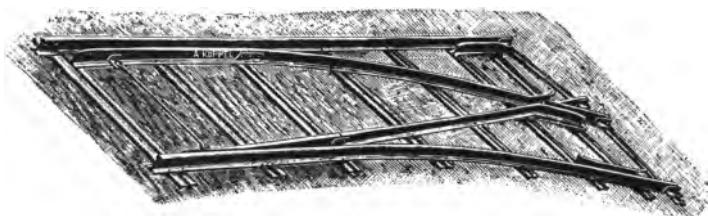


FIG. 9.

on the hub of the loose wheel is not so great, since merely the relative rotation between the hub and the axle, running in the same direction, comes into play.

3. *Conical Wheel Rims* (taper  $\frac{1}{16}$ - $\frac{1}{20}$ ).—This makes the tubs press against the outer rail when passing round curves, and consequently the outer wheel travels on a more extensive periphery than the inner one.

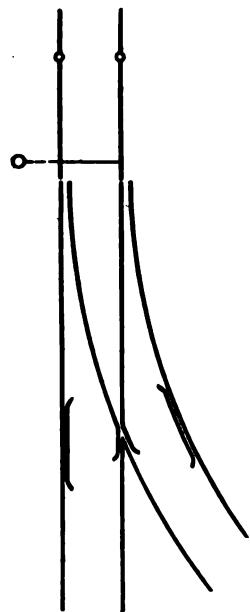


FIG. 11.

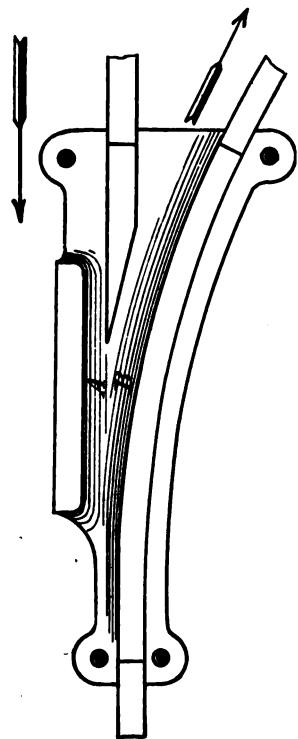


FIG. 10.

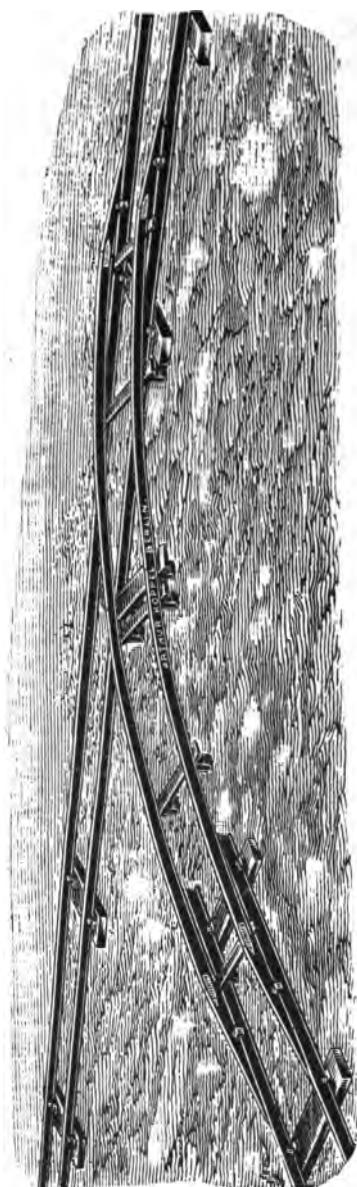


FIG. 12.

The radii of curvature should be selected as large as possible, *i.e.*, over 90-120 ft. True, in the pit, one is sometimes obliged to have curves as sharp as 30 ft. radius, and even less; but very sharp curves may often be advantageously replaced by turn-tables.

*Switches.*

1. **Fixed Switches.**—Where tubs have to be hauled singly, whether by horse or hand labour, the switch rails, *a* (Fig. 8), may be

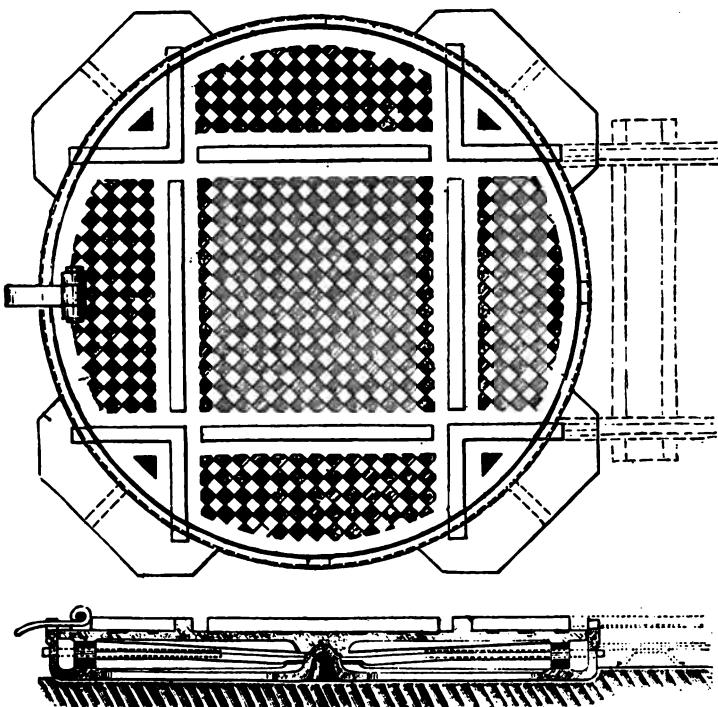


FIG. 13.

entirely omitted, plates of iron, over which the tubs run on the wheel flanges, being inserted between the outer rails.

2. **Adjustable Switches.**—(a) *Closed (Point) Switches* (Fig. 9).—The switch points are fastened together, and worked by the foot or a switch lever. Where the switching on to a branch is always in the same direction, *e.g.*, towards the right, then only one movable point is needed, in this case the left. These switches may be made automatic by fitting them with a spring or weighted

cord to press the point against the rail, and keep the one track always closed to tubs travelling in one direction, whilst those coming along that track in the opposite direction simply push open

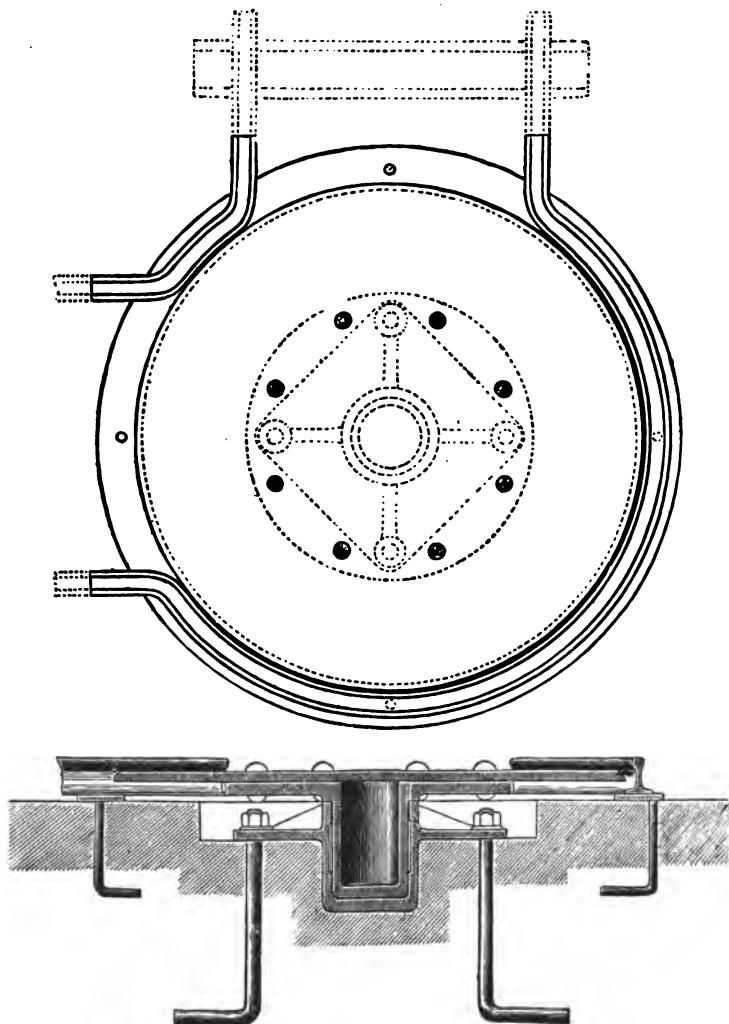


FIG. 14.

the movable point. The arrangement needs no pointsmen, but is liable to get out of order.

The same purpose is served by the plates shown in Fig. 10, the slightly shaded portions of which are bevelled, A being a little higher than B. At this point the tub is running on the wheel

flange, and, when coming from the left, is switched off towards the right.

(b) *Open Switches* (Fig. 11).—These are easier to clean, but more liable to throw tubs off the line in consequence of wrong placing. They are seldom used for single-flange wheels and light work.

(c) *Climbing Switches* (Fig. 12) are very convenient for temporary branch lines.

**Turn-plates and Turn-tables.**—Several types are shown in Figs. 13-15, but turn-tables readily become choked up with dirt and then unworkable, so are not well adapted for pit use.

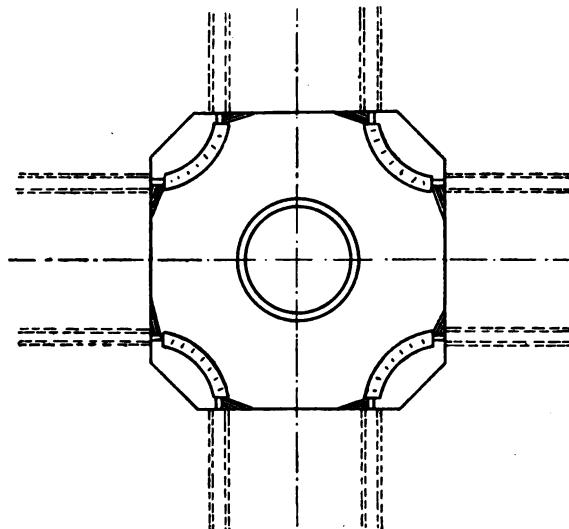


FIG. 15.

### (b) THE TRUCKS.

#### *Force of Traction for Drawing the Trucks.*

No accurate calculation of the force of traction for trucks is possible, the values for rolling and journal friction being dependent to such a great extent on the careful construction of the rolling stock, condition of the track and tubs, and the lubrication. Generally the force of traction ranges between 0·8 and 2 per cent. of the total load, the average being 1 per cent. The resistance is generally

smaller in proportion as the wheels are larger and the journals smaller. In definite instances the actual force can be measured direct by means of a dynamometer. For tracks running on a gradient  $\angle \alpha$ , the force of traction,  $Z$ , per tub is calculated for a given weight,  $A$ , from the relative gravitation and the friction corresponding to the normal pressure. Hence  $Z = Q \times \sin \alpha + Q \cos \alpha \times f$  (this latter factor,  $f$ , being 0.01-0.02). For downhill haulage on slight gradients, the force is  $Z = (Q \times \cos \alpha) f - Q \times \sin \alpha$ ; and where the angle  $\alpha$  is greater, and the tubs run down of themselves, they descend with a force that can be determined from the formula  $Q \sin \alpha - (Q \cos \alpha) f$ . Whenever possible the track should be laid so that the full tubs traverse a down grade of 5-6 in 1,000, the empties having to overcome a similar resistance in ascending. The gradients for automatic inclines range from 10 to 12 in 1,000. In curves the force of traction is increased by 20-30 per cent. above the calculated value. For horse traction the most favourable gradient is 4-8 in 1,000. When hand labour is used it is advisable (at least up to distances of 200 yds.) to let the full tubs run downhill of themselves (braked if necessary) to the haulage road, so that the only labour required is for pushing the empties back up again; the gradient varies from 10 to 15 in 1,000. The maximum gradient for uphill traction by hand or horse labour may be fixed at 50 in 1,000. Other criteria besides the strength of the putters affect the weight of the tubs; for instance, very heavy tubs entail a waste of energy and time in turning on the turn-plates and in setting them back in place when off the line; furthermore, small tubs can be passed through narrow gates and down narrow inclines without trouble. Unless local conditions necessitate deviation, about 18 cwt. may be taken as a good average tub load for ore, and 12 cwt. for coal. The general dimensions of tubs are: Height above rails, 3-4 ft.; width, 24-32 ins.; weight, 45-55 per cent. of the weight of the load.

**Details of Tubs.**—The wheels are mostly single-flange solid wheels, of steel or hard cast-iron, well annealed, the rim tapered, and measuring 2-2½ ins. across, or double the width of the rail heads, in order that both wheels may properly cover the rails in running

round curves. Double-flange wheels are sometimes used in inclines, to enable simpler, automatic switches to be employed. Wheel diameter, 12-18 ins.; larger wheels are advantageous, but increase the wheel base and the height and weight of the tubs. The wheel base should not exceed the wheel diameter by more than 1½-3½ ins., and must be reduced to a minimum in the case of tracks with sharp curves. An exception is afforded by the case of tubs drawn by an overhead rope, which are liable to run off the line often unless the wheel base is lengthened; and tubs for use in inclines are too easily tipped over when the wheel base is small.

The wheels are either mounted on loose axles or run loose on fixed axles. In the former case they are fastened in place by narrow transverse keys, only one wheel, however, being usually fixed in this way, the other running free. On that end the axle is fitted with a cap or nut and cottar, or a key is pushed in laterally in such a manner as to fit in an annular groove in the axle, and thus prevent the wheel from slipping off sideways though not from turning round.

The proper mounting and greasing of the wheels and axles is a very difficult matter, and the tubs suffer considerable damage from concussion, careless handling, dust, damp, etc. If the tubs do not have to pass over a tippler, and especially when the bearings can be placed outside the wheels, it is advisable to fit them with grease boxes, like those on railway trucks, with bottom oiling by means of felt pads.

For tubs that have to be tipped, nothing is better than the simple bearing, open underneath. When these are used, greasers are provided at intervals in the haulage road, consisting of roller brushes or elastically mounted discs that dip into an oil trough and apply a little grease to the axles of every tub that passes over them.

The most popular form at the present time is the tubular bearing, in which the entire length of the axle is surrounded by a sleeve of cast-iron or cast-steel. The portion forming the actual bearing is often filled up with composition. To diminish the waste of oil and at the same time keep dust out of the surfaces in sliding contact,

several patent devices have been introduced, notably those of Halmay (Fig. 16), with sliding cover, and Franz (Fig. 17), the latter being packed with rubber rings.

Where the rolling stock is extensive, some special means must

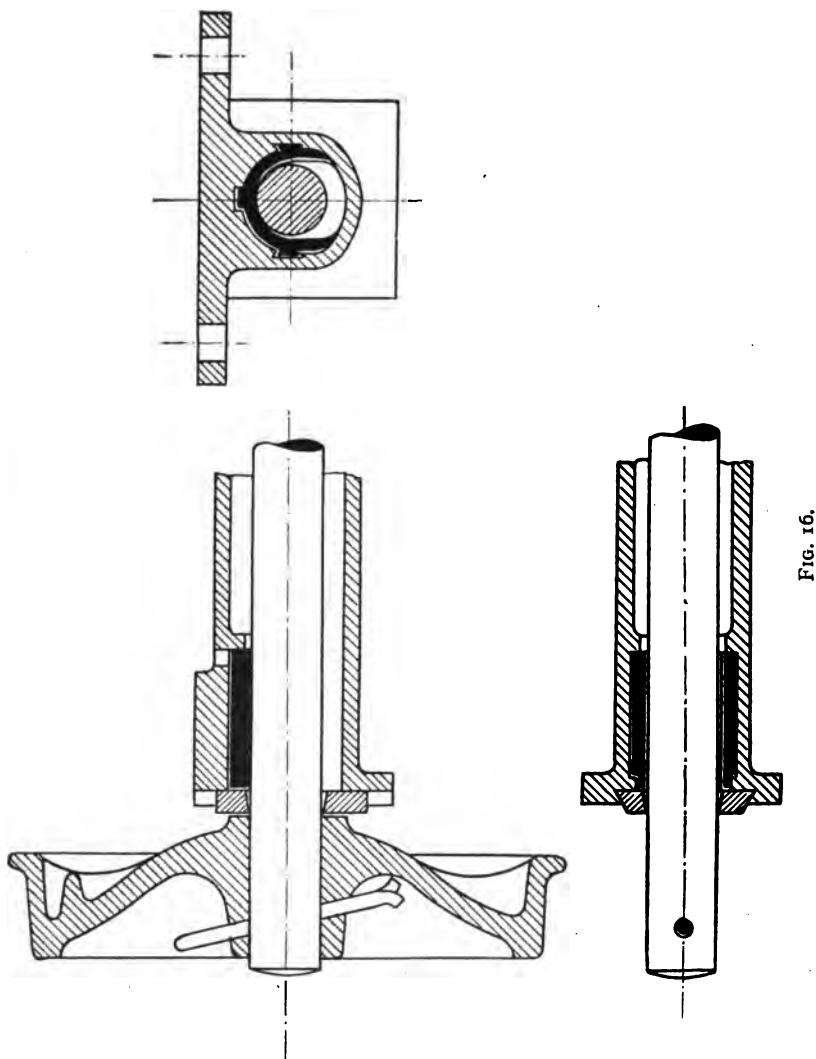


FIG. 16.

be adopted for keeping up the supply of lubricant to the tubular bearings just described. For this purpose a direct coupled steam engine (or compressed air motor) and oil pump can be recommended, the latter drawing the oil from a warmed storage vessel, and forcing

it through a pipe and suitable connections into the tubular bearing of the tub, which has been turned upside down in a tippler.

Though the weight of the tubular bearing is considerable, it at the same time greatly adds to the rigidity of the tubs, and renders any additional frame unnecessary. It has, however, in common with all bearings for solid lubricants, the defects of high friction and rapid wear. Loose wheels with oil lubricators would be preferable, were it not that existing forms are mostly unsuitable for pit work, journals that have worn loose, and therefore jolty, being a frequent cause of tubs leaving the track. At the same time it should not be

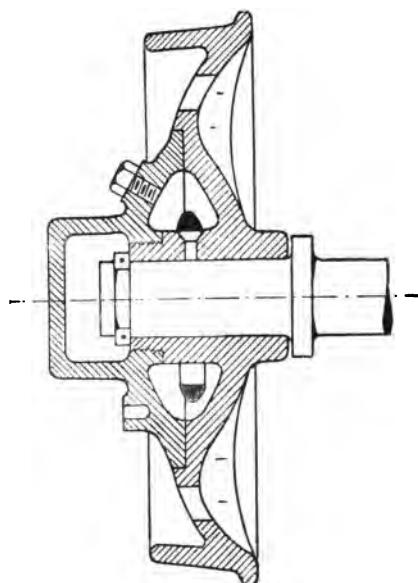


FIG. 17.

forgotten that—especially in coal mining—diminished friction and the resulting economy of motive power are not such very important items, and that a delay of several hours, on account of interruption of the haulage work, will nullify all the advantages that an improvement may possess. Fig. 17 represents the Schulz patent loose wheel.

*Body and Frame of Tub.*—The external shape should be such as to enable the sectional area of the haulage road to be properly utilised. Where wood is cheap this material is still largely used,

especially for large tubs ; it is also better able to stand shock. The sides should be 1-2 ins. thick, the bed 1½-3 ins. Angle iron fittings increase the rigidity and strengthen the corners ; or the planks may be covered with zinc. Iron tubs are often provided with two longitudinal beams of wood in the frame, and a few transverse struts, which increase the elasticity and power of withstanding shock, but reduce the carrying capacity. The long timbers may

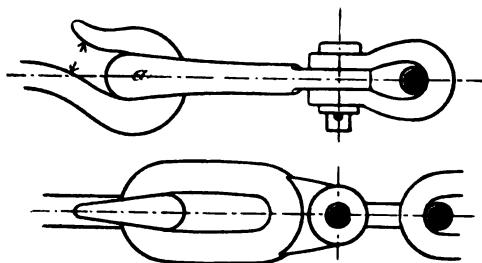


FIG. 18.

project and be faced with metal to serve as buffers. The shape of the body should be such that the horizontal projection conceals the wheels, and protects these susceptible parts against accidental falls of stone. The sheet-iron used is  $\frac{1}{6}$ - $\frac{1}{4}$  in. thick.

*Coupling Tubs.*—Hooks and links should be provided for this purpose, and arranged in a proper manner. When, in train haulage, it is not desired to transmit the whole force of traction to the tub

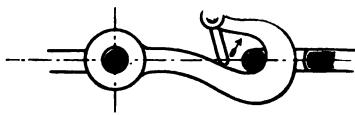


FIG. 19.

beds, a bar passing from front to back is attached to the bed or frame, the coupling hooks and links being fastened to the two ends.

Safety hooks are generally used, a small bow or ring being passed through the end of the hook ; on hooking into the link, this ring gives way, in the direction indicated by the arrow, and afterwards drops down, thus preventing the coupling coming undone. Or the end of the link,  $\alpha$ , may be thicker than the opening in the hook, so that the link must be turned through an angle of  $90^\circ$  before it can be slipped in (Figs. 18 and 19).

**Brakes.**—If the force producing a downward movement (relative gravitation minus friction) is represented by  $Z$ , then, assuming  $K$  to be the normal pressure that has to be applied to the wheel in order to check the movement,  $K = Z$ . Nevertheless, to ensure the tub being brought rapidly to a standstill, in the event of accidents, it is necessary to increase this brake power four to five fold. The pressure applicable by means of hand brakes may be set down as 45-70 lb., and that with the foot brake as 90-130 lb., the lower values referring to youths. The brake should automatically move away from the rim of the wheel when released. A few simple forms of brake for tubs are shown in Fig. 20.

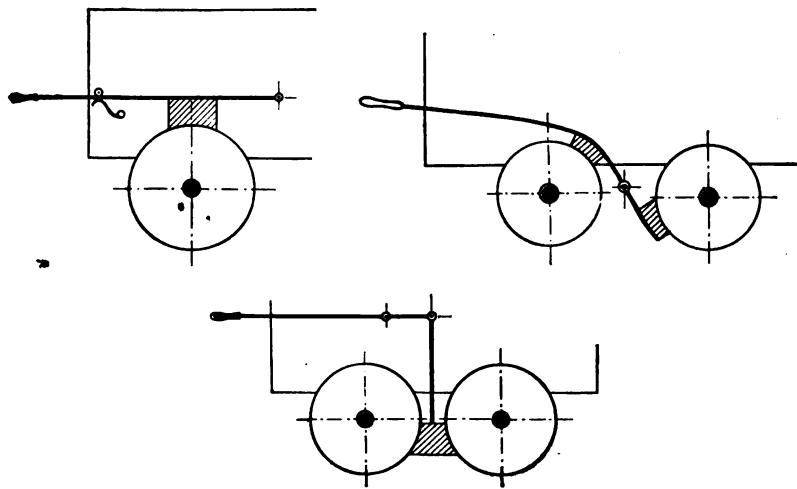


FIG. 20.

**Flat Trucks for Inclines (Fig. 21).**—Where the gradient exceeds  $20^\circ$  ordinary tubs will topple over, or else must be sent off only part full. In such event flat trucks are used to carry the full tubs, the latter being mostly pushed on from the side. When, however, the two haulage roads run in the same direction as the incline, arrangements must be made to push the tub off the truck without catching against the rope. With this object the rope, instead of being attached direct to the truck frame, fastens on to a strong iron bow, of sufficient height and width to allow the tub to pass through. If, by reason of heavy rock pressure, etc., it is necessary to reduce

the width of the incline as far as possible, the flat truck must be provided with a turn-table, so that the tub can be turned round at an angle of  $90^{\circ}$ , its greater diameter coinciding with the direction of the incline. The track gauge is 40-42 ins., and the wheels are small, to reduce the height of the truck, the defect of greater friction being of minor importance. The trucks must be strong, and more particularly well stayed and fitted with buffers, to take up the impact on the stops at the bottom of the slope. The tubs are held

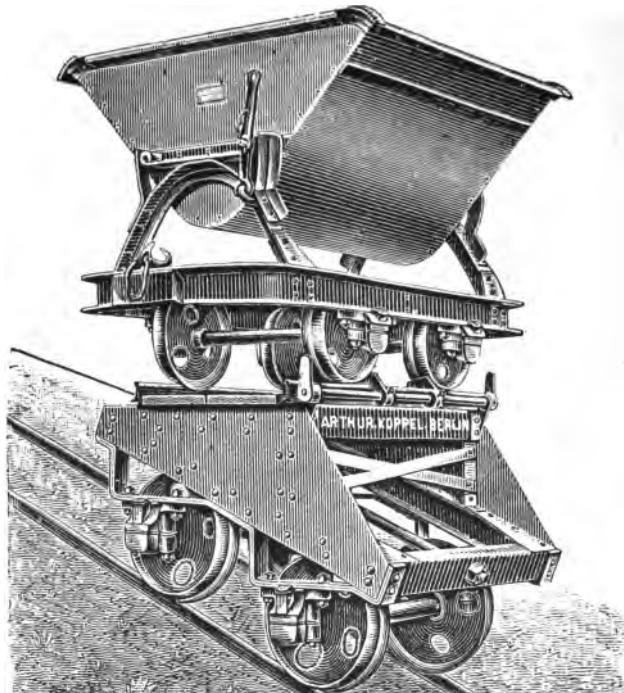


FIG. 21.

in position on these trucks in the same manner as in the cage (*q.v.*). Safety clutches are sometimes adopted, such as a hook, which, under ordinary circumstances, is held up by the haulage rope, but in the event of the latter breaking, falls down and bites in the floor. These appliances, however, are unreliable, and clutches like those used in cages would be better, but would entail the provision of expensive guides of strong timber, which in turn would hinder the provision of carrying rollers for the rope. Safety appliances placed

in the inclines themselves, and not attached to the tubs or trucks, are dealt with under "Inclines".

**Emptying Tubs.**—This may be effected:—

1. By tipping the entire tub or the body only. Fig. 22 shows a tub arranged to tip forwards, the front wall being sloped; Fig. 21 a trough or hopper-shaped tub, for tipping sideways. These are suitable for work above-ground—traffic between the preparatory works and the loading ramp, etc. The locking devices should be attached in such a manner as to preclude the possibility of the tub tipping over on the side at which the attendant stands when releasing the catch.

Fig. 23 represents the Nietsch tipping catch.

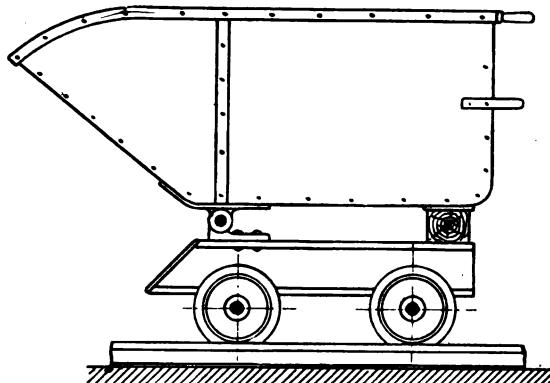


FIG. 22.

2. By providing doors in the sides or bed of the tub. These doors, however, are a frequent source of repairs, and considerably impair the rigidity of the tub body; they must be hung in such a manner that they can swing freely when opened, otherwise they are liable to be knocked about and soon spoiled.

3. By overturning the entire tub on a tippler. This method ensures rapid and convenient discharge of the contents; and when properly constructed, all injurious shock to the tubs is prevented, as well as damage to the coal. Fig. 24 represents a forward tippler (for pit heapsteads), mounted on a convenient portable and adjustable frame. Fig. 25 is a simple arrangement used in England, the axis of which is so disposed that the centre of gravity of the

empty frame is in front, and the common centre of gravity of the frame and the full tub in front of the axis of rotation ; hence the whole tips over as soon as the tub is pushed on. The common

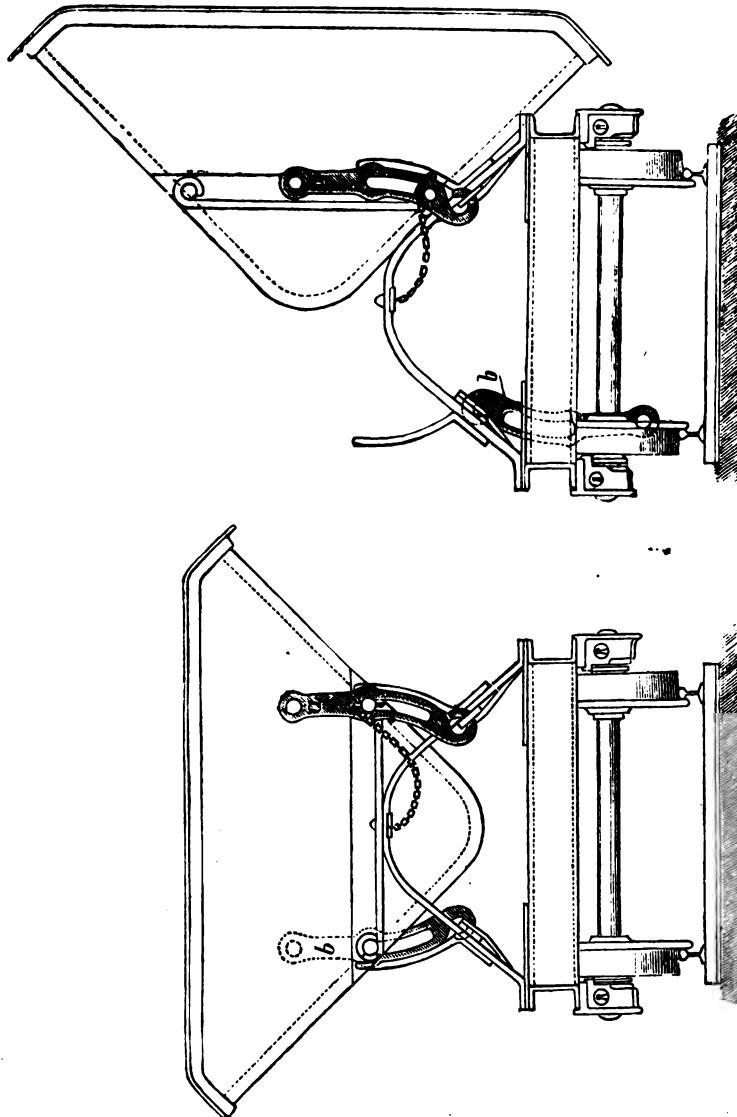


FIG. 23.

centre of gravity of the frame and empty tub being in front of the axis, the tippler returns automatically to first position. The angle of rotation is mostly  $150^\circ$ , and a stop is provided to limit the

travel. A better form is the circular or lateral tippler (Figs. 26 and 27), the depth of the shoot being smaller and the coal better protected from damage. For some loading purposes travelling tipplers

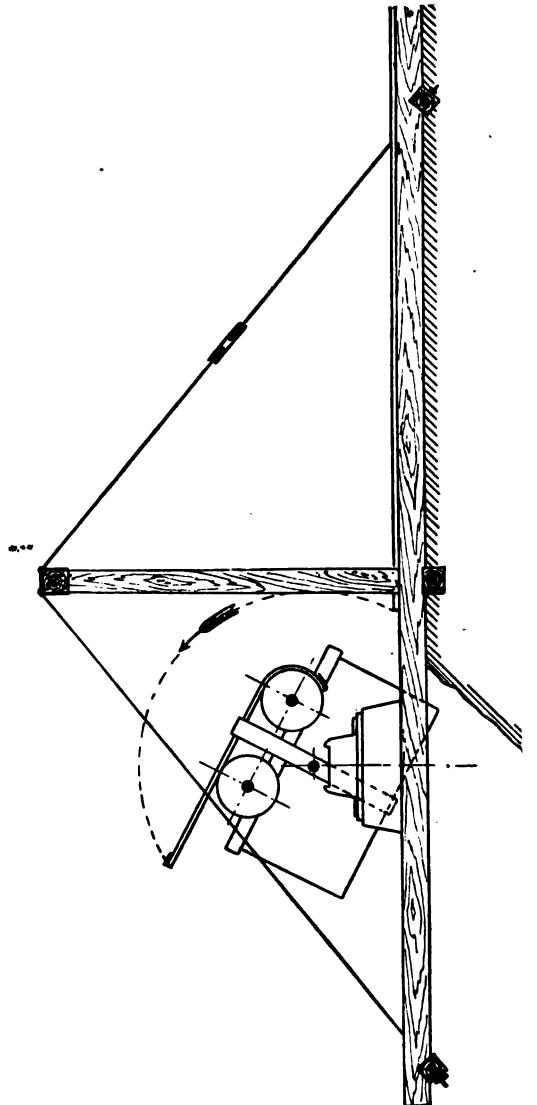


FIG. 24.

are desirable, all that is then necessary being to mount the carrier rollers on a U-iron frame running on wheels. In many instances the tipplers are worked from a driving shaft, from which motion is

transmitted to the carrier rollers by fast and loose pulleys or a friction coupling ; or the tippler is fitted with a toothed rim. The movement can be regulated so that a uniform speed is maintained

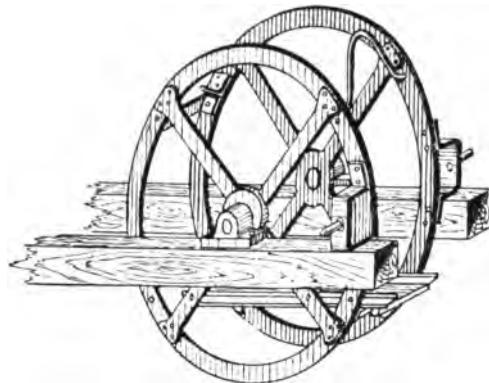


FIG. 25.

throughout, or the tub may be emptied slowly and then raised rapidly. This effect may be obtained by means of suitable driving gear, or more simply as shown in Fig. 28, where the roller, 1, works

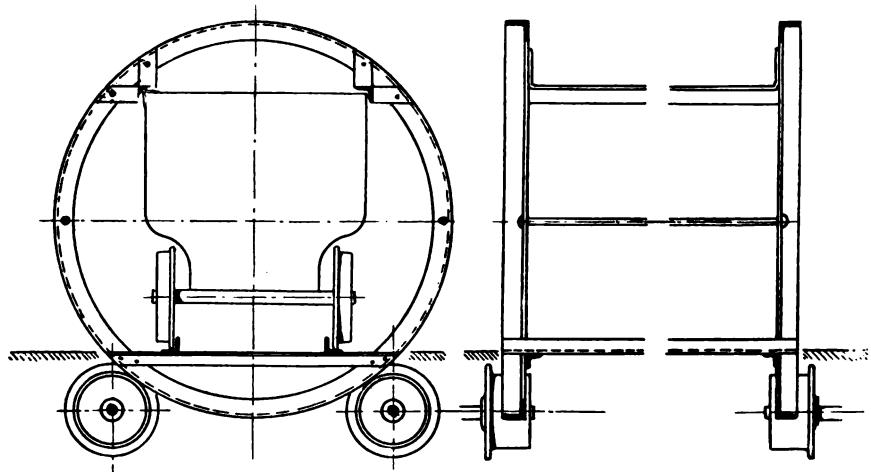


FIG. 26.

FIG. 27.

against the rim, *a*, whilst the rim, *b*, is thickened round part of its circumference by a bar, which, coming in contact with the roller 2, lifts away from 1 and leaves the tippler moving at a lower rate of speed, driven by 2. To ensure better contact the rollers and rims

are often fluted like friction gear. When the empty tub has been raised, the tippler is stopped by displacing the belt, throwing the

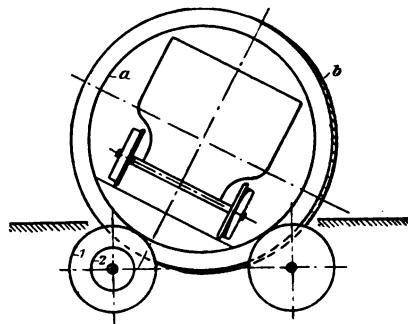


FIG. 28.

clutch out of gear automatically, or by recessing the rims at suitable places, so that the rollers cease to act on them.

## CHAPTER III.

### CAGES AND WINDING APPLIANCES.

#### CAGES.

THE cage consists of a top portion and several stages or decks, connected together by a strong framework. The rope is attached to the head, and the decks are loaded, at the pit eye, with the full tubs, which are removed when the cage has ascended to bank. The provision of several decks in one cage enables four, six or even ten tubs to be raised at one journey; moreover, these high, and comparatively narrow, multiple-deck cages adapt themselves better to the guides. On the other hand they take longer to load and unload, or necessitate the installation of special appliances—that cannot always be arranged as simply as is desirable—at the pit eyes and bank (see p. 44).

The head, decks and frame of the cage should be of bar and shaped iron, as light as possible, but well stayed. The side walls—especially of cages with several decks—are subjected to a strain, not merely of tension, but also of compression (or buckling) when lowered, and are also exposed to numerous shocks, on which account profile iron is preferable to plain bars for these parts. It is likewise better to allow the stops of the catches at the pit eye to engage below the upper framework of the cage, so that the latter is held by suspension and not supported from underneath. The flooring of the intermediate decks is often removable, and can be taken out when a compartment of greater vertical dimensions is required, *e.g.*, for conveying timbers, horses, etc. When the cage is used for conveying miners, the sides must be covered in with sheet metal or fine lattice work, and the ends fitted with doors of sufficient height and fastened from the outside. A loose sloping cover, cap-

able of turning back, must also be fitted to the cage, to keep out falling water or anything else that may accidentally fall down the shaft.

The dimensions of the cage are as follows: Height inside, 6 ft. if the men stand up, or 4 ft. at least if they sit down. Floor space per man, in the former event, 2 sq. ft., in the latter,  $3\frac{1}{2}$  sq. ft.; weight of cage, 40-90 per cent of the load to be raised.

The tubs are fixed in the cage (1) by bows, hooks or bars, resting against the tub sides, or (2) by pivoted bars inserted between the axles or in front of the wheel rims. For greater safety it is advisable to use both kinds together, or automatic locking devices which are released on the cage coming into contact with the stops at the pit eye or bank.

**Shaft Guides.**—The proper guiding of the cage is a very important point, and is secured by means of rods, extending the whole length of the shaft, and attached to horizontal beams.

The guides rest against the sides or ends of the cage, the arrangement mainly depending on the dimensions and partitioning of the shaft. End guides require a smaller amount of timber, take up less room, and on account of the greater distance between the points of contact, prevent the swaying of the cage more effectually than if arranged at the sides. At the same time they prevent the tubs falling out and damaging the shaft in the event of any breakage of the closing device of the cage. On the other hand, the main guides must be cut away, and replaced by lateral guides, at the pit eye and bank, in order to enable the tubs to be run in and out of the cage. However, this is unnecessary when each deck of the cage accommodates two tubs, side by side, since then the tubs can be run past the guides on either side. Iron rails or profile bars are for the most part arranged on one side of the cage only, a single set of superposed cross bars, between the cage compartments, then sufficing to carry the guides. When wire cables are used for guiding cages, three or four points of attachment are employed.

**Timber Guides.**—Oak or pine timber, free from knots, or American woods are used. Dimensions,  $4 \times 6$  to  $6 \times 8$  ins., the broad side being mounted on the cross beams (timber, H- or U-

irons) so as to fit accurately and run exactly vertical. Attention must be bestowed on arranging the guides and supports so that they are readily accessible and removable.

The guide timbers are fitted together as in Fig. 29, or by means of wrought-iron fish-plates, the joints resting on the cross timbers.

Contact between the cage and the guides is effected by means of cast-steel slides or wrought-iron lugs screwed on to the head

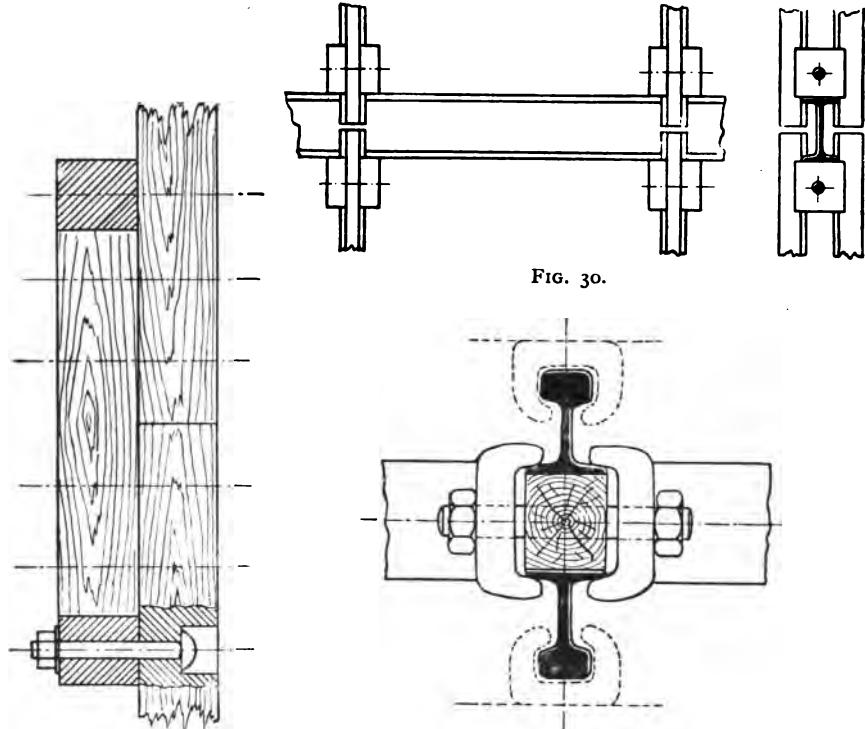


FIG. 29.

FIG. 31.

and floor of the cage, and engaging with the guides on three faces, with a play of  $\frac{1}{4}$ - $\frac{1}{2}$  in. Sometimes these short shoes are replaced by bars extending the full height of the cage. Both ends of the shoes are widened and rounded off.

Owing to the comparatively short life of wooden guides, and the disturbance to mining operations entailed by their frequent renewal, they are gradually being replaced by iron guides, which also enable the play between the guides and slides to be reduced,

thus improving the guiding and allowing a higher speed to be safely attained in winding. On the other hand, they retard the action of the safety clutch. Figs. 30 and 31 represent the Briart guides, made of iron rails; but U- or T-irons can also be used.

*Wire Rope Guides* are very popular, for medium depths, in English pits. The guide ropes—closed rope or cable constructed of a few thick wires ( $\frac{2}{5}$ — $\frac{3}{5}$  of an inch in diameter)—are anchored firmly above-ground, and hang free in the shaft, down to the very bottom, where they are passed through a frame built into the shaft walls, and are strained taut by means of heavy weights. The cages, however, sway considerably, so that a free space of 12-16 ins. must be left on either side; and hence, although cross timbers are dispensed with, these guides require wide shafts. The eyes traversed by the ropes are usually of hard bronze, and the cages are guided at three or four points. Sometimes the ropes between the cages are not used for guiding, but merely to prevent their coming in contact with each other.

Guides of iron or wire rope must always be kept well greased.

**Safety Catches.**—These are designed to prevent the cage falling down the shaft in the event of a breakage of the winding rope. These accidents may be caused by defects in the rope or connections, overwinding, sticking or jamming of the cage—in which event, on the down journey, the rope may hang in loose coils above the cage, so that the latter, when released, falls suddenly and breaks the rope. Other causes are: fractures of the guides, head pulleys, etc. The fundamental principle of safety catches can be gathered from a description of the appliance of White & Grant, illustrated in Fig. 32. When the rope is taut, the spring, *f*, is held in tension, and the toothed catches, *F*, are in the position shown, *i.e.*, about  $\frac{1}{8}$  of an inch from the guides. When the rope breaks, the spring, *f*, is released, and then presses the pivoted catches, *F*, so tightly against the guide beams that the teeth bite into the wood, the weight of the cage pulling them further in. As the spring is also released when the cage is held by the keps at the pit eye, the weight being then off the rope, corresponding recesses are cut in the guides; and the condition of the catch can always be ascertained by watching

how the eccentrics, F, play when in this position. Swayings of the rope, and the pressure of acceleration under increasing velocity in winding, often reduce the rope tension on the descending cage. To prevent the catch coming into action under these circumstances, only about  $\frac{1}{10}$  of the weight of the empty cage is applied to keeping the spring, f, in tension; and this proportion can be suitably modified by using several springs, or a train of levers between the spring and the rope. The residual weight of the cage and load is taken up by a connection, A, of the king rod, or by stirrup chains.

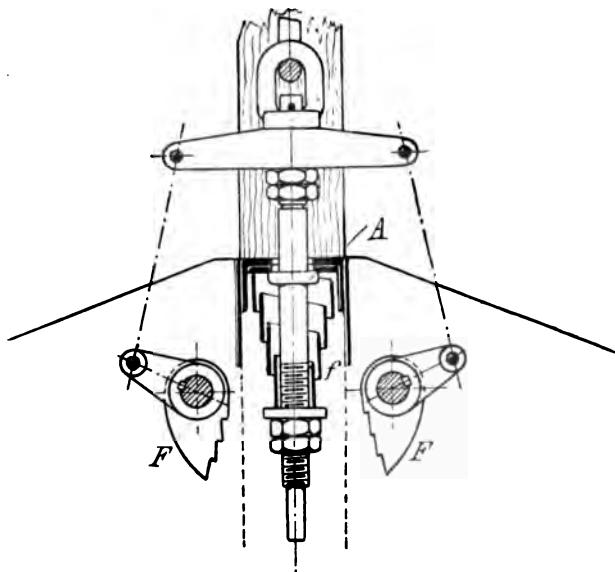


FIG. 32.

Von Hauer divides the safety catch into three parts:—

1. The catches (F, in Fig. 32);
2. The motor (the spring, f, in Fig. 32);
3. The intermediate gear, conveying motion between the motor and the catch.

The stopping of the cage should ensue as quickly as possible, before it has had time to attain any high velocity in falling, and before the effectiveness of the appliances has been impaired by the slinging and looping of the rope tail. The principal conditions favouring the rapid action of the catches are: short length of stroke

of the catch from the position of repose to the point of contact with the guides, and a relatively short travel of the rope end (stirrup, king rod) against the cage. The spring tension should be as high as possible, the play of the spring necessary to bring the catch into action small, and the difference between the spring tension for raised and depressed catch slight.

Latterly these quick-acting catches have been progressively abandoned in favour of fall brakes, which act without shock, the kinetic energy of the descending cage being gradually consumed during a long brake stroke. The resistance checking the cage

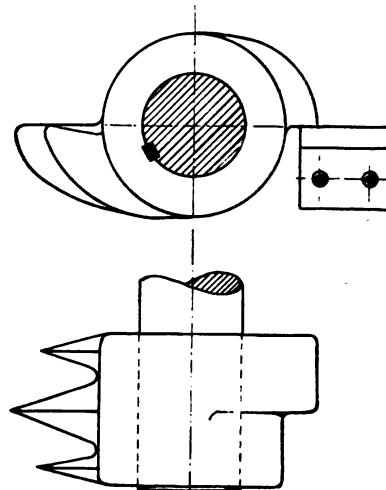


FIG. 33.

when the catch comes into play must increase from zero to a figure equal to two or four fold the weight of the cage at least; but, on the other hand, must not be of such magnitude that the check is too suddenly applied. The old White & Grant safety catch has been altered into a fall brake, in a very ingenious manner, by Oberegger, for example. The catch (Fig. 33) consists of three knife edges, which, when pressed against the guides, cut furrows in the wood. The depth to which they can penetrate is limited by a stop, which forms a measure of the maximum braking resistance, the latter being also capable of apportionment according to the weight of the cage, by adjusting the angles of the cutters.

Externally similar to the old eccentric catch is also the new brake-action safety catch of Gerlach & Boemke (Fig. 33a). In the event of the rope breaking, a spring turns the catch shaft, W, in the direction of the arrow, and presses the toothed rings, R (which are mounted loose on the eccentric disc, S), against the guide. The rings revolve and set up strong friction against S ; and the pressure between R and the guides increases, by the nearer approach of the eccentrics, until the *vis viva* of the cage is consumed.

By altering the angle at which the eccentrics are set, the braking action can be accelerated or retarded, or the catch can be utilised for greater or smaller loads.

*The Muenzner Safety Catch* (Fig. 34, Plate I.) is also largely used. As can be seen from the sketch, Fig. 34a, the blades A, B are turned in the direction C, D for action, thus forcing their way into the guides and cutting furrows in the wood. The pivots of the blades are connected by a cross-piece, which is pressed downwards in the event of the rope breaking. This catch also merits special attention as having been employed, in conjunction with the Undeutsch apparatus, for the determination of very precise measurements respecting the distance traversed between the time of the rope breaking and the catch coming into action, and also of the injurious effect of the breaking of the rope, and the subsequent check, on occupants of the cage. If, in addition, the resistance opposed to the blades by the wood be determined by experiment, then all the materials for calculation will be at hand.

*The Hoppe Catch* (Fig. 35).—This is used in the case of guides of T-iron, the spring released on the breaking of the rope raising the two brake cheeks until they press firmly on the surface of the iron guides. The resulting friction causes the brake cheeks to lag behind the cage, the eccentric elbow-levers, K, assume a more and more horizontal position, and the pressure increases until the further movement of the cheeks is prevented by striking against a stop on the cage frame. From this point onwards the pressure and friction between the brake cheeks and the guide remain unaltered, the *vis viva* of the cage is gradually consumed and the latter brought to

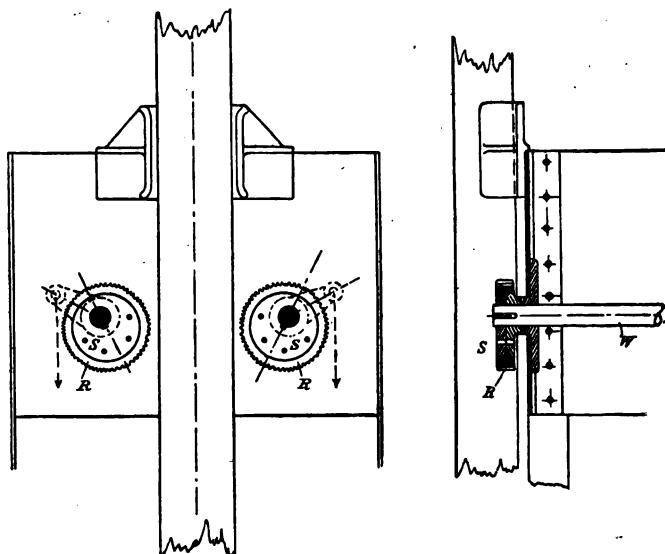


FIG. 33a.

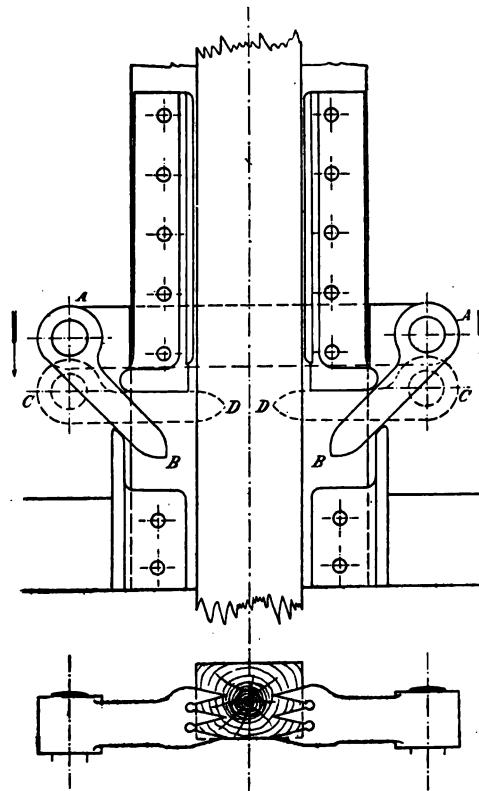


FIG. 34a.

a standstill. The distance traversed in the interval is often 5 ft. and over. The pressure on the levers, K, tends to force the abutments, W, outwards, and if these are bolted firmly on to the framework, there ensue in the latter elastic changes of form which determine the extent of the maximum pressure exerted by the brake cheeks. This pressure, however, will be immediately reduced in a considerable degree as soon as the guides are worn down a small fraction of an inch, and consequently the outward thrust of

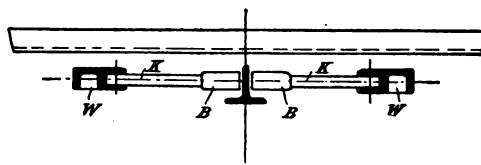
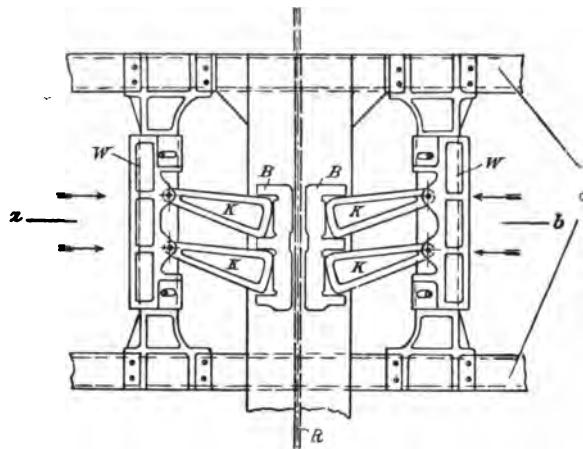


FIG. 35.

the abutments is correspondingly reduced. For this reason the abutments, in the later models, are mounted so as to slide in the direction  $a, b$  instead of being bolted fast. By the intermediary of elbow-levers, the pressure of very powerful springs is transmitted, in the direction of the arrow, to the abutments, the flexion of these springs thus fulfilling the same purpose as that of the framework in the older pattern, with this difference, however, that the brakes still act in a reliable manner even when the guides

are considerably worn. At the same time no troublesome adjustment is necessary, neither does the brake act too forcibly and suddenly in the case of new guides.

In the case of Briart guides, the Hypersiel catch is often used, in which, on the rope breaking, a fork, fluted on the inside and tapering downward, grips against the guide bars (Fig. 35a).

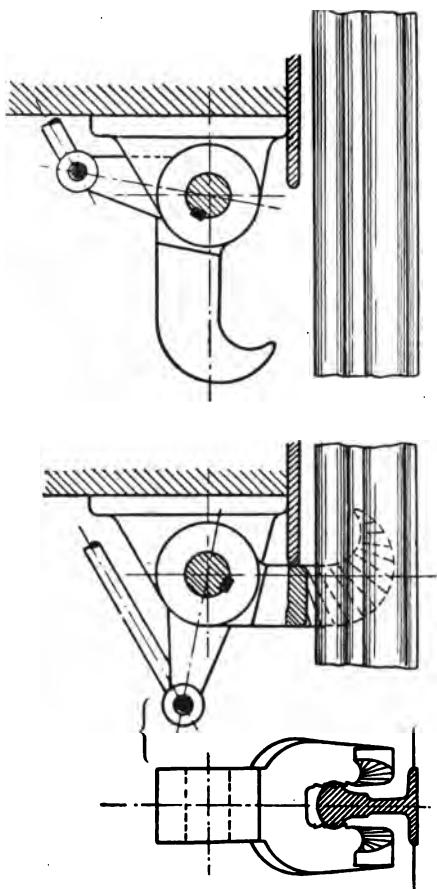


FIG. 35a.

**Connection between Cage and Rope Cap.**—In Fig. 32 the cage is shown suspended by a bridle chain attached to the rope cap, a swivel and an adjusting screw being often interposed between them, as shown in Fig. 36, the former appliance serving to correct the twist of new ropes, and the latter for accurately regulating the

length of the rope. In the event of the bridle chains breaking, the load is taken up by safety chains between the rope cap and the upper frame of the cage. The bridle chain is made of best wrought-iron, and must be examined daily, and also be carefully annealed from time to time. At the same time the bridle chain prevents the looping of the over-long rope when the cage is on the keps, and

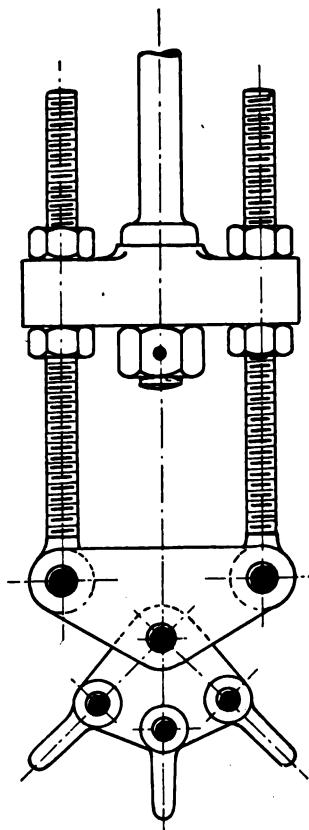


FIG. 36.

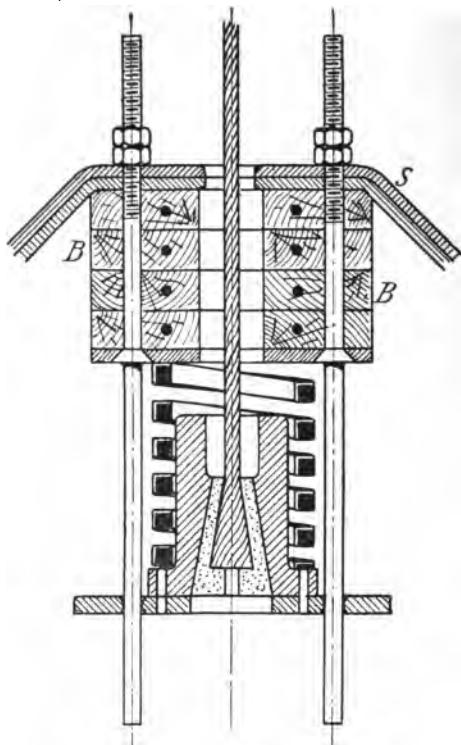


FIG. 37.

thus protects the wires from breaking above the cap. However, in improved forms of winding drum, the length of rope can be so accurately adjusted that it is possible to dispense with the dangerous bridle chain.

Fig. 37 shows a method of connecting the cage and rope, in which hanging of the rope is prevented by a spring and guide

blocks, BB, whilst ensuring at the same time an elastic starting pull.

On the other hand, such springs retard the action of the safety catch. Means must also be taken to prevent the rope becoming detached from the cage in the event of the spring breaking.

Every shaft should have at least five cages: two in use, an equal number in reserve, and one under repair. The reserve cages should be kept on low trucks, to facilitate changing as quickly as possible.

#### KEPS.

It is essential that, both at bank and at the pit eye, the cage should rest exactly on a level with the tracks on which the tubs are conveyed; and to retain the cage in that position the appliances known as keps are provided.

The simplest form of keps is shown in Fig. 38, and consists of pivoted stops, *a*, mounted loose on a shaft and abutting on the nose-pieces, *c*. Two levers are keyed on this shaft, a long one, *b*, and a short one, *d*, carrying studs engaging below the stops. The ascending cage which lifts the loose stops must be drawn up far enough above its position of repose for the stops to fall back underneath it into their original position, whereupon the cage is lowered again on to the keps. When the exchange of tubs is completed and the cage is to be lowered again, it must first be lifted far enough to allow the stops to be turned back by means of the lever, so as to leave the shaft free for the cage to descend. At the pit eye the cage rests on the projecting stops, direct. Of course when coal is wound from haulage roads at different levels in the shaft, great care must be taken to prevent any of the intermediate keps being allowed to project, either by accident or of *malice prepense*. Lockable keps, or signals indicating to the engine driver which keps are set, are in use.

When work is very brisk, the time consumed in raising the cage above the keps, lowering it, and then raising it again, becomes inconvenient, and consequently keps have been introduced that allow the cage to descend without the preliminary lift. Most of these appliances are based on the action of elbow-levers. Out of the

numerous existing types—constructed by Frantz, Ochwadt, Westermeyer, Stauss, Albert and others—mention may here be made of the “Asphaleia” keps (Fig. 39). A shaft,  $d$ , is mounted in two slides,  $b$ , capable of moving back and forth in slots cut in the frame,

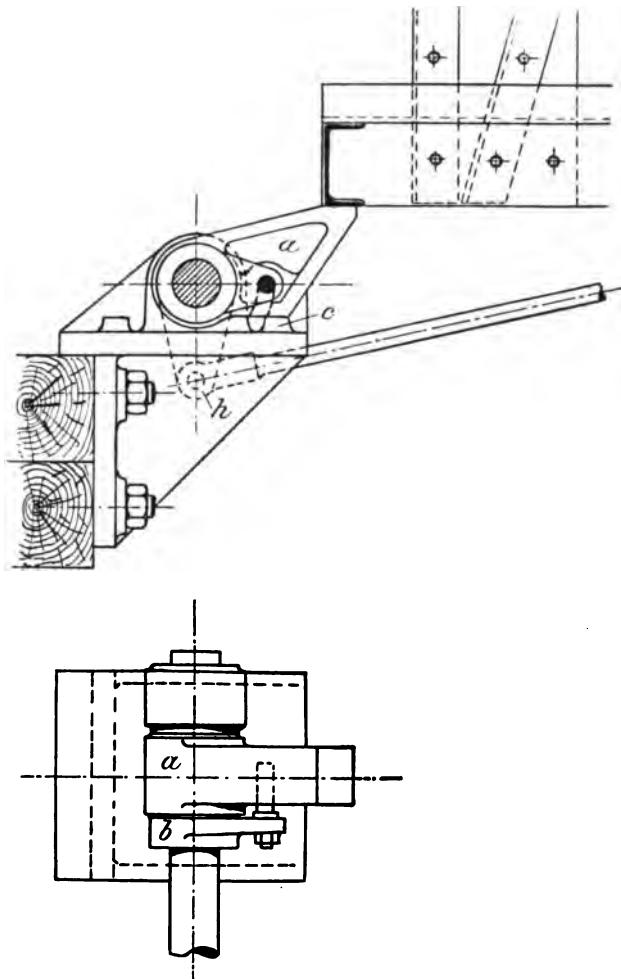


FIG. 38.

*a.* The shaft,  $d$ , carries the loose stops,  $e$ , and the lever,  $k$ , which forms a double joint with the lever,  $h$ , keyed on the hand-lever shaft,  $g$ , which joint is slightly depressed when in the position of repose. Counter-stops,  $o$ , are fixed on the under frame of the cage. Setting-on is effected the same way as before, the cage being lifted

a few inches above the level of the bank. To allow the cage to descend the lever is pulled and draws back the stops, the cage

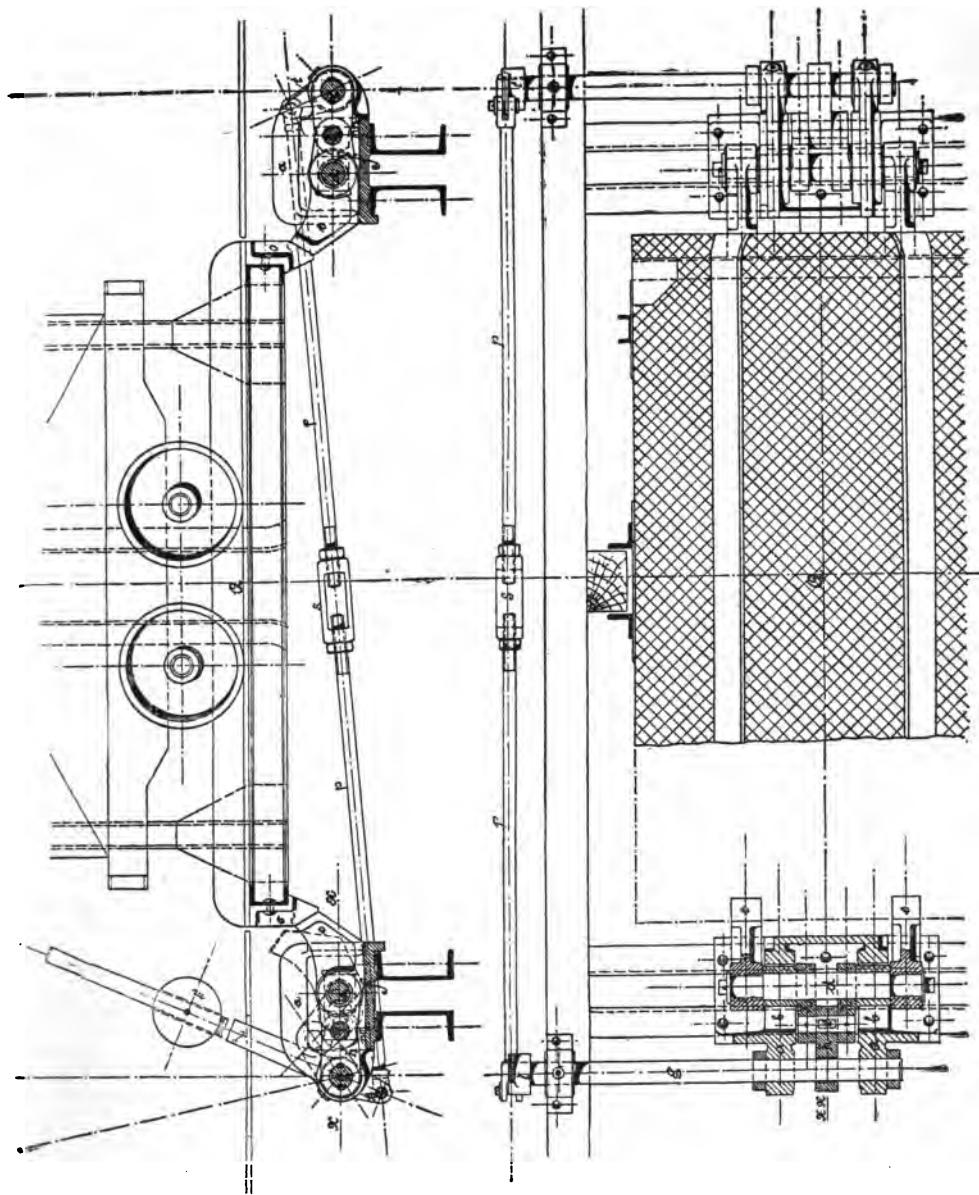


FIG. 39.

sliding quietly over the sloping surface thus presented, and consequently there is no jolting, even if the rope hangs somewhat loose.

Fig. 40 represents the Haniel & Lueg keps, when the cage is set on, and also when the latter is descending and rising, respectively. The bearing frame, *g*, and the lever, *k*, keyed on the shaft, *f*,

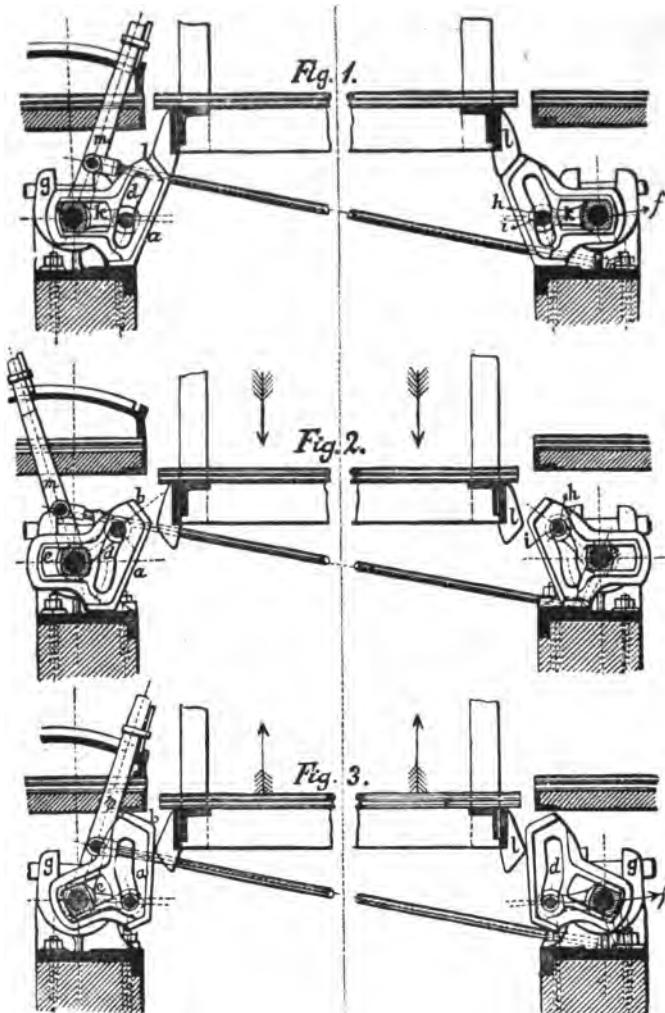


FIG. 40.

are in duplicate, one on either side of the stop, *a*. When the hand-lever is moved, and *k* with it, the pin of the stop is drawn backwards in the slot, *d*, and thereby slides on the base-plate and on the block seen in cross-section. This latter is loosely mounted on the

shaft, *f*, so that the ascending cage is enabled to move the stop and the block upwards in the manner shown.

To reduce the shock in setting-on the cage, it is preferable to mount the keps on somewhat elastic iron or wooden girders.

**Shaft-closing Devices.**—The opening of the shaft is enclosed by railings, provided with doors or collapsible lattices, which are closed except when the cage is in position for the change of tubs. As a rule these shaft doors are locked by bars which are pushed away by the cage, and when the shutter-gates are collapsible in a vertical direction, they are fitted with arms, which project into the

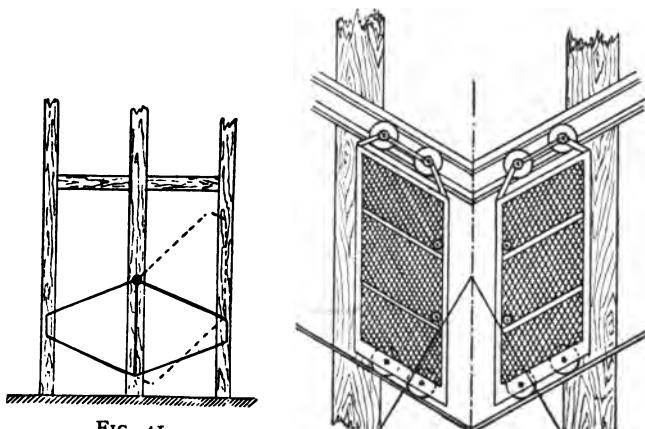


FIG. 41.

FIG. 42.

shaft and are lifted by stops on the rising cage. To prevent concussion, the lattices are made as light as possible and counterpoised, and the cage stops are fitted with buffers. The task of lifting the lattice can also be performed from the winding drum shaft, a wire rope attached to the gate being passed over pulleys to the engine room and there wound on a small drum, which is set in motion by the engine just before the cage reaches the bank. The coupling up of this drum at the proper moment may be effected by a collar moving along a revolving screw spindle.

Doors are also provided at the pit eye, chiefly for the purpose of preventing the tubs being run into the wrong winding compartment

of the shaft. A simple form of these doors is shown in Fig. 41, consisting of a light rhombic frame pivoted at the upper angle and turned by the oncoming cage in the direction shown by the dotted lines, thus closing the other compartment.

An automatic closing device, the Mauerhofer system, specially designed for intermediate floors in the case of hoists or blind shafts, is shown in Fig. 42. The opening into the shaft is closed by two sliding doors running on inclined rails. The cage is fitted at the top and bottom with a wedge-shaped attachment that makes contact with small rollers and pushes the doors outwards.

**Closing Device for Ventilating Shafts.**—If the winding shaft

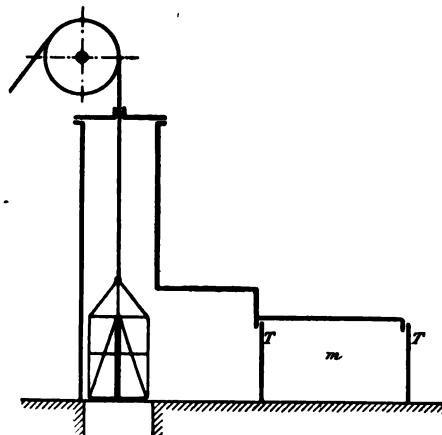


FIG. 43.

also serves for ventilation (as an upcast), it must be closed at the top. In Fig. 43 the pit mouth is enclosed in an air-tight tower of masonry or iron, the change of tubs being effected by the aid of two tight-fitting doors, T, and the chamber (air lock), m, without allowing the outside air to gain access to the shaft. A simpler method is to close each winding compartment with a cover, in the centre of which is an aperture for the passage of the rope. This aperture in turn is closed by a small cover which shares the unavoidable swayings of the rope. Below the mouth, the shaft is lined for a distance rather deeper than the height of the cage, and of such diameter as to leave but very little play at the bottom of the cage. By this arrangement the ascending cage first closes the

winding compartment and then pushes up the cover. The shock is ameliorated or prevented in the same way as with lattice doors.

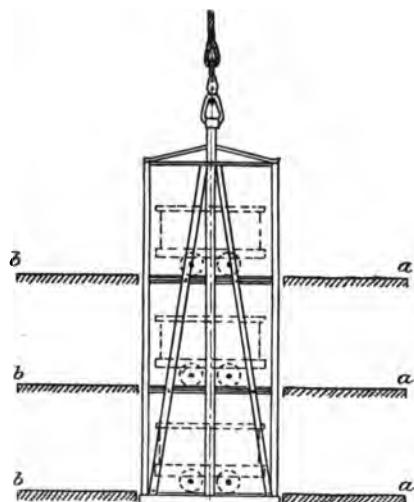


FIG. 44.

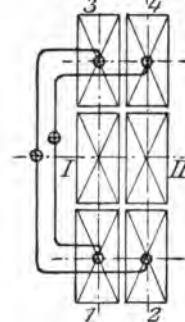
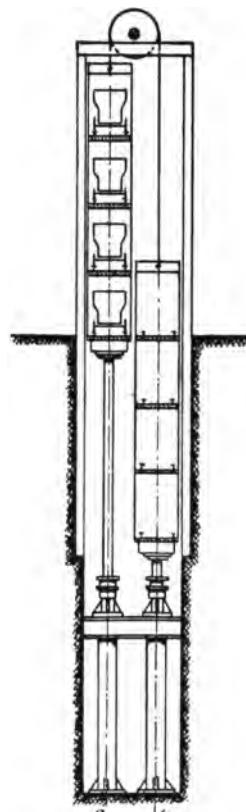


FIG. 45.

#### CHANGING TUBS IN MULTIPLE-DECK CAGES.

1. The several decks are successively brought to the level of the bank by raising or lowering the cage with the engine.

This method wastes time, entails great care on the part of the driver, and increases the consumption of steam. It is particularly unsuitable when conical drums or pulleys are used, wherein the rope coils are of unequal diameter, and consequently in raising or lowering one cage the other does not move to an equal extent.

2. The lowered cage is not adjusted by the engine, but rests on a platform that is lowered the height of a deck after the tubs have been changed. This facilitates the handling of the cage, especially in the case of conical winding drums.

1 and 2 cannot be recommended for cages with more than two decks.

3. Changing the tubs on all decks simultaneously. In this system, floors,  $\alpha$ ,  $b$  (Fig. 44), of the same height as the cage decks, are provided at bank and the pit eye. The tubs are pushed out of all the decks at once on to the floors,  $\alpha$ , whilst those to replace them are kept ready on the floors,  $b$ . The cage then makes a trip up or down the shaft as the case may be, and in the interval the tubs on  $\alpha$  are removed, whilst fresh ones are run on to  $b$ . This is effected by tracks running from the different floors to a common level (a plan that entails greater space than is conveniently available, at the pit eye especially), or else by the aid of small hoists, or movable hydraulic stages, the best method being to make the floors  $\alpha$ ,  $b$  movable, so that there are, as it were, supplementary cages on each side of the actual working cages.

Fig. 45 shows the arrangement devised by Tomson. The supplementary cages 1 and 2, 3 and 4, are connected by a chain, and also rest on hydraulic plungers, the cylinder of No. 1 being connected with that of No. 4, and the same applying to Nos. 2 and 3. Then, if the full tubs are loaded on to No. 1, their weight in descending raises No. 4, which is filled with empties on each deck as fast as No. 1 is discharged. On cage 2 coming to bank the full tubs are discharged into 2, which raises No. 3, and the empties from No. 4 take their place, and so on.

A regulator enables the rate of descent to be controlled and the cages to be stopped in any position, and also admits water to the hydraulic cylinders in the event of the weight of the full cage being insufficient to raise the corresponding empty one.

## CHAPTER IV.

### WINDING ENGINES FOR VERTICAL SHAFTS.

THIS work is performed by the aid of steam, compressed air, water power or electricity ; more rarely by hand labour or animal power (winches, whims).

#### (a) STEAM ENGINES.

The general arrangement of a steam winding engine is shown in Fig. 46 (Plate II.). On the engine shaft are mounted two drums, from which the upper and under ropes run over guide pulleys to the shaft. The one rope, carrying the full cage, is drawn up, the other, with the empty cage, descends. Consequently, the ropes are alternately wound and unwound on the drums, which latter must therefore change their direction of movement every trip. On this account the engines have to be reversible, and generally also capable of overcoming different resistances, since not only may the load vary in each trip but also the pull exerted by the descending cage increases with the weight of rope paid out, whilst that of the ascending cage decreases. Hence the reversing and valve gear is the most important part in a winding engine, the other parts differing nothing in principle from ordinary engines.

#### *Reversing Gear.*

It is only in the case of small winches, or when locomotive engines are used, that the direction of movement of the winding drum can be changed without reversing the engine ; for the most part the latter must be fitted with reversing gear.

1. **Slide Valve Gear.**—The reader is presumed to be acquainted with the nature of simple shell-valve gear.

The internal gear parts comprise ordinary shell valves, load-freeed flat valves, separated slide valves, Allan trick valves, plunger valves and rotary valves.

However, as in locomotives, the simplest forms alone have made any headway. The *external* parts consist almost exclusively of eccentrics, link-motion and valve-rods. Only in the case of so-called "internal valve gear" (without expansion, suitable merely for small winches) is the link-motion dispensed with. Reversing by means of loose or sliding eccentrics has gone out of use.

(a) *Link-motion Gear*.—The Stephenson link-motion is shown in Fig. 47a. On the crank shaft are two eccentrics,  $E_1$  and  $E_2$ , set at an angle of  $90 + \delta$  with the crank. The eccentric-rods are attached to the ends of the sector, which is suspended by a pivot,  $w$ . The valve-rod,  $s$ , passes through a special guide, and is bolted on to a

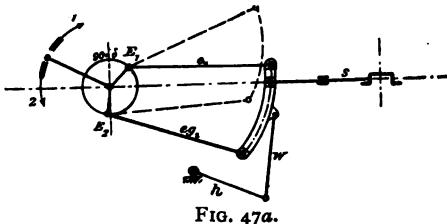


FIG. 47a.

sliding piece. When the link is in its lowest position, as shown in the Fig., the movement of the eccentric-rod,  $e_1$ , is transmitted to the valve, with practically no alteration, and the gear works as though only a single eccentric were present, set so as to lead the crank by an angle of  $90 + \delta$ . Motion occurs in the direction indicated by the arrow, 1. When the lever,  $h$ , is raised and the link consequently lifted into its highest position, then the motion of the eccentric-rod,  $e_2$ , is transmitted to the valve. At the same time, as can be seen from the Fig., the valve is reversed, and the engine begins to run in the direction of arrow 2, since the eccentric necessarily always leads the crank. When the link is in the central position, the steam pipe is closed, or at any rate opened to such a small extent that the engine does not continue to run.

It can be demonstrated that, in any position in which the travel of the valve is influenced by both eccentrics, the valve play is pre-

cisely the same as though there were only one eccentric present, but with a lead greater than  $\delta$  and a diminished eccentricity, and therefore a valve with earlier cut-off. The momentary centre of such a hypothetical single eccentric, which, for any given position of the link, would give the same distribution of steam as the two actually present, is situated along the dotted curve  $E_1, E_2$ , Fig. 47b.

The shape of this curve causes an alteration in the so-called

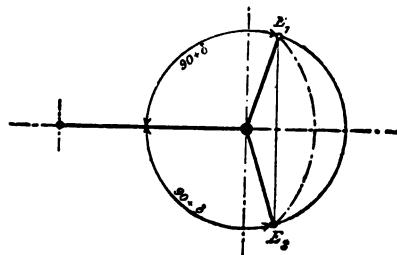


FIG. 47b.

"linear lead" (the opening of the admission valve when the crank is at a dead point), which is increased as the cut-off is accelerated. This defect is obviated by Gooch's device, wherein the centre of the supposed eccentric is displaced along the straight lines  $E_1, E_2$ . Fig. 48 shows that in this gear it is the sliding piece and not the link that is raised and lowered. The gear is longer than that of Stephenson, and is therefore unsuitable for necessarily compact

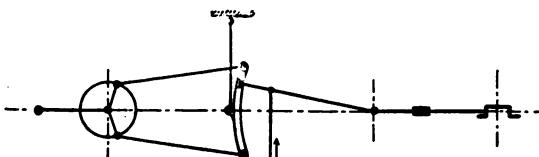


FIG. 48.

engines. The other classes of valve gear (those of Allan, Heusinger, Fink, Klug, etc.) are not much used; they are more suitable when, as in the case of locomotive or marine engines, it is desired to have a particularly favourable distribution of steam during the forward movement of the engine. Occasionally, separate admission and exhaust valves, each fitted with link-motion, have been constructed; but though these are accompanied by advantageous lead and

cushioning, together with high expansion, they are more difficult to look after.

*Movement of the Reversing Lever.*—It has been mentioned that the raising or lowering of the link also entails the shifting of the valve, and hence the friction of the valve has to be overcome. For this reason the reversing of large engines with flat valves necessitates a considerable exertion of force. Now, it is essential for rapid, and at the same time safe, winding, that the reversing-lever should be movable with ease and celerity; and, if only for this reason, preference is given to plunger or circular valves over flat ones.

The working of the lever can be facilitated by supplementary

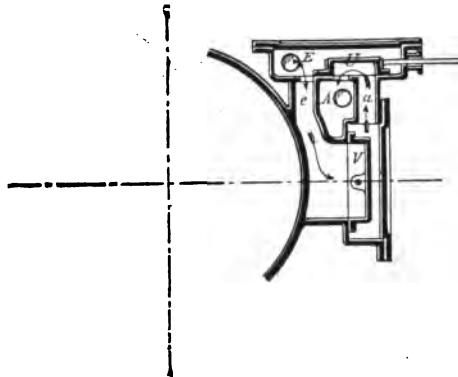


FIG. 49.

gearing, consisting of a small cylinder (for steam or hydraulic power), the piston of which actuates the reversing-lever, leaving only the valve of this supplementary engine to be worked by the driver. Naturally, this supplementary engine must enable the gear to be set to any desired cut-off, and consequently the cylinder diameter is usually made so small that the cylinder pressure is insufficient to move the link without the assistance of the machinist; or the piston-rod of the supplementary engine is prolonged rearwards and fitted with a second piston which works in a braking cylinder. The latter is filled, *e.g.*, with oil, and communication is established between the two ends, so that when the desired position of the link is attained, the closing of this means of communication prevents any further movement of the supplementary piston.

(b) *Internal Reversing Gear.*—This class of gear prevents any lap or lead, and therefore any expansion or cushioning. The steam consumption is high, and the efficiency is diminished by throttling, or applying a brake to the main shaft.

Internal reversing gear is divided into two kinds. In one, the engine is reversed by means of a special reversing slide or cock, which causes the admission valve to play the part of the exhaust, and *vice versa*; in the other, the distributing valve is composed of two valves, one acting while the engine is running forwards, the other when it is reversed. A type of the first kind is illustrated in Fig. 49. When the reversing valve, U, occupies the position shown, the distributing valve, V, acts as admission valve, the steam entering from the inside, and the space above the valve is in communication with the exhaust, A. On turning U towards the left, the steam enters through  $\alpha$  and escapes through  $e$ . It is necessary to provide some means of preventing the valve being raised from its seat by the steam pressure when the steam enters from the inside.

*Inter alia*, the Danek and Fouquemberg valves (Figs. 50 and 51 respectively) belong to the second class. Fig. 50 shows that the “positive” valve,  $m$ , and the “negative” valve,  $n$ , are combined in the same piece. The valve-rod must be capable of turning so far on its own axis as to admit of either  $m$  or  $n$  being brought into position over  $\alpha$  or  $e$ . From the direction of the arrows, it will be seen how this movement immediately effects the converse steam distribution and causes the reversal of the piston movement. In Fig. 51 a movable valve-plate is arranged. The chambers 1 and 2 of the distributing valve communicate with the cavity, 5, whilst 3 and 4 communicate with the live steam. In the position shown, the piston moves towards the right; but on pushing the valve-plate to the left, the steam is admitted to the right face of the piston *via* 4—y—c, the exhaust passing away to the left through  $\alpha$ —x—1—5, and the piston is driven towards the left.

2. *Valve Gear.*—The short stroke and ready mobility of the valves enable them to be easily and rapidly opened and closed; there is but little resistance to be overcome in reversing, and they

are easily replaced and ground, a circumstance that compensates for the defect that they are liable to hammer extraneous substances into their seat, whereas flat or circular slides simply brush such substances from the surface.

The greatest wear on the valve spindles is produced at the part

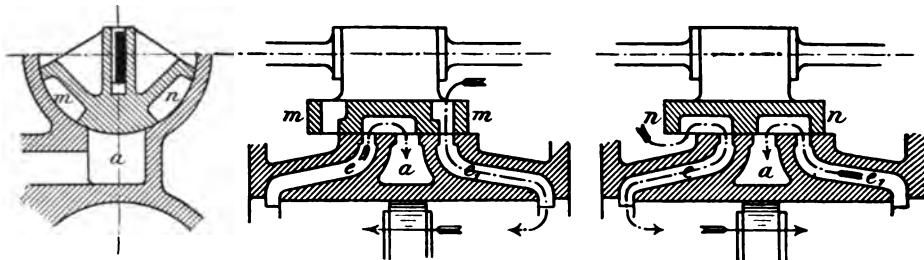


FIG. 50.

corresponding to a medium cut-off. If the engine is working with full admission (*e.g.*, at starting, etc.), there is a risk of the valve stem jamming in the gland, so that the valve is prevented from closing. On this account it is desirable to provide some means of compelling the valve to close. Cushioning valves of suitable dimensions should

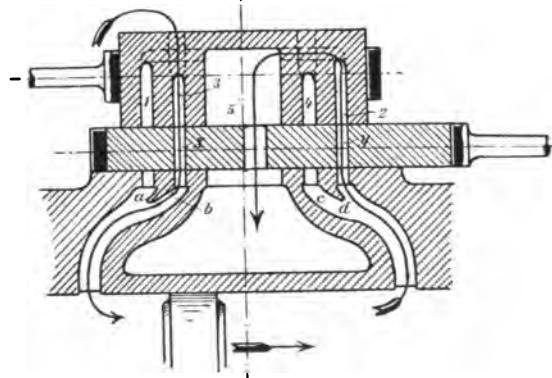


FIG. 51.

be provided at the cylinder heads, in order to prevent a dangerous compression during cushioning, and also to ameliorate water knocks. These valves open into the admission or exhaust pipes.

*Arrangement.*—An admission and exhaust valve are provided at each end of the cylinder. The valve chests are either bolted on

to the side of the cylinder, so that all four valves are close together,

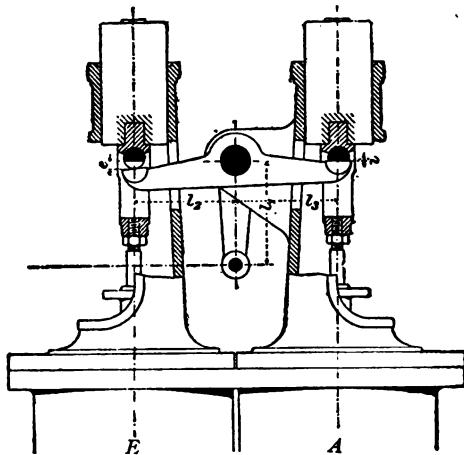


FIG. 52. (Note.—*E* = admission; *A* = exhaust.)

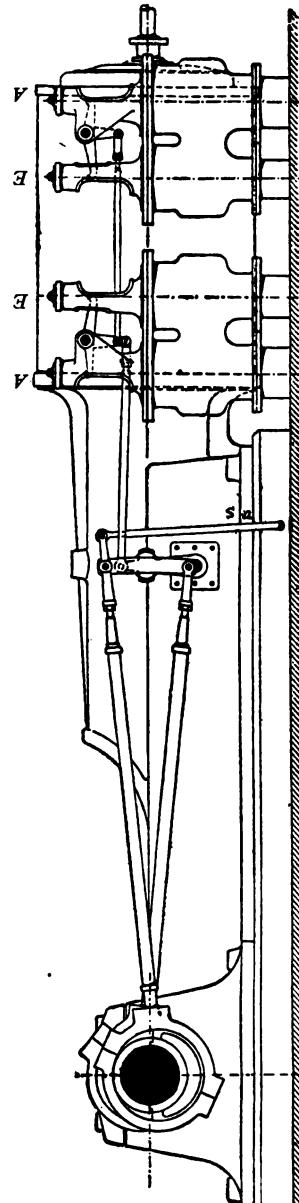


FIG. 53. (Note.—*E* = admission; *A* = exhaust.)

on about the same level, and readily accessible; or else the admission valves are situated above, and the exhaust valves in front of,

the cylinder; or, finally, they are arranged in the same manner as in ordinary engines.

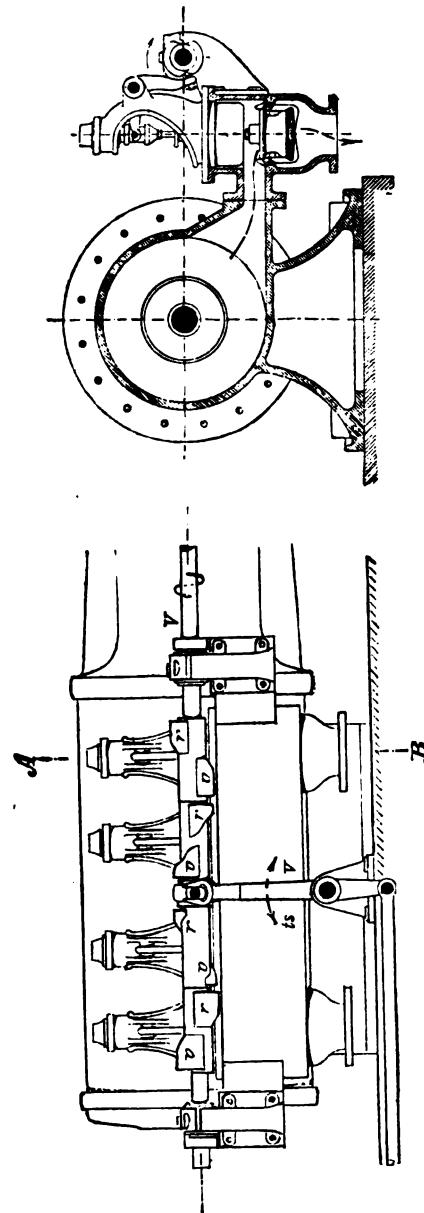


FIG. 54. (Note.—*ts* = backwards; *V* = forwards.)

The valves can be actuated from a pivot (Fig. 52), which is controlled by a link (Fig. 53). The distribution is effected in

exactly the same manner as with a link slide valve, though this partly nullifies the advantages of the arrangement ; nevertheless, the gear is simple and easily manipulated.

A form of valve gear very largely used is that of Kraft & Brialmont (Fig. 54). A valve shaft in front of the cylinder carries a number of oval collars, which actuate the corresponding valve stems by means of bell-crank levers. The shaft is provided with a feather, on which the collars are adjustable ; and each collar is fitted with two contact pieces,  $V_1$  and  $V_2$  (Fig. 55).

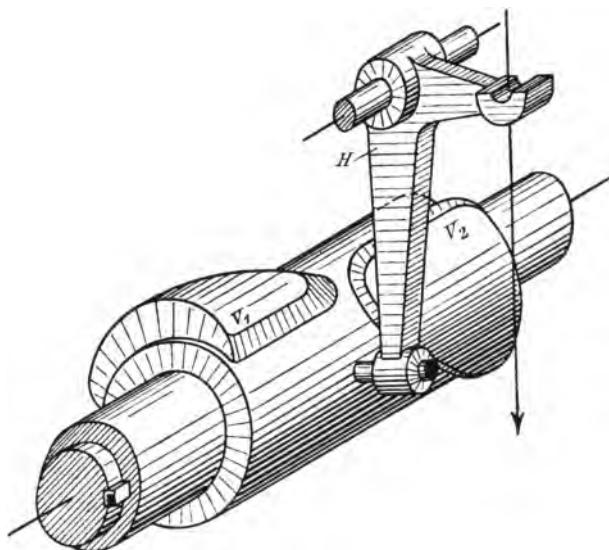


FIG. 55.

These contact pieces act on the cams (studs, or bowls) on the bell-crank lever,  $H$ , and open the valve, the reclosing being effected by a spring on the valve stem. When the cam is in the middle between the two contacts, *i.e.*, on the cylindrical part of the collar, then the valves are not raised ; but if the collar is slipped to the left or right, then  $V_1$  or  $V_2$  comes into play. The contact pieces are shaped and placed in such a manner that one series is for the forward motion of the engine, and the other for when the engine is reversed. Fig. 56 represents the unrolled surface of an admission valve collar, from which it will be evident at once that, in addition to reversing the engine, an alteration in the cut-off is very easily effected by

this means. The bevelled edge,  $\alpha$ , of the contact piece opens the valve, which remains in that position until the cam has passed the edge,  $\alpha$ . Since  $\alpha$  is parallel to the axis of the shaft, the lead remains unchanged for all positions of the collar, whereas the length of time the valve is kept open, and therefore the cut-off, is increased in proportion as the broader portion of the contact piece is made to act on the cam by sliding the collar. In engines working without rope compensation, and where consequently the consumption of power continually diminishes, it is advisable to correspondingly increase the expansion automatically, since experience teaches that the driver prefers to decrease the efficiency of the engine by throttling the live steam rather than by pulling back the valve-gear lever.

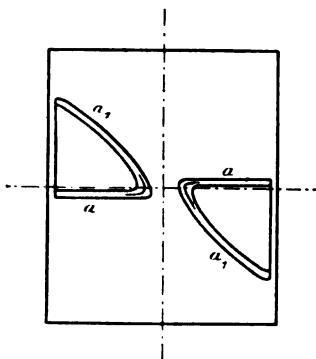


FIG. 56.

This automatic adjustment of the cut-off is effected as follows: The valve-gear shaft terminates in a slow screw thread, which imparts motion to a non-rotating nut, transmitting its own movement to a rotatable toothed sector, which is situated directly in front of the gear shaft and can be coupled thereto by a pawl. At the commencement of the trip, the reversing-lever is in its extreme outer position, and if now coupled with the toothed sector, shares the movement of the latter, and thus gradually approaches the middle position, the degree of expansion being increased to a corresponding extent. The reversing-lever can be released at any moment, so that the controllability of the engine is not prejudiced in any way by the adoption of this contrivance.

As a defect of this gear it may be mentioned that, in course of time, the studs or cams grind channels in the collars and thus impede reversing, a supplementary engine being then necessary.

The Radovanovic Parallelogram gear (Fig. 57) is a modification of Klug's reversing gear. The valve shaft carries an eccentric, the

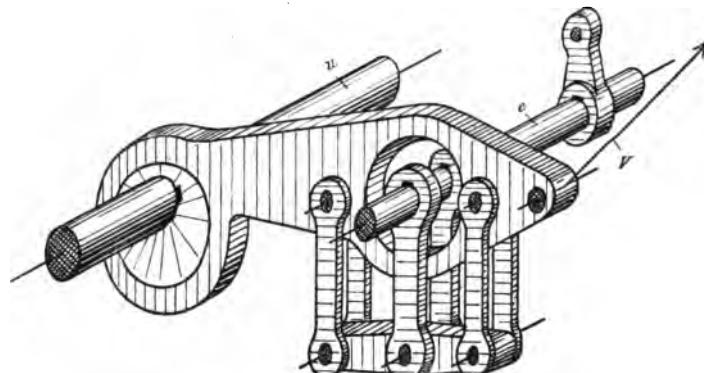


FIG. 57. (Note.— $u$  = valve shaft;  $e$  = reversing shaft;  $V$  = to the valve.)

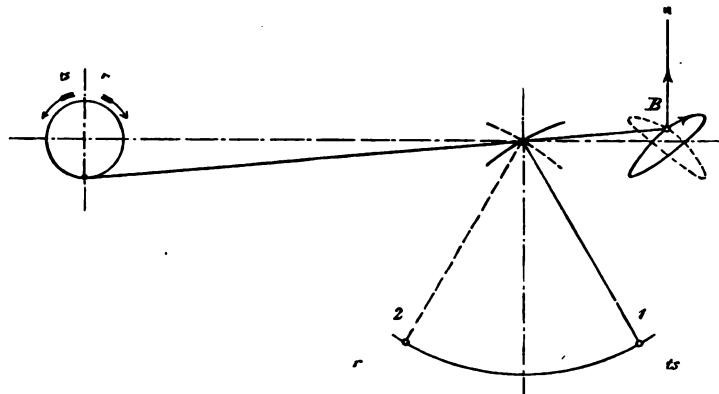


FIG. 58. (Note.— $ts$  = forwards;  $r$  = backwards;  $z$  = to the valve.)

elongated rocker of which actuates the valve. A circular aperture is cut through this rocker, and the centre of this aperture describes an arc, the centre of which can be displaced by turning the valve shaft, with the result that the cut-off is modified. The crank can also be reversed by the same means.

The path of the pin, B, for positions 1 and 2 of the lever, H, is shown in the diagram (Fig. 58).

The perfectly central arrangement of all the parts precludes one-sided wear, reversing is easy, and the steam distribution favourable, especially under high admission pressure, no further disturbance being caused by the increased cushioning resulting from early cut-off.

#### *Winding Drums.*

The winding drums take up the rope when rotated by the engine.

Fig. 59 (Plate III.) represents a fast-coupled drum, whilst Fig. 60 shows a portion of a detachable drum, which can be quickly uncoupled from the engine shaft. When it is desired to alter the depth from which the cage has to be raised, the length of the tail rope must be changed whilst the second cage is at rest. The cage worked by the detachable drum is raised to bank, and, the drum being held fast by the brakes, the coupling to the engine shaft is loosened, the engine being then started and the other cage raised or lowered until the desired position is reached ; this done, the loose drum can be coupled up again. Another way is to set the upper cage on the keps, detach the rope, lap it round the drum and fasten it in place, the other cage being then brought into the desired position by the engine.

The detachable drum is attached to the keyed (tangent wedges !) rosette on the engine shaft by bolts, the total shearing strength of which is three times the mean strain they have to withstand. The numerous slots in the rosette enable the position of the drum to be adjusted so as to reduce the shortening of the rope to a minimum and thus avoid slack rope. A more recent form of detachable winding drum, shown in Fig. 61 (Plate IV.), is fitted with wrought-iron spokes and wrought-iron rim. A toothed wheel is keyed on the shaft, and the motion of the shaft is transmitted to the drum by toothed sectors, which can be advanced or drawn back by hand wheels. When the drum is uncoupled the cast-iron hubs run in split metal bushes, which can be easily replaced when worn.

For small drums, friction couplings are also employed.

The rope is fastened to the drum by passing the end through the casing of the latter and lashing it to the shaft or to one of the spokes. As a rule there is no strain on this fastening, the pull of the rope being taken up by the extra turns on the drum.

The weight for counterpoising the reciprocating parts of the engine can be attached to the drum rosettes; and this greatly facilitates uniform slow winding for the inspection of the shaft, etc.

Each wheel of the drum has 6 to 12 spokes properly stayed by St. Andrew's crosses and transverse struts, so that the rope strain is taken up equally between the two.

The drum is faced with oak timbers  $2\frac{1}{2}$ -5 ins. thick, in which grooves are turned; and recently sheet-iron with a thinner wood lagging, or fluted cast-iron segments, have been used for facing the drums. A section of this latter type of facing is shown in Fig. 62.

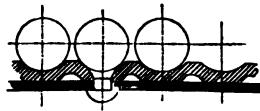


FIG. 62.

*Dimensions.*—Diameter according to the thickness of the rope; width  $b$ —for a single layer of rope—depth of shaft  $h$ , drum circumference  $2R\pi$ , rope thickness  $d$ , and number of extra turns  $n$ .

$$b = \left( \frac{h}{2R\pi} + n \right) d.$$

$b$  is seldom less than 5 ft., so that for deep shafts  $R$  must be considerable, and, under certain circumstances, the injurious overlapping of coils on the drum must be put up with. The strength of the spokes must be based on the maximum rope strain, consisting of the weight of load, cage, and length of rope paid out. Furthermore, the spokes must be capable of standing the extra strain ensuing should the rope break.

#### *Compensating Weight of Rope.*

In deep shafts the weight of rope to be lifted at the commencement of the cage trip is an important factor. Powerful

machines are needed, but, since the work to be done decreases in proportion as the weight of the descending cage comes into play, the cut-off must be progressively accelerated or the steam pressure reduced. However, as engines of constant power are more economical in work and can be more efficiently controlled, it becomes desirable to compensate the resistances, an effect obtained by the following means :—

1. By weights that act with the engine during the first part of the trip, but against it in the second half (tail rope, Gerhard's compensation, etc.).
2. By modifying the effective radius of the winding drum (conical drums and bobbin pulleys).
3. By storing up (*e.g.*, by means of pumps and accumulators) the surplus power of the engine during the second half of the trip, and utilising the same during the first half of the succeeding trip. This method, however, is not used.

The most important in the first group of methods is that of compensating by means of the

**Tail Rope.**—To the bottom of each cage is attached a rope of equal weight, per unit length, with the winding rope, and hanging down in the shaft to a depth exceeding that of the lowest pit eye. Thus, during the whole of the trip a uniform length (and therefore weight) of rope is in action, and the compensation is therefore complete. The defects of this system are the great weight to be moved, the dangerous swinging of the tail rope in winding at high speed, the difficulty of looking after the tail rope, the heavier load on the winding drum shaft, and the heavier strain imposed on the rope cap, which has to bear the weight of the tail rope in addition to that of the cage and load. In the event of the rope breaking, the safety catch must be strong enough to support the additional load entailed by the presence of the tail rope. Moreover, since, when a tail rope is used, the strain is uniform at all portions of the rope, tapered winding ropes cannot be employed, and consequently tail ropes are only suitable for shallow or medium shafts, though for these the system is the simplest possible means of compensating the resistances, especially when the winding is confined to one level.

Tail ropes may consist of old winding rope, flat rope, or aloe-fibre rope, the last named, for instance, when the rope pulleys are close together, and where consequently the rope has to form a small loop. In some cases partial compensation is employed, the tail rope being lighter per unit length than the winding rope.

With a view to winding from different depths, the main and tail ropes are often connected in the following manner:—

The main rope, instead of terminating immediately above the cage, is passed right down through the latter, so as to leave a long piece hanging, which is then connected with the tail rope by a loop and spring gland, the attachment of the cage to the main

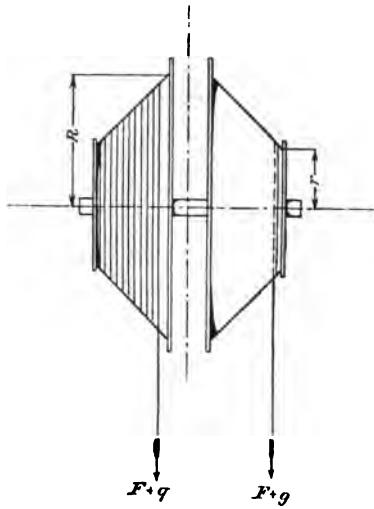


FIG. 63.

rope being effected, *e.g.*, by a Baumann rope clamp. To adjust the cage for winding perhaps from a higher level, the cage at bank is detached from the rope, and the second cage raised to the higher level in question, the rope at the same time running freely through the clamp of the stationary cage, which is afterwards connected up again by the clamp.

For very shallow depths the rope may be replaced by a chain, each cage carrying a piece of tail chain, which gradually coils on the shaft bottom as the cage descends, and *vice versa*.

**Conical or Taper Drums.**—Tapered drums are shown in Fig. 63. As the loaded rope ascends and the empty one descends, the

leverage of the drum radius on which the load acts is increased, the weight of the rope being at the same time diminished by coiling on the drum. The converse effect—reduction of the leverage and increase in the weight of the rope—takes place in the empty rope. Provided the proper taper be given to the drum, the moment of rotation, and therefore the resistance to be overcome, remains unaltered. Perfect compensation, however, is not attainable by the use of any conical drum, a rotating body of somewhat sinuous contour being necessary for this purpose.

In approximate calculations, the condition of uniform static moments at the beginning and end of the trip must be taken as a basis.

Commencement of the trip, empty cage at bank.

The unwinding rope, weighing  $G$ , and loaded with  $q + F$ , acts on the radius  $r$ ; the rope of the empty cage acts on the radius  $R$ . Hence the initial moment =  $(q + F + G)r - FR$ .

End of trip, full cage at bank.

Empty cage  $F$  and weight of rope  $G$  on radius  $r$ , loaded cage  $q + F$  on radius  $R$  (Fig. 63).

Hence the final moment =  $(q + F)R - (F + G)r$ .

On posing these two moments as equal, we have:—

$$(q + F + G)r - F \times R = (q + F)R - (F + G)r,$$

whence

$$R = r \left( 1 + \frac{2G}{q + 2F} \right),$$

$r$  is selected in accordance with the rope diameter, and  $R$  is determined from the foregoing equation; the mean radius  $\varrho$

$= \frac{R + r}{2}$ , and the depth,  $H$ , of shaft furnish the number of coils

$Z = \frac{H}{2\varrho\pi}$ . Let  $b$  be the breadth of the drum and  $e$  the distance

between two coils of the rope, both measured parallel to the axis of the drum, then  $b = Ze$ . To take up the extra coils the drum is widened as a cylinder at the smaller end. In the case of deep shafts the rope diameter is large, and therefore also the values  $r$  and  $R$ ; the drums have to be very broad, overlapping of the coils

being impracticable, and hence this method of compensation is only suitable for medium depths (1400-2000 ft.). For greater depths it is necessary, in order to obtain shorter and lighter axles, to mount the drums separately, and couple them by cog gear or coupling-rods, as is done with the driving wheels of locomotives. The defect of the tapered drum system is the variable winding velocity under constant engine speed.

For the same reason, the mean winding velocity is smaller for any maximum velocity than is the case with cylindrical drums.

$R$  is often assumed as smaller than would result from the above equation, partial compensation being then accepted as satisfactory. If the pitch of the cone, relative to the axis, exceed  $30^\circ$ , the coils of the rope no longer lay evenly side by side in the spiral

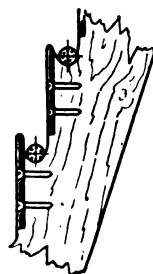


FIG. 64a.



FIG. 64b.

groove on the drum casing, but the correct laying of the rope must be secured by the provision of partition walls. These drums are termed spiral drums, different forms of which are shown in Figs. 64a and 64b.

In other respects tapered drums differ but slightly from those of cylindrical form.

**Flanged Pulleys.**—These are used instead of drums for flat ropes. They consist of a small core (Fig. 65) bounded by two wheels or flanges, between which the separate coils of the flat rope are wound one on the other. Hence the leverage of rope tension increases on the ascending rope, whilst the rope on the descending empty cage unwinds from a core of progressively diminishing diameter.

For the condition of equal moments at the beginning and end

of the trip the equation  $R = r \left( 1 + \frac{2G}{q + 2F} \right)$  again applies; moreover, the thickness of the rope paid out and wound up is the same, and therefore  $R^2 \pi - r^2 \pi = Hd$  ( $H$  representing the depth of the shaft and  $d$  the thickness of the rope).

Assuming  $1 + \frac{2G}{q + 2F} = A$ , and therefore  $R = Ar$ , we have

$$r^2 A^2 \pi - r^2 \pi = Hd, \text{ and } r = \sqrt{\frac{Hd}{\pi(A^2 - 1)}}.$$

If, from this equation,  $r$  works out smaller than appears desirable in view of the thickness of the rope, one must be content with partial compensation, increasing the value of  $r$  and determining  $R$  from the equation  $R^2 \pi - r^2 \pi = Hd$ .

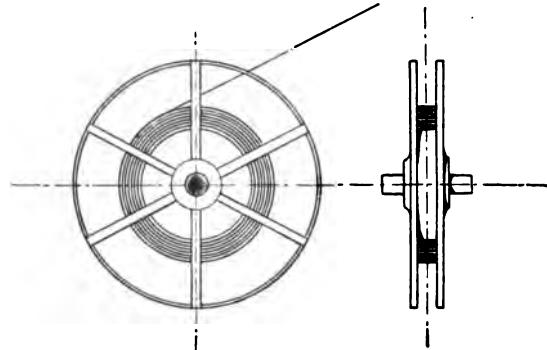


FIG. 65.

A considerable alteration in the resistance during winding occurs in the case of tapered drums and flanged pulleys with partial compensation; but, at all events, it remains of positive value, and there is therefore no need to apply the brakes or reverse the steam admission during the second half of the trip.

Fig. 66 shows a flanged pulley, with a core divided into four sections, to which are bolted wooden spokes forming wheels or flanges that diverge somewhat at the rims, in order to secure a better guiding of the rope. The rims consist of cast-iron segments. If the wooden spokes be replaced with profile iron, it is advisable, in order to protect the rope, to provide an inner lining of wood, or flat bars with rounded edges. In contradistinction to tapered drums, flanged pulleys are very unsuitable for taper ropes, the

outer windings of the diminished rope leaving too much play

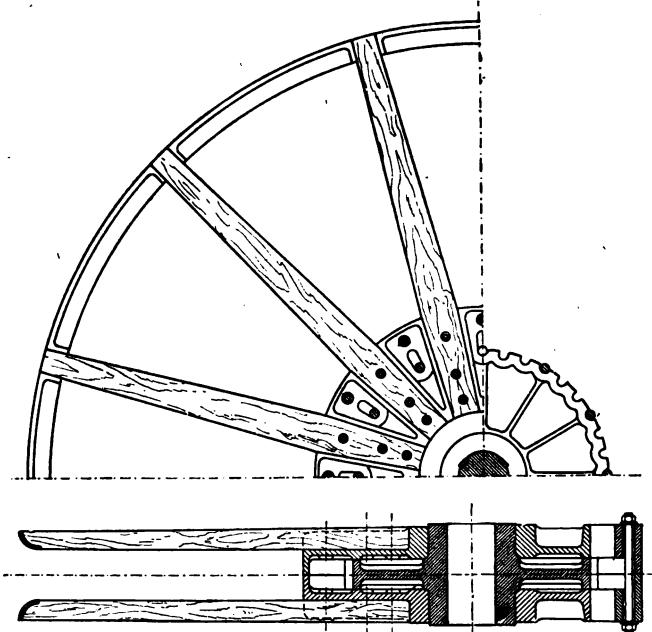


FIG. 66.

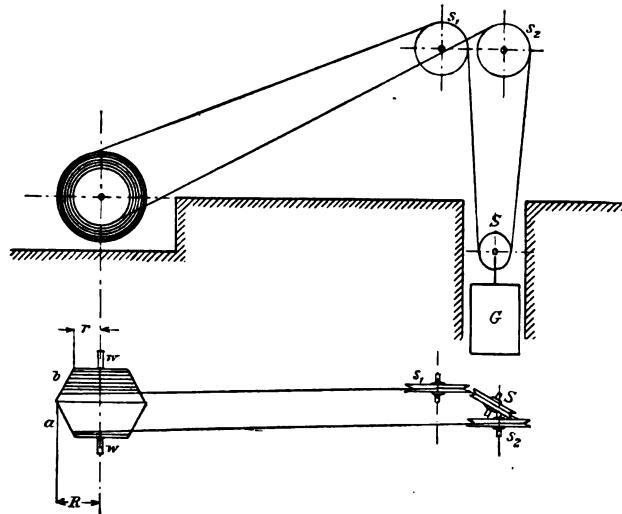


FIG. 67.

between the wheels or flanges. The advantages of flat ropes—

great flexibility and little tendency to twist—are a point in **favour** of flanged pulleys, and the latter can be placed in close proximity to the head pulleys, because the path of the rope remains constant. On the other hand, the strain on flat rope is very unfavourable, the inner coils being strongly compressed by the overlying ones, the life is shorter, and the load per unit of sectional area must be fixed at a low figure from the commencement. In the case of **very** deep shafts one must be content with partial compensation, the calculation furnishing, for the diameter of the core, figures that seem inadmissible, having regard to the flexion of the rope. Now that the comparatively light, cylindrical or taper ropes of patent crucible cast-steel, with high tensile strength, are almost exclusively used, and the construction of properly controllable engines, economical in working, and with variable expansion, has become possible, flanged pulleys are disappearing.

Compensating by means of weights is a plan devoid of the necessary simplicity, and moreover is costly to instal, so that only one example need be given, namely, that of Gerhard, illustrated in Fig. 67. The shaft, *w*, which carries two tapered drums, is coupled direct to the driving shaft. One rope passes from *b* over *s*<sub>1</sub>, *S* and *s*<sub>2</sub>, back to *a*, and suspended from *S* is a heavy weight, *G* (consisting of, *e.g.*, an old boiler filled with pieces of cast-iron), which moves in a shallow supplementary shaft. At the beginning of the cage trip, more rope unwinds from *b* than is taken up by *a*, and therefore the weight descends; in the second half of the trip, *a* coils up more rope than is paid out by *b*, and the weight, *G*, is therefore lifted. At the start the moment  $RG - rG$  assists the movement, whilst towards the end an equal moment exerts a retarding action.

#### *Brakes.*

Every engine must be fitted with reliable appliances for retarding the velocity of winding, promptly checking the motion, and arresting the cage in any desired position. This appliance comes into action: towards the end of the upward trip; in case of accident; when the shaft or piping is being inspected or repaired, etc.; and as soon as the weight of the descending cage preponder-

ates. Such a condition may arise when the miners are being brought up in the cage, pit timbers are being lowered, etc.; and also, in deep shafts, owing to the surplus weight of the rope (during the second half of the trip). The engine could be checked by reversing the admission of steam, but this would not suffice to retain the cage firmly in any desired position, and, moreover, control over the winding drum would be lost in the event of breakage of any part of the engine between the drum shaft and the piston. Hence the necessity for providing brakes, usually two in number, one an emergency brake, acting quickly and energetically in case of accident, whilst the ordinary brake is of lighter construction. In the case of double-cylinder engines, under proper control, the second brake may be dispensed with. Two kinds of brake are used: band brakes and block or cheek brakes. The brake wheel can be advantageously attached direct to the winding drum; but in some cases special brake pulleys are provided, especially with flanged pulleys, or the crank disc is utilised in the case of small winches.

**Cheek Brakes.**—The simplest form of this class of brake, as used for holding the loose drum, is shown in Fig. 68, the wooden brake cheeks, or blocks, being forced tightly against the rim of the drum by means of the hand wheel, screw spindle and brake lever. The friction  $fD$  produced by the normal pressure  $D$  checks the movement of the shaft.

The brake cheeks are let into and bolted to the lever; when greater force is in question, the cheeks are held in place by suitable iron plates, or bedded in a special cast-iron box. The wood should be cut across the grain so that the ends of the fibres come in contact with the drum rim. The brake lever is made of a heavy beam of timber, or a profile iron girder. The section of the brake rim is shown in Figs. 60 and 61 (Plates III. and IV.). Fig. 69 represents a brake for large engines, the double cheeks exerting a powerful retarding force and obviating one-sided pressure on the drum shaft. The diverging levers tend to throw the brake off automatically. As is shown in Fig. 61, such brakes often act on two rims on the inner side of the drum.

*Calculation for Cheek Brakes.*—For the emergency brake, which

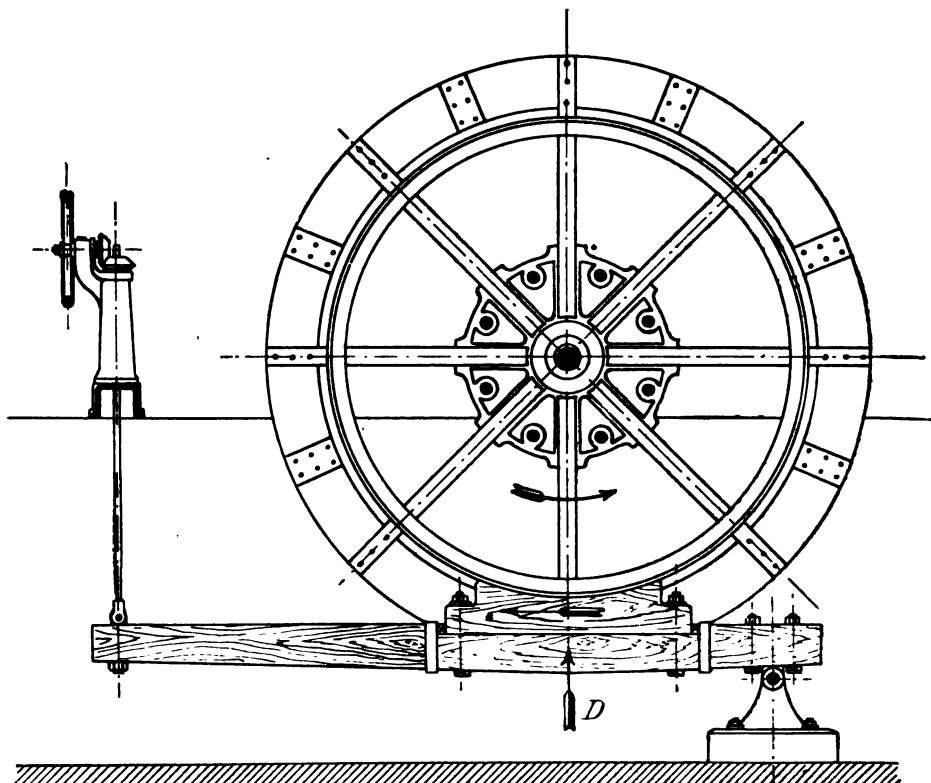


FIG. 68.

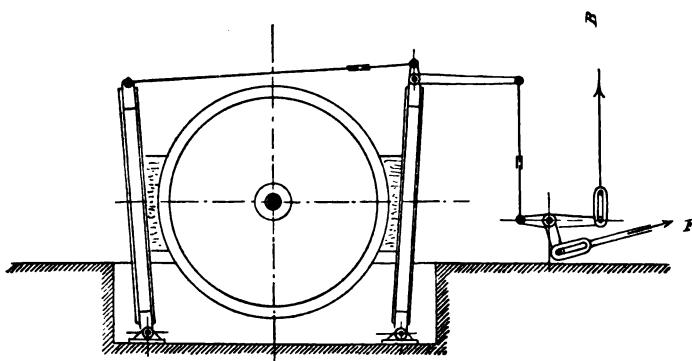


FIG. 69. (Note.—B = to brake piston; F = to hand or foot brake.)

must be capable of supporting the second cage in the event of the

winding rope breaking, and also be able to quickly stop the engine when danger or overwinding arises, the equation

$$P = 1.5 (q + F + G) \frac{R}{r}$$

may be set out, wherein  $R$  is the radius of the winding drum,  $r$  the radius of the brake rim,  $q$  the load to be raised,  $F$  the weight of the cage, and  $G$  the weight of the rope.

For flanged pulleys and tapered drums, the same value may be taken—loaded cage at the pit eye—or else  $P = 1.5 (q + F) \frac{R_1}{r}$ , in which  $R_1$  represents the maximum radius of the coils.

For ordinary brakes it is sufficient to assume the retardive tangential resistance as  $P = (q + G) \frac{R}{r}$ . From what has been already stated,  $P$  is  $= fD$ , wherein  $f$  is the coefficient of friction (0.5 for wood on iron), and  $D$  the normal pressure of the brake beam against the rim.

When a safety appliance for the prevention of overwinding is present (*q.v.*), the brake must be capable of stopping the engine and cage within a certain definite distance,  $s$ , usually 30-50 yds. The braking effect exerted on the rim of the drum must then be equal to  $s (q + F + G)$ , increased by the *vis viva* of all the moving parts.

**Band Brakes.**—In this form of brake a band of hoop-iron or steel surrounds a portion of the brake rim, and can be tightened by means of a bell-crank lever. The brake is often lined with wood, to increase the friction and protect the iron band; and, to compensate for wear and tear, at least one end of the band must be mounted so as to allow of adjustment. Since the normal position of the brake is "off," the lever must be counteracted by a counterpoise or spring.

*Calculation for Band Brakes* (Fig. 70).—If  $S$  and  $S_1$  represent the tension in the end portions of a band brake, surrounding the arc  $a$  of a pulley with the radius  $R$ , then for the direction of rotation  $i$  we obtain the relation:  $S = S_1 e^{fa}$ , in which  $e$  is the basis of the natural logarithm,  $f$  the coefficient of friction (0.5 for wood on iron,

and  $0.12-0.2$  for iron on iron). The tangential resistance,  $P$ , opposing movement is  $S - S_1$ . This furnishes:  $S_1 = \frac{P}{e^{\alpha} - 1}$ ; for  $\alpha = 0.8\pi$  and  $f = 0.5$ ,  $e^{\alpha} = 3.513$ . Hence,  $S_1 = 0.4 P$ , and  $S_1 = 1.4 P$ . It is therefore sufficient to produce in the left-hand portion of the band a tension of  $0.4 P$ . At the next trip of the cages the direction of rotation is changed, the smaller tension  $S_1$  being shifted to the right end of the band, whilst a force of  $1.4 P$  must be applied to the left end in order to produce the same effect. Assuming the maximum pressure exerted by the foot at  $t$  to be 70 units of weight, then :  $tc \ 70 = cb \ S$ ; the leverage ratio  $\frac{tc}{bc}$  must therefore be  $= \frac{S}{70} = 0.02 P$ .

If, however, when the direction of motion is 1, the machinist

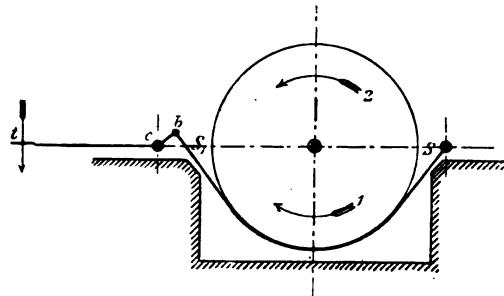


FIG. 70.

erroneously applies a pressure of 70 weight units to the lever, then the tension in the right extremity of the brake band increases to about 5 P, and consequently provision must be made for the band and its fastenings to stand this tension.

The braking effect increases with the dimensions of the arc enclosed by the brake band. In Fig. 70a,  $\alpha = 1.6\pi$ , hence  $e^{\alpha} = 12.35$ ,  $S_1$  merely  $= 0.088 P$ , and  $S = 1.088 P$ . The leverage ratio becomes smaller, but the tension at the end  $c$  may increase to 14 P. A far more satisfactory arrangement, therefore, is that shown in Fig. 71, representing a double brake, in which each of the bands has only to produce one-half the resistance: *i.e.*,  $S_1 = 0.2 P$ , and  $S = 0.7 P$ . The bands are usually drawn back from the rim by means of weights or springs.

The brake lever may be moved by hand, with the foot, by

weights or springs, steam, compressed air, electro-magnets, etc. To enable the brakes to be kept "on" for some considerable time, a locking device must be provided when the levers are worked by hand or the foot. Hand wheels, though sometimes used for applying the brakes, are too slow for emergencies. To produce a powerful effect with hand or foot brakes, a high ratio of leverage is

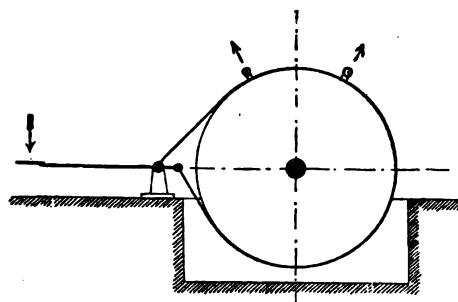


FIG. 70a.

necessary, and consequently the levers have to be made very long, even when the blocks are set within a fraction of an inch of the rim.

**Steam Brakes.**—Steam brakes are powerful and quick in acting, but the suddenness with which they act at full force is injurious to the machine. Furthermore, since steam brakes could not be applied in the event of the main steam pipe bursting, it seems

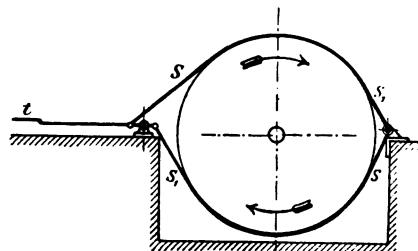


FIG. 71.

advisable to employ a separate supply pipe for conveying steam to the brake cylinder, or else to arrange a heavy weight, which is released in the event of a breakage of the steam pipes, and acts with a high leverage against the brake lever. The cylinder and valve chest of a steam brake are illustrated in Fig. 72, the position of the piston corresponding to "brakes off". Both sides of the

cylinder are in communication with the live steam. On drawing the valve slide towards the left, the steam on the right side enters the exhaust, the piston is driven forward and applies the brake. This uninterrupted contact between the piston and the live steam prevents the disturbances arising from condensation on the admission of steam in the ordinary way. Provision is also usually made

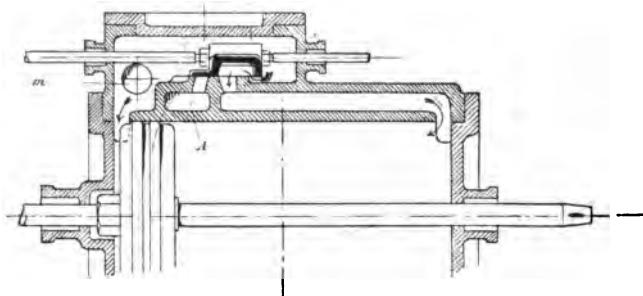


FIG. 72. (*Note.*—*m* = admission ; *A* = exhaust.)

for setting on the steam brake by hand (see Fig. 69). The vacuum and pneumatic brakes, that have proved so useful in railway work, are now also often met with in winding engines. They enable the checking to be effected gently, with the desired power, and obviate the dangers that might arise from the deposition of water in the cylinders of steam brakes.

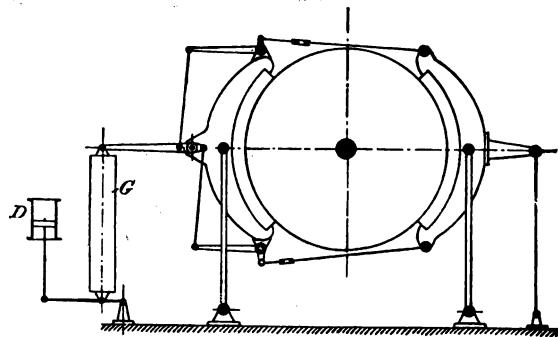


FIG. 73.

**Loaded Brakes** are also met with, heavy weights, acting at a high leverage against the brake cheeks, being employed. To set the brakes off, the weights are lifted by steam or compressed air. An American brake of this class is represented in Fig. 73, *G* being the weight and *D* the steam cylinder for raising same.

**Braking by Reversing the Engine.**—If the reversing-lever be turned over while the engine is running, the latter acts as a consumer instead of a producer of power, inasmuch as it draws in air through the exhaust and forces it into the boiler. According to Audemar, the defects attending this practice (overheating the cylinder by the high temperature resulting from the compression of the air, and the attainment of a dangerously high pressure in the boiler) can be obviated by placing the exhaust in communication with a large vessel in which the steam and hot condensed water collect. When the engine is reversed, a throttle or non-return valve enables the free sectional area of the pipe between the cylinder and the said vessel to be reduced to very small dimensions; and, in this event, attenuated steam, instead of air, is returned to the cylinder.

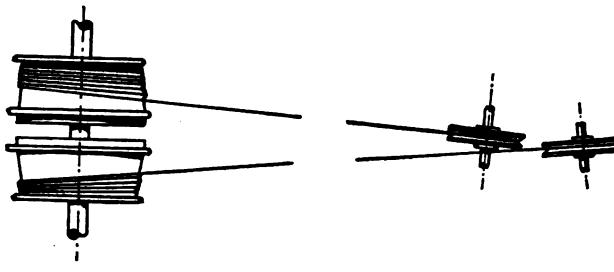
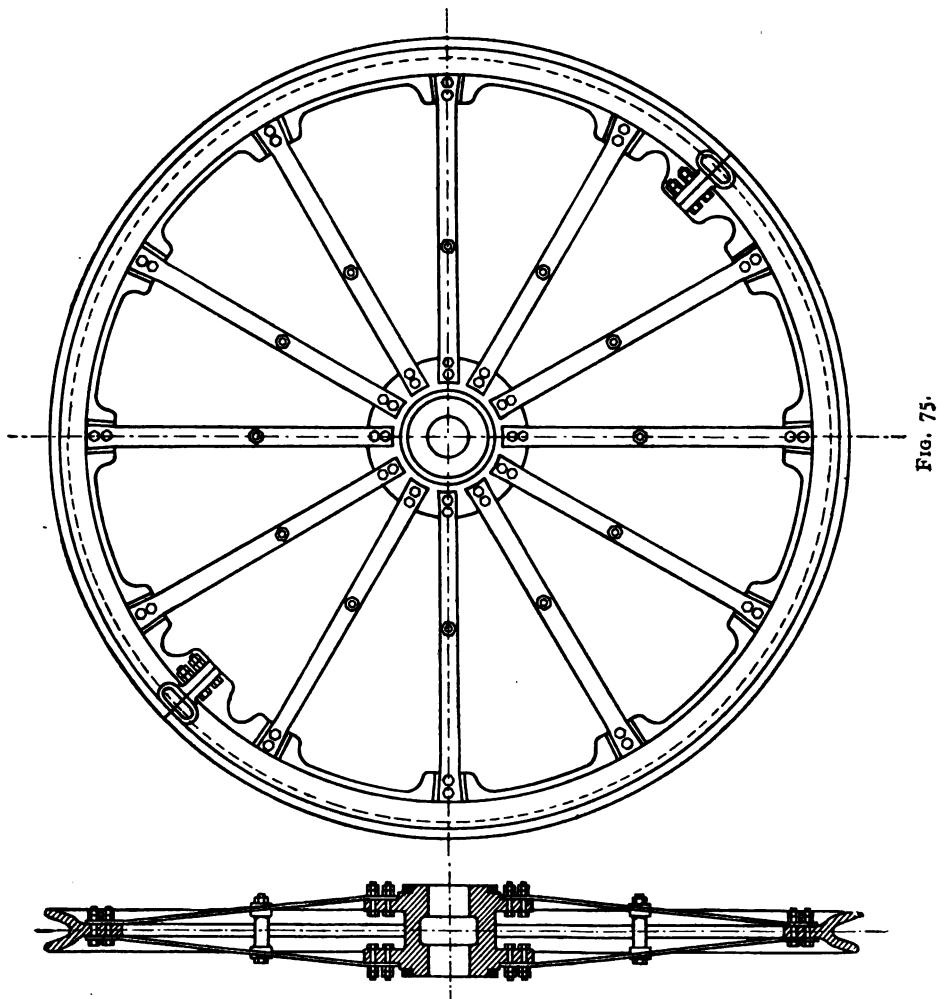


FIG. 74.

#### *Head Pulleys.*

As shown in Fig. 46 (Plate II.), the rope passes from the drum over a pulley at a higher level. These pulleys should occupy a position central to the plane of the corresponding drums, and their shafts be mounted parallel to those of the latter. It is seldom that the arrangement represented in Fig. 74 is resorted to in order to ensure a better coiling of the rope by making the drum faces slightly conical. To reduce the risk of the cage coming in contact with the head pulley in the event of overwinding, the latter must be mounted at a sufficient altitude above bank, the distances averaging 10-40 yds., according to the working velocity, diameter of the drums, and height of the cages. The distance between the drum and the head pulley is usually 25-50 times the breadth of the drum, and should

be sufficiently great to ensure the turns of the rope lying uniformly side by side. If the distance be too small, the rope is subjected to injurious friction against the pulley flange in consequence of the high deviation from the central line; whilst if too far away, an in-



convenient swinging of the rope is produced. In the case of flanged winding pulleys, the distance may be reduced to any convenient extent.

The diameter of head pulleys depends on the thickness of winding rope used. The pulley shaft should be as long as possible,

and the supports firm and well stayed, to resist the lateral strains produced by the rope. The shafts and journals must be selected in accordance with the tension in the ascending and descending ropes, and the weight of the pulleys themselves. The rope tension to be considered is the breaking strain of same.

*Construction.*—Small pulleys cast in one piece, divided hub, spokes of oval, X or H section; large pulleys in two or more sections, the spokes being often of wrought-iron (round bars, gas-pipe, flat rods, U-iron, etc.). Round spokes are cast into the hub and rim, flat or profile spokes bolted as shown in Fig. 75. The groove in

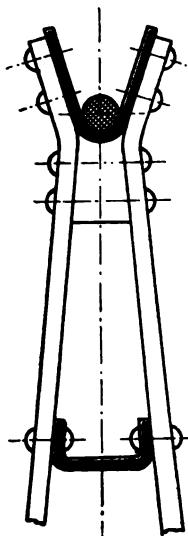


FIG. 76.

the rim should be deep and V-shaped, the base being of thick metal to allow for wear. The amount of wear should be ascertained from time to time, by means of templates, or by holes drilled through the rim for that purpose. The groove is sometimes lined with wood, leather, rubber, hempen rope, etc., but, as these materials will not stand much wear, they are not often used now.

Fig. 76 represents a pulley rim of wrought-iron exclusively.

The pulleys should be as light as possible, so that they may readily adapt themselves to alterations in the speed of winding, and not cause any attrition of the rope in the groove as a result of their

inertia. They should be accurately balanced and run perfectly true. Hence, pulleys made in one piece should be turned true after they are keyed on the shaft, those in sections being merely clamped tightly on the shaft by means of the screw bolts on the two halves of the hub.

At one time towers of masonry were used to support the head pulleys, but have now been almost entirely displaced by iron head frames, timber being used only for small shafts or temporary purposes. The lower part of the pulley should be provided with a protecting case, to prevent accident in the event of a breakage of the pulley shaft or of the pulley itself.

The head frame should also project somewhat above the bearings, to enable a crane or crab to be erected for the purpose of lifting the pulley out of the bearings, etc.

#### *Installing the Winding Engine.*

Winding engines may be vertical or horizontal, single- or double-cylinder engines, with or without intermediate gear, and with either a common driving shaft for the drums, or with two separate shafts for the latter. Under ordinary circumstances at the present time, the usual form of engine is the direct-action, horizontal, double-cylinder (or compound) type, with cranks set at an angle of 90°. For low-speed work (underground haulage, etc.), single-cylinder engines, or better, double-cylinder engines, with intermediate gear are chosen.

In the present state of constructive engineering, it is possible to make toothed gearing that will work reliably and noiselessly, so that engines with intermediate gear are again coming into the field for winding purposes.

Large vertical engines are rarely met with on the Continent, and separate driving shafts for the drums (Fig. 77) are only required under special local conditions. One advantage of the arrangement shown is that both ropes run overhead from the drums, thus obviating the unfavourable doubling bending of one and the same rope.

Separate drum shafts are also useful with drums of great breadth (p. 56), and where the head pulleys are set close together, since the

deviation from the central plane, otherwise suffered by the rope, is hereby diminished. The constructive details are based on the same fundamental principles as with engines for driving shafting, though greater importance attaches to ease of supervision and the accessibility of all parts. These conditions are secured by high foundations, placing the steam pipes, etc., in well-lighted passageways, placing the levers for starting, reversing and braking the engine at the driver's stand, which should preferably be in such a position as to command a view of the pit bank. The main starting valve

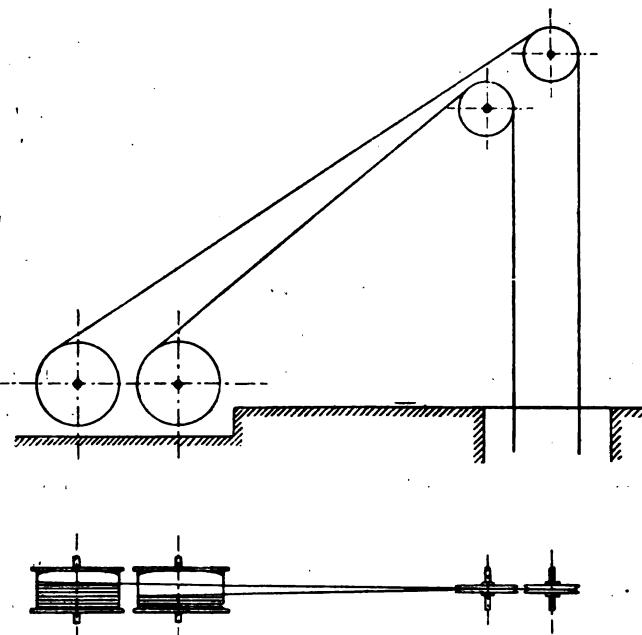


FIG. 77.

should open and close with a single turn, the valve stem being fitted, for this purpose, with a cross bar, the ends of which are guided in a spiral line.

Furthermore, to compel the driver to work with expansion, the starting valve is occasionally done away with, as well as the notches on the quadrant of the valve-lever.

*Compound Engines.*—These engines produce an economy of 10-20 per cent. in the consumption of steam, a result due, not merely to the acknowledged advantages of the compounding, but

also to the compulsory expansion of steam in the low-pressure cylinder, independently of the working of the valve-lever.

The good effect of compounding is largely reduced, however, by long pauses in working and by considerable fluctuations in the resistance to be overcome ; and for deep shafts, without rope compensation, equally favourable results are obtained with double-cylinder engines. Compound engines are less easily controlled, and, on starting, fresh steam must be admitted into the low-pressure cylinder, whilst the waste steam from the small cylinder is conducted to the exhaust. Unless this plan be adopted, it takes a longer time to get up full speed with a compound engine than with a double-cylinder engine of the same horse-power. For specially heavy winding, tandem double-cylinder engines are now constructed.

Condensating is to be recommended where fuel is dear, and the feed water is bad, otherwise necessitating expensive purifying plant, and where there is available at the same time a plentiful supply of water for the condensers.

Spray condensers are the only form coming under consideration for separate engines, but connection with a central condensing plant is preferable.

To prevent the drawing of water into the cylinders, the condensed water may be removed through a barometer tube, or non-return valves are provided in the steam pipes ; change valves may also be provided, to enable the engine to work without condensation.

The steam consumption in winding engines is a very variable quantity. In general it may be assumed that 20-65 lb. of feed water are required per hour for each ton raised a height of 330 ft., so that when, for example, 50 tons an hour are raised from 1,000 ft.,  $1\frac{1}{2}$ - $4\frac{1}{2}$  tons of feed water will be needed in the same time.

#### *Special Arrangements.*

1. **Single-cage Winding.**—Where there is only a single cage, the winding drum is coupled to the non-reversing engine during

the upward trip, the empty cage being lowered by braking the disconnected drums.

**2. Koepe Winding Pulley.**—The Koepe system of winding (Fig. 78) consists of a pulley, fitted with a single groove and keyed on to the engine shaft, the rope being simply slung round this pulley, and the two ends led up round the head pulleys to the pit. The rope is moved by the friction of the driving pulley, on which account the pulley groove should be lined with leather,

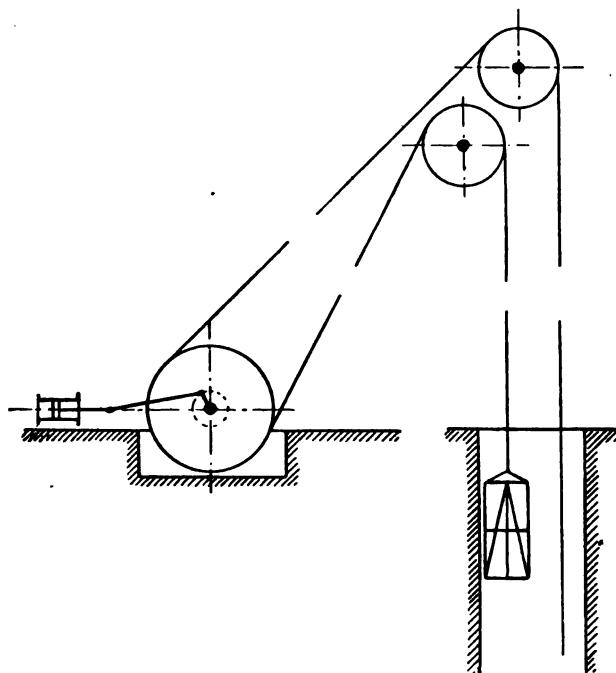


FIG. 78.

oak or white beech wood, and the rope should not be greased. Valuable adjuncts to this method of winding are the use of compensating tail ropes, and Baumann's rope clamps, which enable the cage to be adjusted to different levels for winding. Since overwinding seems impossible, the head pulleys may be situated close above the pit mouth; for when the descending cage is resting on the bottom keps, the tension on that part of the rope is so small, and hence the friction in the pulley groove is so low, that the cage at bank cannot be raised any further, the rope simply

skidding in the groove. The disadvantage of the system is that, should the rope break, both cages will be precipitated down the shaft, and that if one winding compartment is obstructed, the other cannot be used.

In some cases catch ropes have been provided to take up the load of the cage on the breaking of the winding rope, but this causes the system to lose its feature of being cheaper than winding drums.

**3. Steam Winches.**—This name is applied to small, compact and easily portable winding and hauling engines. The larger winches, such as those constructed by Bolsano, Tedesco & Co., of Schlan (Fig. 79), do not differ greatly from double-cylinder engines with intermediate gear. For small powers, however, vertical engines with oscillating cylinders, internal reversing gear, or change gear for reversing the rotation of the drums, are frequently used.

Fig. 80 shows a pulley winch, and Fig. 81 a horizontal-pulley winch (E. Wolff, Essen), specially adapted for winding from winzes. The position and mounting of the pulley are shown in the Fig. ; the power is applied by oscillating cylinders, set at an angle of  $90^\circ$ .

#### *Winding Engine Calculations.*

Let  $F$  be taken to indicate the weight of the cage,  $G$  that of the rope, and  $q$  the load to be raised. Since the two cages balance, the initial resistance to motion is  $= q + G$ , together with the supplementary resistances, reduced to the periphery of the winding drum, say 4 per cent. of the total load, which gives us

$$W_1 = q + G + 0.04(q + G + 2F).$$

At the end of the up trip, before the descending cage is on the keps, we have

$$W_2 = q - G + 0.04(q + G + 2F) = W_1 - 2G,$$

and after

$$W_3 = q + F - G + 0.04(q + G + F).$$

In shallow pits  $W_3$  is the most important value,  $W_1$  where the depth is considerable. ( $W_3$  does not come into consideration when keps are not used and slack rope is entirely avoided.) The average

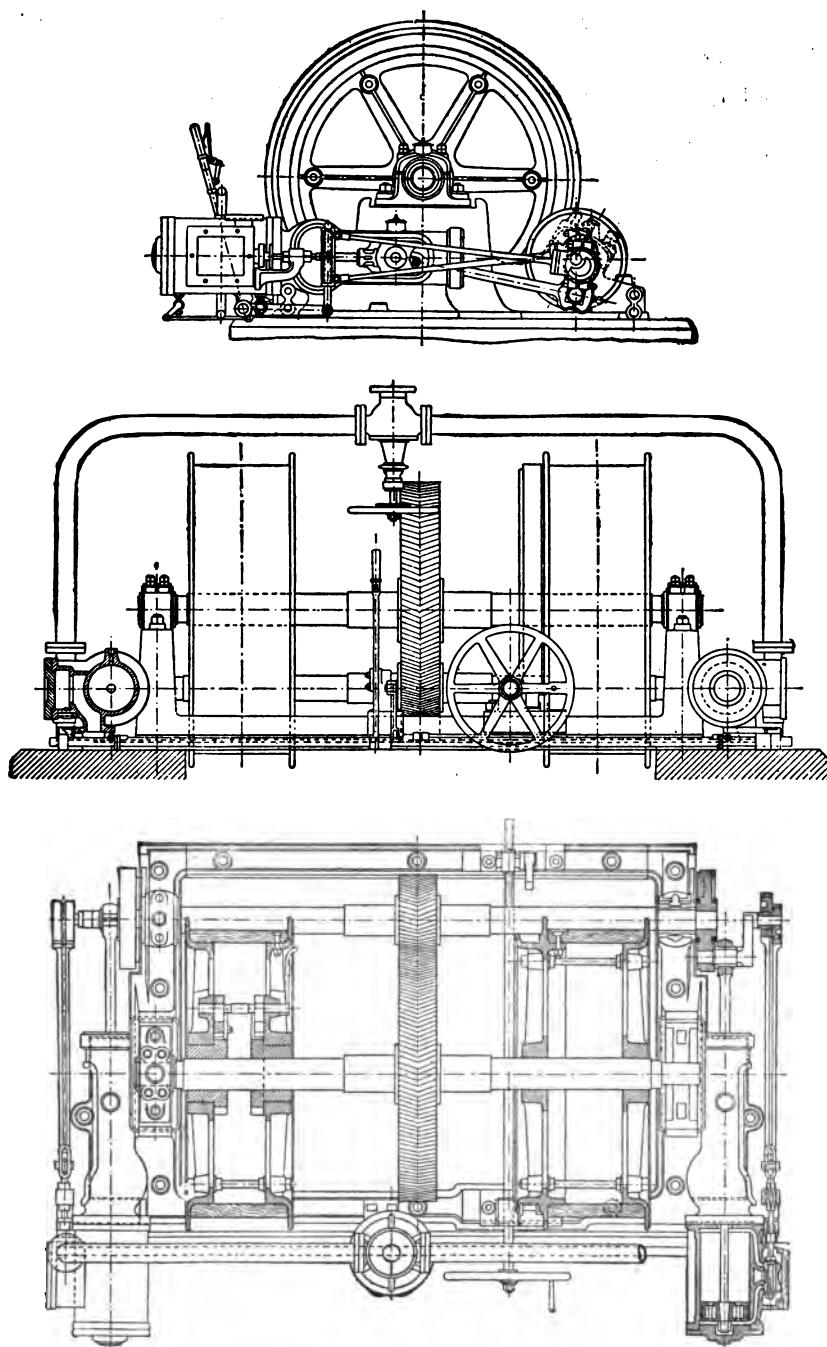


FIG. 79.

cage velocity is 33.43 ft., but the maximum lies much higher. The maximum permitted for winding coal (50-65 ft.) and men (about 13 ft.) is usually fixed by legislative enactments.

For any given velocity,  $v$ , the useful effect  $N = \frac{Wv}{75}$  h.p., and

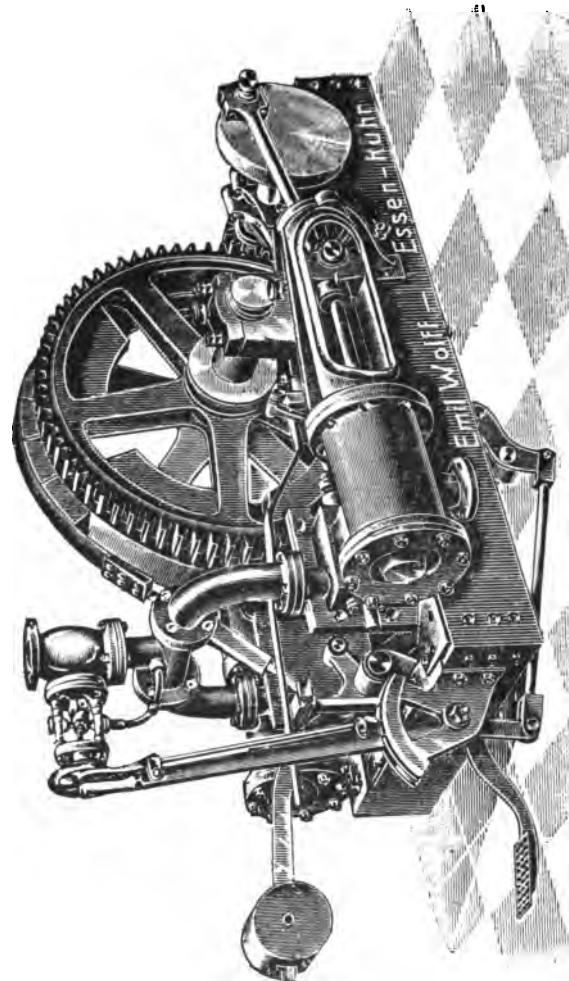


FIG. 80.

from these data the particulars of the engine can be calculated, assuming a certain steam pressure in the boilers, a given cut-off, and an efficiency of 60-70 per cent. In such case the engine will work under full load with full pressure or small expansion, but

under the lowest duty  $\frac{W_2 v}{75}$  with high expansion. The medium expansion corresponds (Hrabak) to the economically most advantageous cut-off. In the case of double-cylinder or compound engines, an additional calculation is required to ascertain whether, in the event of the one crank being in an unfavourable position (at the dead point) the engine is still able to lift or hold the load with one

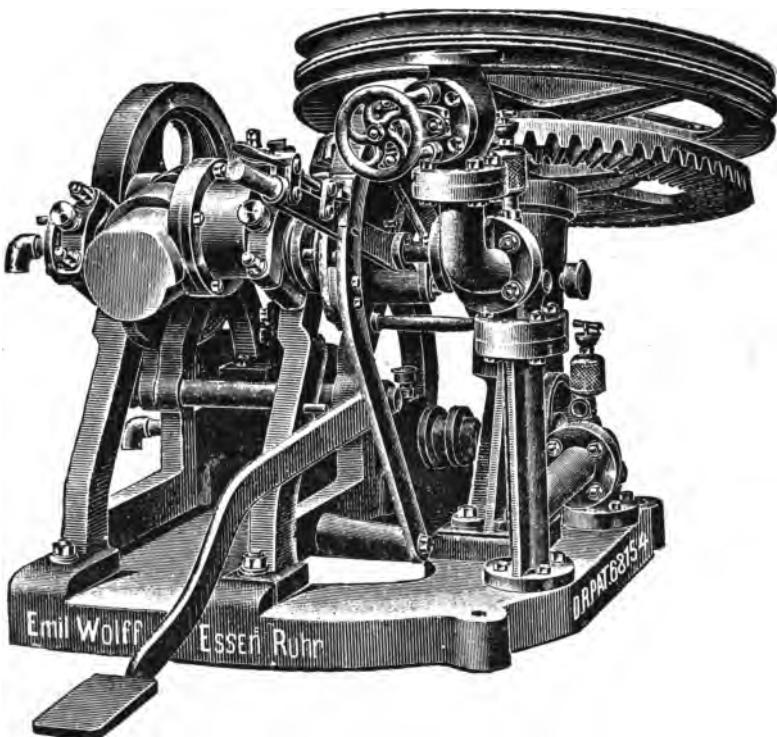


FIG. 81.

cylinder. Another requirement, namely, that the engine shall, in the event of the rope breaking, be capable of raising the loaded cage at uniform velocity from the bottom of the shaft, is really too stringent. To facilitate starting, the valve gear of double-cylinder engines should be so arranged as to permit of the admission of a full head of steam; and in compound engines a direct inlet for fresh steam into the low-pressure cylinder must be provided.

Where the winding traffic is busy, the duration per trip must

be determined from the amount to be raised in the day ; also the necessary mean velocity, and the requisite acceleration when it is desired to attain the highest permitted velocity at 30-50 per cent. of the distance traversed. A calculation is then made as to whether the tangential pressure on the crank pins is sufficient to impart this acceleration to all the moving parts.

For engines with tapered drums or flanged pulleys, the approximate calculation is very similar ; only the resistances must be referred to a mean radius  $\rho = \frac{R + r}{2}$ , and the corresponding mean velocity inserted :—

$$W_1 \text{ becomes } = \frac{r(G + F + g) - RF}{\rho},$$

$$W_2 \text{ becomes } = \frac{R(g + F) - r(F + G)}{\rho},$$

$$\text{and } W_3 \text{ becomes } = \frac{R(g + F) - Gr}{\rho}.$$

Moreover, it is advisable to determine the resistances for a few of the intermediate positions, and to calculate whether starting from intermediate levels necessitates a greater output of power. Of course the highest values so obtained must be kept in view.

#### • *Signals and Safety Appliances.*

The engine driver must be advised when the cages are ready to start, and receive a signal from the pit eye or cage, besides being aware at all times of the exact position of the cages in the shaft.

Signalling is effected by means of a bell or hammer in the engine-room. A cord, or better still, a thin wire, runs down the shaft to the pit eye. Speaking tubes and pipes fitted with whistles are insufficiently reliable ; but iron rods, struck by a hammer, will carry sound well, and may be used for signalling from the cage. Latterly the use of electric signals has made headway ; and by this means signals can be sent also from the travelling cage to the engine-room. The winding rope can be utilised as one conductor, the other consisting of a copper wire, extending all down the shaft outside the cage, and placed in electrical communication with the latter by a contact piece.

**Depth Indicators.**—These are appliances for indicating the cage trip on a reduced scale, and thus showing the momentary position of the cage. In one form, motion is transmitted from the drum shaft or valve shaft to two screw spindles carrying travelling nuts attached to a pointer. In order to ensure the proper setting of the pointer when the rope is altered, it is advisable that only one of the spindles should be actuated by the engine shaft, the other being driven from the hub of the detachable drum. The depth indicator, or a separate similar appliance, can also actuate a bell as soon as the cage is within two or three turns of the rope from bank.

A painted mark on the drum indicates the exact position at which the engine must be stopped.

**Tachometers.**—While on the one hand the permissible maximum velocity must not be exceeded, it is essential on the other to wind as quickly as possible; consequently some instrument for indicating the velocity of the cage is indispensable. Most tachometers greatly resemble governors in construction, and act on a pointer, usually a pencil which traces the curve of velocity on a revolving paper drum.

Another form of tachometer is a small centrifugal fan, which produces rarefaction of the air in accordance with the speed at which it is run. The rarefaction is measured by a pressure gauge, which indicates the corresponding velocity. Such appliances, however, are dependent on the temperature and barometric pressure of the air.

**Overwinding.**—A frequent source of accident in winding is overwinding, *i.e.*, the cage being raised too high. The means of prevention are: (*a*) releasing the connection between cage and rope, (*b*) clamping the cage between tie guides, and (*c*) automatically applying the brakes or stopping the engine.

(*a*) *Releasing the Rope.*—Fig. 82 shows the appliance devised for this purpose by Haniel & Lueg, in both positions, open and shut. To the bridle chains are attached shears, consisting of three plates, *a*, against which fit, on either side, the plates, *f*, attached to the rope. The accidental release of the rope when slack is prevented by a copper tube, *c*, the same effect being produced, when

the rope is taut, by the form of the recesses at *h*. When overwinding occurs, the shears enter the funnel-shaped catch, *k*, which is

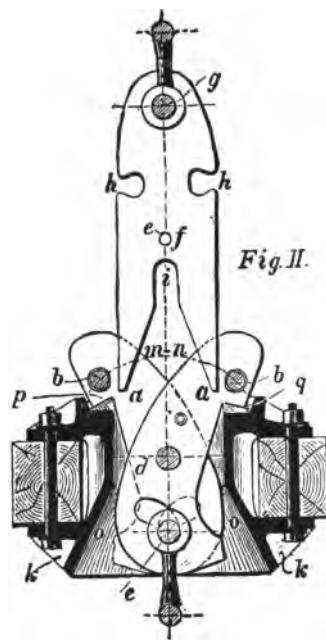
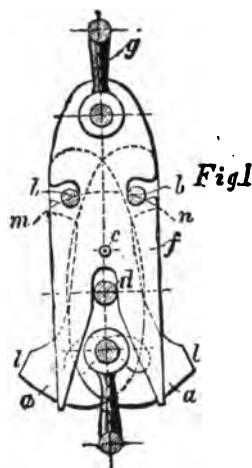


FIG. 82.

situated a little below the head pulley. The connection is broken, the opened shears engage with the steel ring, *g*, and support the cage. As the plates, *f*, are drawn over the head pulley and up to

the drum, it is necessary to interpose a strong partition between the path of the rope and the engine. The appliance just described is one of the best of its kind ; but is attended with the disadvantage of requiring careful looking after, owing to the considerable increase in the number of parts in the connection between rope and cage.

(b) *Clamping the Cage in the Guides.*—Between the bank and the head pulley the cage guides are drawn somewhat closer together. This method, however, has little to commend it, since either the guides will be forced apart or the rope break. Of course, suitable supports must be provided to catch the cage.

(c) *Automatically Stopping the Engine.*—In older appliances the admission valve is shut off and the brakes applied as soon as the cage, and consequently the nut on the depth indicator, rises above a certain height. The nut lifts the pawl restraining a weight, which thereupon falls and effects the stopping of the engine. If the cage passes bank at a moderate speed, this method enables an accident to be prevented, but not when the cage velocity is high. The idea therefore suggests itself of throttling the live steam or the exhaust by means of the ascending nut of the indicator, and thus automatically slowing down the engine before the cage reaches bank. This, however, somewhat interferes with the controllability of the engine at starting, and it therefore seems preferable to prescribe a definite limit of speed at the end of the trip, and to provide for the automatic application of the brakes if that limit be exceeded. At the same time the simultaneous throttling of the steam is often effected ; but it must not be forgotten that, in such event, the driver is prevented from reversing the admission of steam.

Of the numerous appliances devised for this purpose (the Roemer, the Mueller, the Westphal, the Wodrada safety appliance, etc.), only that of Baumann will be described here (Fig. 83).

The spindle of the depth indicator imparts longitudinal motion to the non-rotating nut,  $i$ , whilst the toothed rocker,  $a$ , is turned by a governor, and, as the speed increases, approaches the nose on the nut,  $i$ . If now the speed is not sufficiently reduced as the cage nears bank,  $i$  comes in contact with  $a$ , the lever,  $c$ , is turned,  $e$  is released, and the falling weight,  $f$ , sets on the brake or throttles the

steam. The same applies when, at any moment during the trip, the projecting piece, *d*, of the rocker, *a*, presses against *c*, and thus releases *g*.

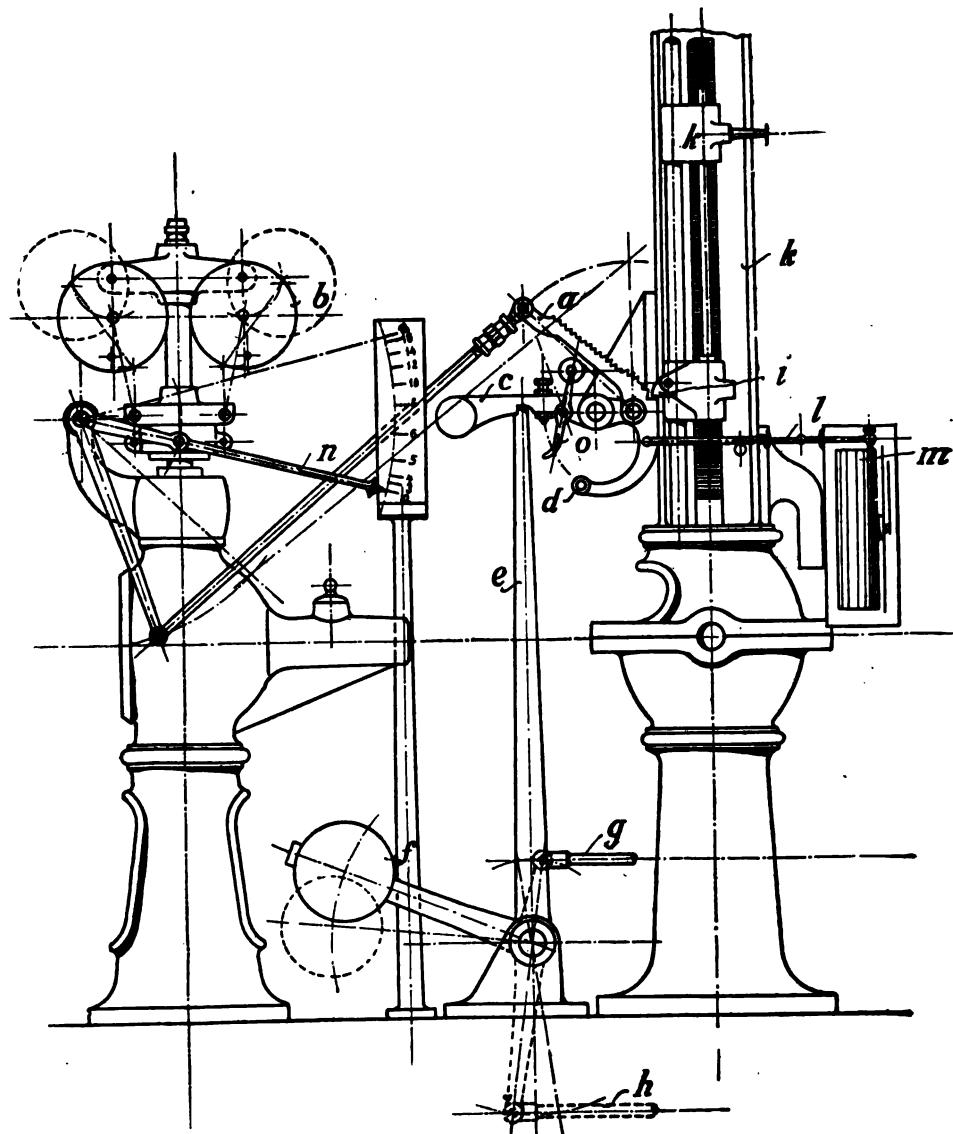


FIG. 83.

For winding the men, in which case the permitted speed is of course much lower, the pivoted lever, *o*, is set in action, thus corre-

spondingly decreasing the distance between *a* and *c*. The governor at the same time serves the purpose of a tachometer, the curves of velocity being recorded by means of the paper drum, *m*.

(b) HYDRAULIC ENGINES.

Water wheels and large turbines are now rarely employed directly, preference being given to utilising the water power for generating electricity, and using the latter as the source of power. On the other hand, hydraulic engines, small turbines and Pelton wheels are still largely used. These may be driven by water specially subjected to pressure, water flowing from a higher level, or finally water from the mains. In the latter contingency especially, the cost both of installation and working is low.

*Hydraulic Engines*

do not differ in principle from steam engines. The admission of water to the cylinder is regulated by plunger valves, slide valves or other forms of valve ; and pistons or plungers are used. The simplest hydraulic motors are fitted with one or two driving cylinders, and work under a full head. Reversing is effected by interchanging the admission and outlet by means of reversing slides or cocks. Of course such motors consume an amount of water equal to the cubical capacity of the cylinder, whether the work to be done be much or little. Hence they work the more economically, and can be constructed the more simply, in proportion as the resistance to be overcome is the less subject to variation ; and consequently hydraulic lifts and winches should always be fitted with good rope compensation. With diminishing resistances, either the shaft must be braked or the water pressure decreased by throttling the admission (or increasing the counter pressure of the waste water). This, however, does not diminish the amount of water consumed. Hydraulic engines may be adapted to fluctuations of load by—

1. Altering the stroke, by adjustable crank pins—a method seldom used, and suitable only for very small engines.
2. Modifying the working surface of the piston, the engine being made with three to twelve pistons, all of which work together

when the load is at its highest, while some of them can be cut out when the work is reduced.

3. Altering the admission. Since water can neither expand nor be compressed, it is insufficient to merely shut off the supply,

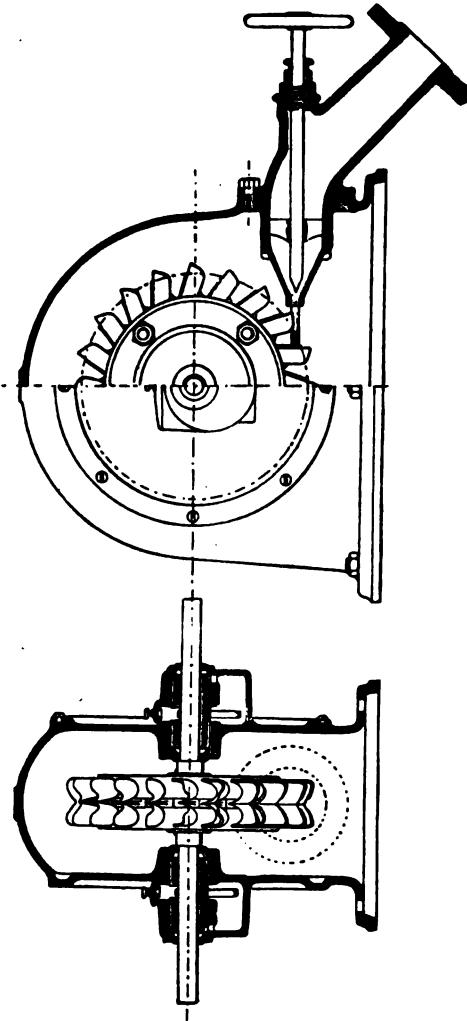


FIG. 84.

since the forward movement of the piston would then lead to the formation of a vacuum in the rear, whilst closing the outlet would result in concussion (water knocks) instead of cushioning in the front end. In order to obviate both evils, one must either—

(a) Take the precaution, after shutting the admission valve, to

admit water under ordinary pressure (*e.g.*, from the waste pipe) into the cylinder; and after shutting the outlet allow the water in the cylinder to be forced back into the feed pipe; or

(b) Provide large air bags above both ends of the cylinder. On shutting off the feed water, the air in the bag at that end of the cylinder will have the same tension as the water, and will expand in proportion as the piston advances. If the valves have been properly set, the air pressure should recede to that of the atmo-

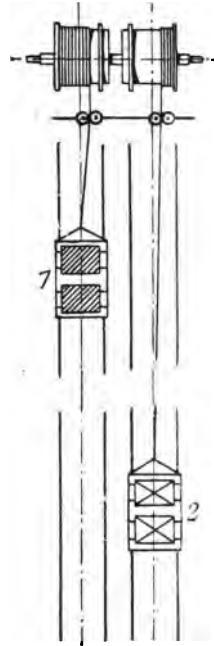


FIG. 87.

sphere by the time the outflow commences. At the close of this stage the air is compressed, and should attain the same pressure as the water by the time the piston has returned to its initial position.

#### *Turbines*

are in many respects superior to hydraulic engines, especially the smaller sizes. Compact construction, convenient handling and high efficiency specially characterise the Pelton wheel (Fig. 84), which can easily be arranged to reverse by mounting two wheels, with paddles set in opposite directions, on the one shaft, and

providing two sets of water nozzles (double motor). Figs. 85 and 86 (Plate V.) illustrate a haulage winch driven by a Pelton wheel.

The regulating spindles for closing the nozzles are here attached to pistons working in small cylinders. Each cylinder is fitted with a cock, which enables water to be admitted above or below the piston, thus closing or opening the nozzle. The cocks of the four nozzles are connected with the valve-lever by coupling rods.

#### *Water Tank Hoists.*

These hoists are seldom used in vertical shafts, though sometimes employed for working vertical and inclined hoists in open-cast ore mines. The trucks are fitted with water tanks, or special trucks filled with water are attached to the ordinary ones. The arrangement is sketched, diagrammatically, in Fig. 87. Here the truck 1, with filled tubs and empty water tanks, is ascending, whilst truck 2, with full water tanks and empty tubs, is going down. The drums are provided with brake rims, since brakes are necessary almost all through the trip, especially when there is no rope compensation. The brakes are preferably automatic, and the velocity is low. The filling and emptying of the water tanks being attended with loss of time, the system is only suitable for small loads.

#### (c) ELECTRIC WINDING ENGINES AND COMPRESSED AIR ENGINES.

*(See Chapter VII.)*

## CHAPTER V.

### WINDING WITHOUT ROPES.

THE undeniable defects of rope winding, especially for great depths, have led to numerous endeavours to raise the load direct, without the intervention of any organ of traction.

In this connection, mention may here be made of Blanchet's "pneumatic" system of winding, and the method proposed by Mähnert.

Blanchet inserts in the shaft a pipe (or, for double winding, two pipes), about 60-80 ins. in diameter, reaching from the lowest pit eye to bank. Into these pipes fit the cages, which are mounted on large pistons with leather packing. The cage is raised by exhausting the air at the top of the pipe, and the down trip is accomplished by gravitation, the rate of fall being regulated by throttling the after-flow of air. By this means the ventilation of the mine is effected at the same time. So far, the system has only been tried once, namely, at the Hottingue shaft, near Epinac.

In the Mahnert system two pipes are built in the shaft, these being filled with water, and connected at the bottom by means of a lock chamber. The load is inserted in an iron vessel, which ascends to the surface in the upcast pipe, whilst the emptied and suitably weighted vessels sink down the intake pipe. This method has not been tried in practice.

## CHAPTER VI.

### HAULAGE IN LEVELS AND INCLINES.

HAULAGE on the level and in inclines is divided into two chief classes :—

#### I. Stationary motors :—

(a) The tub wheels run on permanent tracks.

The motive power is transmitted from the motor to the tubs by means of ropes (rope haulage), or by means of chains (chain haulage).

(b) The track for the tubs is a freely suspended wire cable (wire-rope tramways).

#### II. Locomotive haulage.

### I. HAULAGE BY STATIONARY MOTORS.

#### *Rope Haulage.*

##### 1. The tubs are attached to the end of the rope :—

(a) Incline haulage ;

(b) Haulage with rope and return rope ;

(c) Haulage with main and tail rope.

##### 2. The tubs are attached to an endless rope, running above or below them (endless over rope or endless under rope). In either event the rope may be plain or knotted.

Since all these systems have certain points in common, we will first deal with :—

(a) The coupling of the tubs to the rope ;

(b) The method of supporting the rope, and guiding it round curves ;

(c) The moving of the rope, and then with

(d) The methods of haulage.

(a) **Coupling.**—The end of the rope is fitted with a hook or an eye-ring, and is attached therewith to the coupling on the tub. The latter should be provided with strong couplings and coupling bars extending right through the frame. The tubs are formed into a train, and the front tub is hooked on to the end of the rope. A more troublesome method, but one more reliable for steep inclines, is to couple about every second or fourth tub direct on to the rope, either by running a bridle chain along under the tubs, or leading the rope itself under them. At suitable intervals the rope is fitted with hooks which engage in eyes on the tub frames. To couple tubs or trains to an endless under rope use is made of clamps, which grip the rope and are connected with the tubs by hooks or bridle chains.

Fig. 89 shows the Neitsche clamp, consisting of a pair of cheeks which are made to grip the rope on being screwed up by a rimless hand wheel. The operation can be rendered automatic either way by the aid of a horizontal ladder, the spokes of which engage with and turn those of the hand wheel. At the pit eye the track is raised, in relation to the rope, whilst at the junctions with the side roads it is lowered, so that in the former case the rope can escape from between the jaws of the clutch, and in the other enters between them. This system is particularly adapted for haulage above-ground, or for trains of tubs accompanied by a conductor. In many instances the grip consists of a pair of tongs (Fig. 90) over which slides a ring. The ring can be pushed up, and the rope released automatically at the pit eye, by means of appropriately bent rails. Fig. 91 illustrates a method wherein the rope is clamped on to small trucks that fit between the axles of the tubs and carry the latter with them. Used in short, straight, steep inclines.

Tubs may be attached to overhead ropes in the same manner as to under ropes. Simple coupling chains are also used, a light chain being fastened to the tub, then twisted two or three times round the rope, and the terminal hook fixed in one of the chain links. This plan is less injurious to the rope than clamps, and there is no difficulty in guiding the rope round curves. On the other hand, the rope is liable to twist on its own axis, especially

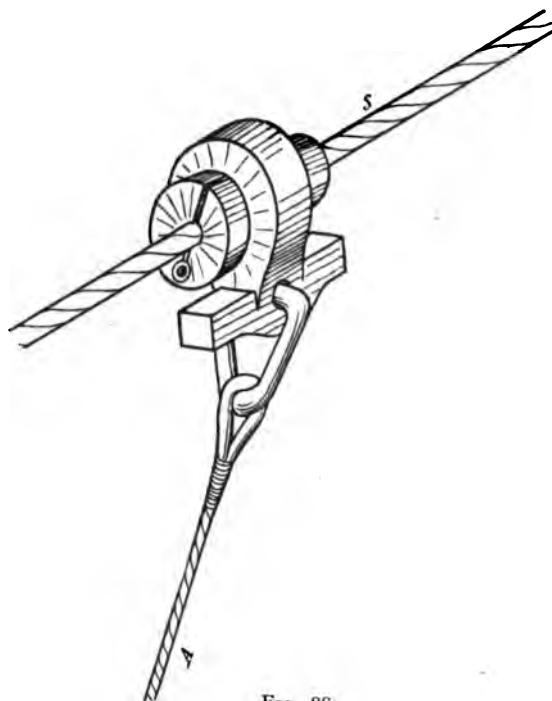


FIG. 88.

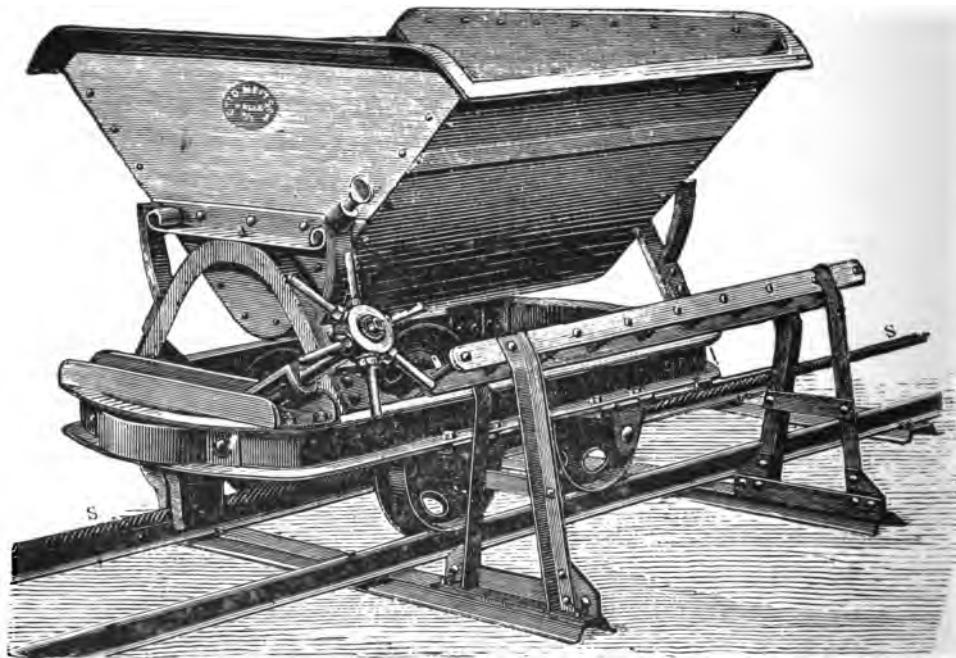


FIG. 89. (Note.—S = haulage rope; A = coupling rope.)

when new, under variable tension, or when going round curves, the

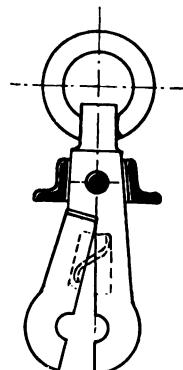


FIG. 90.

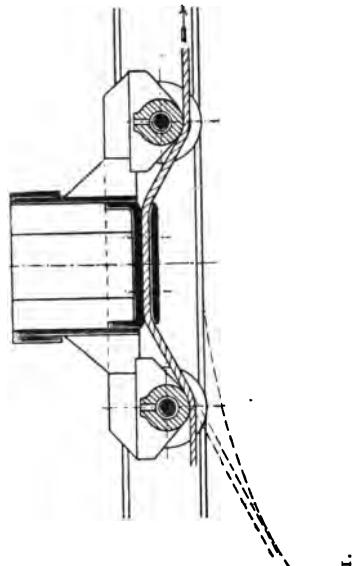
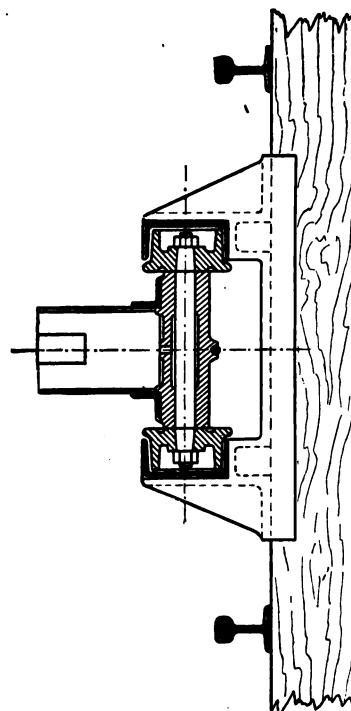


FIG. 91.



result being that the chain gets shortened and draws the tub off the

track. Again, the tubs must be coupled by hand, which entails a greater amount of labour, and the system is no good for work in inclines. Instead of slinging the chain over the rope, use may be made of a clamp (Fig. 92), which is closed by a screw or by the pull on the chain, the ring, R, then serving to secure the fastening. Fig. 88 shows a clutch for train haulage in inclines. Most frequently, however, the coupling between a smooth, overhead rope and the tubs is effected by forked carriers, the English form being shown in

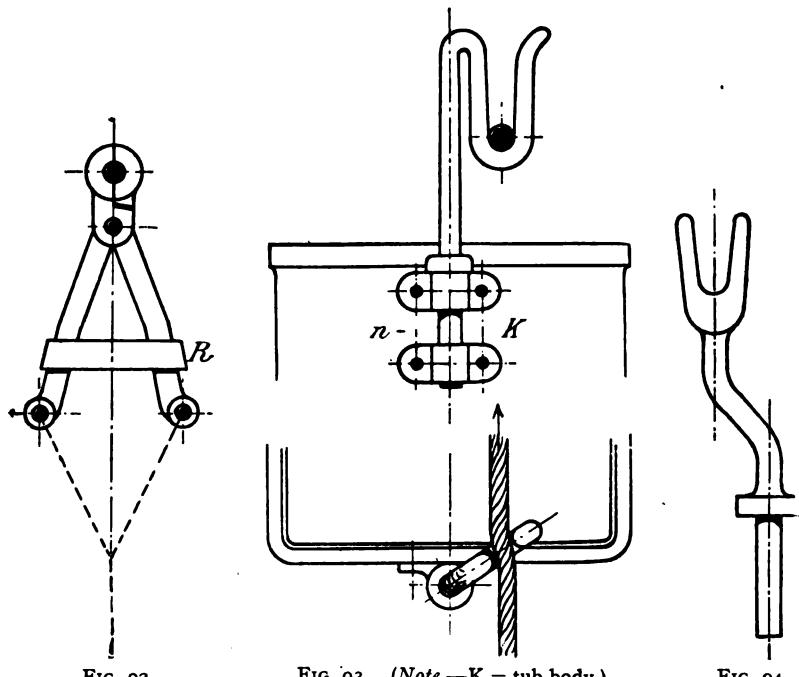


FIG. 92.

FIG. 93. (Note.—K = tub body.)

FIG. 94.

Fig. 93, whilst that represented in Fig. 94 is better adapted for counter curves. The eccentric pull of the rope twists the forks round a little, so that a slight kinking of the rope is produced in the slot, and the tub is drawn along. To release the rope automatically from the forks, the former is raised, and a slight downward gradient is given to the track (see Fig. 122), whereby the truck runs downhill of itself, whilst the fork withdraws and leaves the rope free. When the forks are much worn or damaged, and therefore turn with difficulty, they are often lifted away from the

tub, and on this account a detacher is placed in front of the rope pulley to throw off the forks. Again, the tubs may easily get jammed and derailed if the rope is not lifted out of the forks in good time, and the latter do not turn easily in their sockets. These inconveniences in the automatic release form the chief disadvantage.

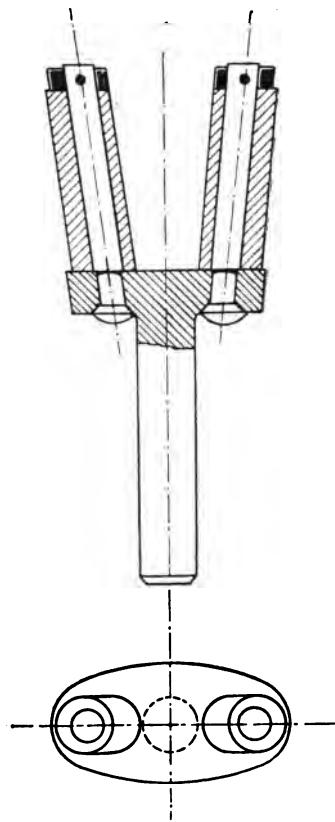


FIG. 95.

of the English rope forks, which otherwise, from their simplicity, are among the best of their kind.

Brown's fork, in which the clamping of the rope is accomplished by means of eccentric sleeves, is illustrated in Fig. 95.

The carriers to be mentioned later, in connection with wire-rope tramways, are also suitable, in principle, for smooth, overhead ropes, but it is not advisable to fit such expensive and easily

damaged couplings to tubs that are exposed to the rough usage of the pit.

The endeavour to discover some method of coupling tubs to the rope, at once simple, cheap, suitable for travelling round curves and up and down inclines, and at the same time automatically detachable and protecting the rope, has led to the employment of knotted ropes, the advantages of which, however, are almost entirely nullified by their numerous inherent defects.

Fig. 96 shows a rope provided with a knot, K, and a counter knot, K', for use in double gradients. The fork in this case is centric. The simplest knots—which, however, are exposed to the greatest wear, and consequently must most often be renewed—

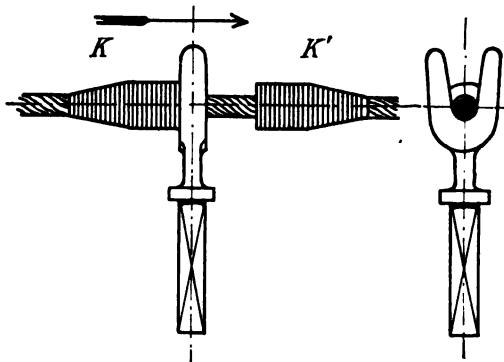


FIG. 96.

consist of well-tarred hemp and hempen cord. Sometimes the end nearest the fork is capped with steel, or the knots are made of divided steel sleeves.

Improvements—though at the expense of simplicity—have been made in knots, by fitting them with elastic coverings or enclosing them in front and rear, so as to do away with the counter knots.

Whereas with the English fork the points of attachment to the rope are constantly changing, and the wear on the rope is consequently uniform, the wear on knotted ropes is always in the same spots. This may be avoided by frequently changing the position of the knots, but the remedy is an expensive one.

(b) **Rope Guides.**—I. *For Open Rope or Under Rope.*—To diminish the wear and resistance, the rope must be prevented from

dragging on the floor of the haulage road, and to this end flanged rollers, 6-10 ins. in diameter and about 6-12 ins. broad, must be arranged at distances of 4-8 yds., according to the minimum rope tension and the height of the rollers above the sleepers. These rollers are of cast-iron, or wood with iron hubs, and run on well-greased fixed journals. They must be well mounted, and looked after with care, or they will soon begin to run so stiffly that the rope commences to slip over them.

The rope may be guided round curves:—

(a) By alternately vertical and horizontal rollers (Fig. 97), the former being often slightly taper, with the greatest diameter overhead, to prevent the rope mounting upwards.

(b) By slanting rollers, fitted with high flanges (Figs. 98, 99).

Since, with these rollers, the rope is not entirely prevented from springing out, bobbins, W, are provided at intervals, to catch the rope in this eventuality. The rollers are not mounted in the centre of the track, but somewhat nearer the centre of curvature. In very sharp curves they must even be placed outside the track, when the tail rope can be induced to enter properly.

2. *For Overhead Ropes.*—On straight roads the rope lies in the forks and is supported thereby, rollers being only needed in the curves and at junctions where the rope is lifted; though if the intervals between successive trucks are considerable, some means must be provided for keeping the rope from dragging on the floor. In curves, the rope may either be left attached to the tubs, or the latter may be freed and left to run of themselves down the gradient then provided for this purpose, to be coupled up again when they re-enter the straight.

This latter method involves considerable labour, and is therefore seldom used. The curve rollers are made as large as possible, and distributed in such a manner that the divergence of the rope by any single roller does not exceed about  $12^\circ$ . The usual form is shown in Fig. 100. To ensure the rope re-entering the forks, it is a frequent practice to provide swing rollers that fit under the rope and are pushed aside by the passing forks. According to Forster, sharp curves should contain only a single large guide pulley (Fig.

101), the rails being replaced by U-irons or by a flooring of iron plates.

(c) **Methods of Actuating the Rope.**—The rope is either wound round an ordinary drum, or led over driving pulleys, being drawn onward by the friction between the rope and the pulley grooves.

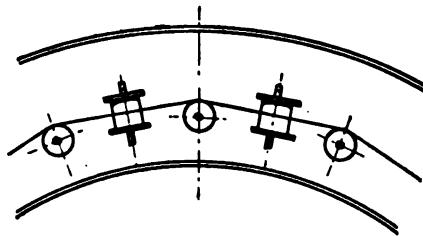


FIG. 97.

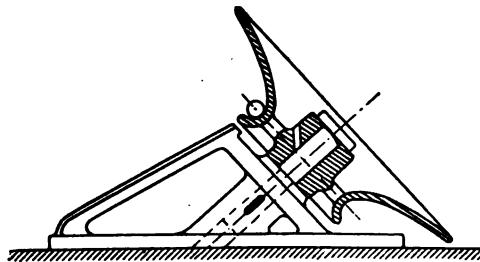


FIG. 98.

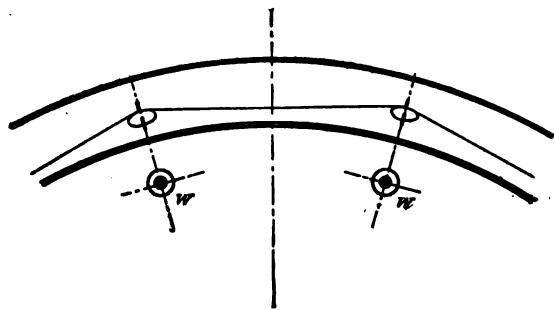


FIG. 99.

In order to preclude slipping  $\frac{S}{S_1}$  must be  $< e^{\alpha}$  (see p. 68),  $S$  being the tension of the oncoming rope,  $S_1$  that of the paid out tail rope,  $e$  the base of the natural log,  $\alpha$  the embraced arc, and  $f$  the coefficient of friction (for ropes running on cast-iron,  $f = 0.1$ ; on wood,  $f = 0.2$ ).

Unless this condition be fulfilled, the embraced arc of the pulley must be increased, or the friction augmented, or the ratio  $S + S_1$  diminished, by increasing the tension on both ends of the rope by an equal extent.

1. *Increasing  $a$ .*—The rope is wound several times round the pulley. In Fig. 102, for instance,  $a = 3\pi$ . In such case the on-

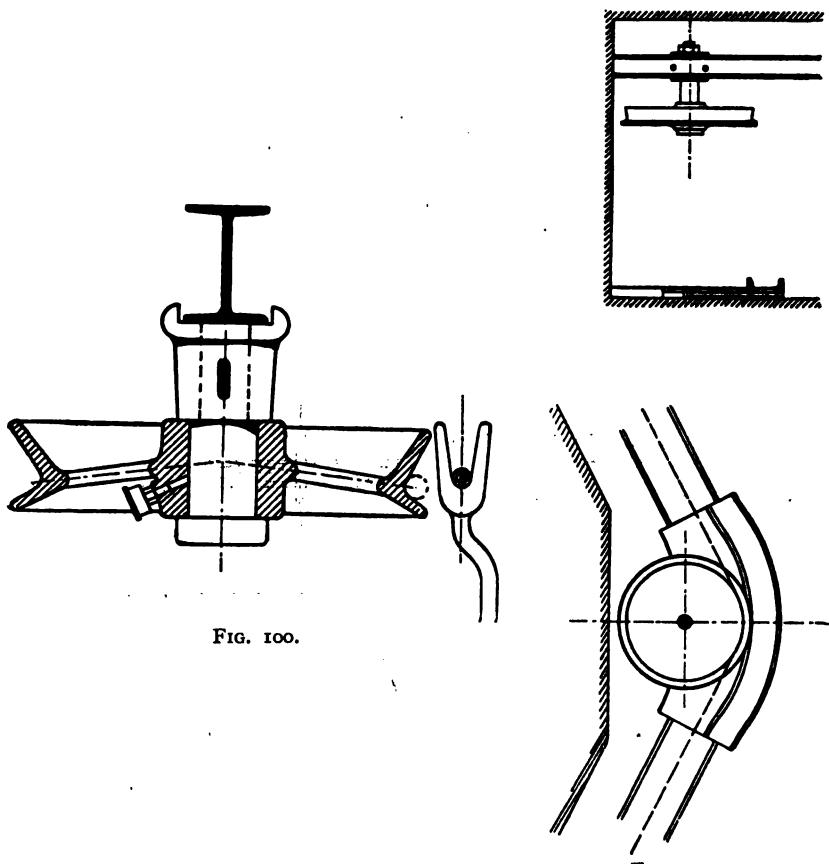


FIG. 100.

FIG. 101.

coming rope has to constantly push aside the turns already on the pulley, the wear being thereby augmented. Mounting the pulley in the manner shown in Fig. 102, or providing a sickle-shaped guide bar, S, will facilitate the coiling of the rope; but the continued sliding of the rope is injurious.

Another arrangement is shown in Fig. 103. Here T is the

actual driving pulley, L merely a guide pulley, the serial numbers indicating the path taken by the rope. If, for example, T is provided with four grooves, then a three-grooved guide pulley will be required. A better plan is to have three single-grooved guide pulleys, only one of which is mounted fast on its axis, whilst the other two

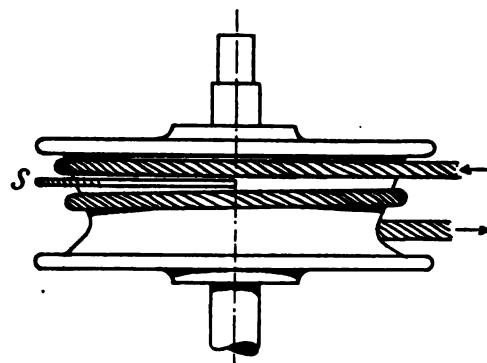


FIG. 102.

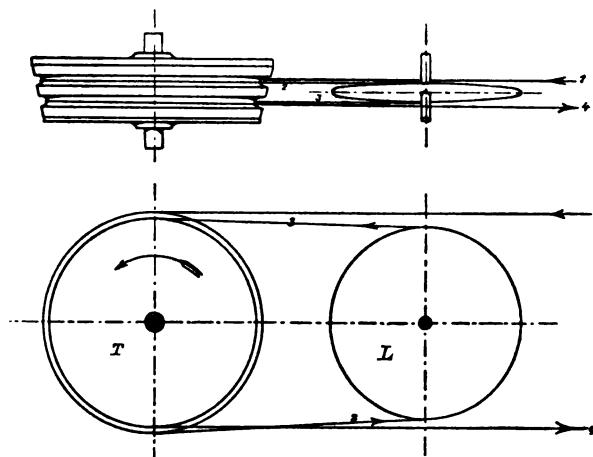


FIG. 103.

run loose, so as to take up slight fluctuations of the rope, without slipping. Very often the one guide pulley runs on a fixed axis, whilst the two loose pulleys are mounted on extensions of the hub, because the relative displacement of the pulleys in revolving is but small, and hence the wear of the hubs is prevented and the simplest lubrication is sufficient.

Owing to the fact that the intake groove of the driving pulley is exposed to the greatest amount of wear, the grooves are made of slightly decreasing diameter, as shown in the drawing.

Laying the rope in S-curves on the pulleys, in order to increase the embraced arc, increases the wear on the rope, and should be discarded.

The driving and guide pulleys should be well stayed one against the other.

2. *Increasing the Friction.*—The coefficient of friction can be raised to 0·2-0·3 by lining the grooves of the rope pulley with wood or leather (Fig. 104). Sometimes hempen rope is laid in the

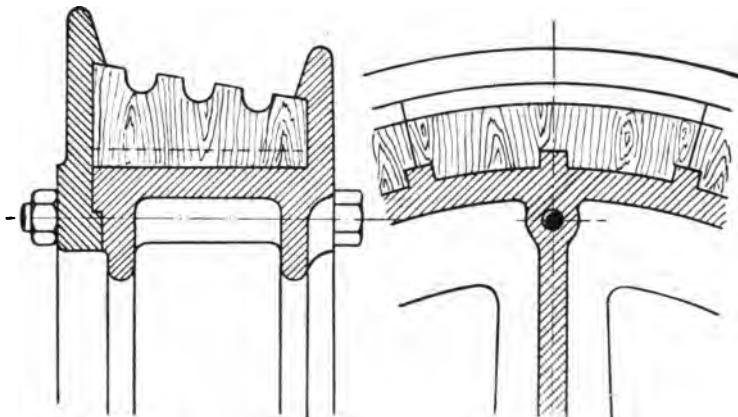


FIG. 104.

grooves. All these means protect the rope, but need frequent renewal of the material.

The friction may also be augmented by increasing the normal pressure, the cross-section of the groove being given the form shown in Fig. 105. Here, as before,  $S = S_1 e^{\alpha}$ , though the value 0·26 can be substituted in place of 0·1 for  $f$ . The wear on the rope is considerable. Fowler's pulley, which belongs to this class, is but little used in mining work.

3. The value of the expression  $S + S_1$  may also be diminished by increasing both tensions, for  $\frac{S + q}{S_1 + q}$  approximates more closely to unity the higher the value of  $q$ . With open ropes—tubs at the

extremity of the rope—the dead weight of the rolling stock is increased for this purpose; but for endless ropes tension appliances are provided. In both instances, however, the rope tension is augmented, and therefore also the rope diameter, waste of power, etc.

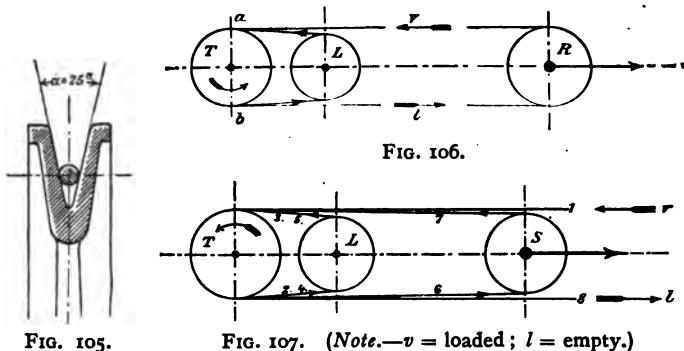


FIG. 105.

FIG. 106.

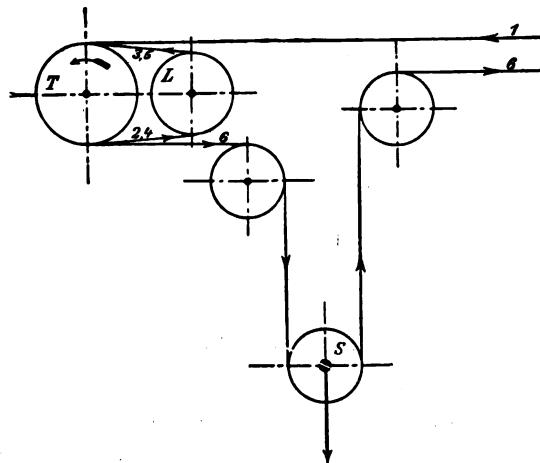
FIG. 107. (Note.— $v$  = loaded;  $l$  = empty.)

FIG. 108.

*Tension Appliances for Endless Ropes.*—A typical example of the course taken by the rope is shown in Fig. 106,  $T$  being the driving pulley,  $L$  the guide pulley, and  $R$  the end pulley for the return of the rope. The tension differs in all positions, being greatest at  $a$  and smallest at  $b$ ; but even in the latter position must be great enough to prevent the rope hanging too slack, dragging on the floor, or slipping over the driving pulley. The adjustment of this

tension, and keeping it up should the rope stretch, is the task of the tension appliance. For this purpose L or R, or both of them, are mounted in such a manner that they may be moved in the direction

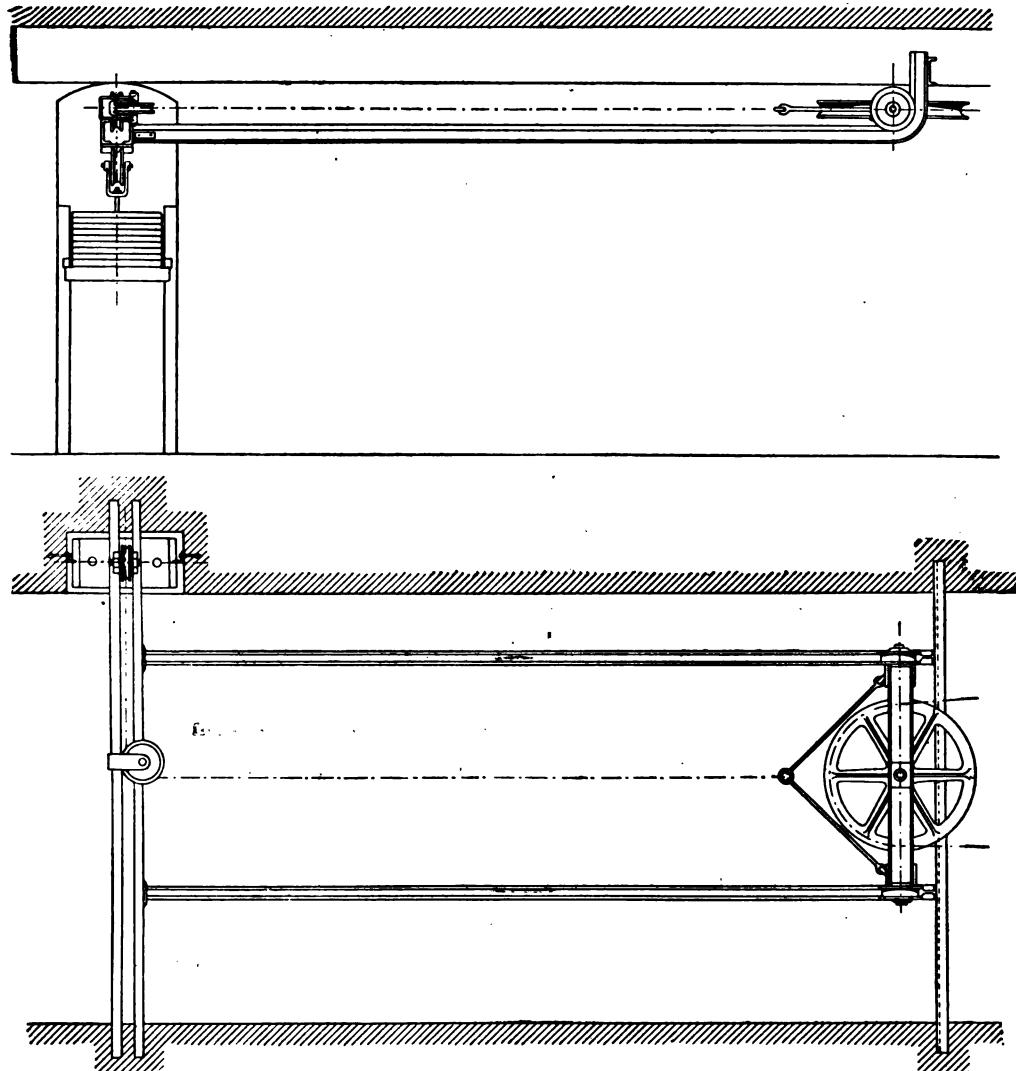


FIG. 109.

indicated by the arrow. The adjustment of the guide pulley is mostly effected by the pull of a weight, and therefore automatically, in which event it serves to maintain the tension, whilst the stretch

of the rope is taken up by moving and refixing R by hand when necessary. In multiple-groove guide pulleys, L, this method cannot be adopted, and a separate tension pulley must, therefore, be provided near the driving pulley.

Fig. 107 applies in the case of vertical driving pulleys, Fig. 108 for those mounted horizontally, Fig. 109 shows an automatic tension pulley (Hoppe's). Instead of weights, the chain for adjusting the tension pulley may be acted on by a screw spindle. When the rope stretches considerably the chain is shortened.

(d) **Systems of Haulage.**—*1. Uphill Double-track Haulage in Straight Roads. Haulage in Inclines.*—The tubs—or skeleton trucks in steep inclines—are fastened to the tail of the rope, and are hauled by a winch fitted with drums or pulleys. If conical drums are used, care must be taken that the tubs do not meet in the middle of the road. Rope pulleys are specially adapted for haulage on skeleton trucks. The calculations for the motors and brakes are identical with those for winding engines. The resistance is compounded of the relative weight of tubs and rope, friction in the tubs (about 2 per cent. of the normal pressure), and the guide-pulley resistance, which for initial calculations may be ascertained by adding to the weight of the tubs 17 to 25 lb. for every 100 yards of track.

If the gradient of the track is progressively steeper from below upwards, the relative weight of the ascending tubs increases, since the length of rope is a continually diminishing quantity; the converse applies to the descending tubs, so that by altering the gradients the weight of the rope can be compensated. The calculation gives a cycloid as the profile of the track.

With varying gradients the engine-power has to be determined for different parts of the track, and the maxima thus obtained must be borne in mind.

The mean velocity is  $v = 80$  ins., the maximum under favourable conditions being twice as great, or even more.

**Track.**—(a) Double track throughout. This is the best, but most expensive method.

(b) (See Fig. 110.) Single track with sidings at intervals, and

movable points. The tubs or trains pass each other at *m, n*. The descending tub, *A*, is switched automatically by the points, which are then in position for the ascending tub, *B*, which in turn displaces them in the opposite direction.

This method is cheaper as regards construction of track and road, but is attended with the defects of the points.

(c) Movable points at *a* and *b* (see Fig. 111). The descending tubs must pass over the up-going rope at the switch, and *vice versa*. It is difficult to dispense with the employment of a watcher at the points, and hence the lower cost of installation is counterbalanced.

A very good plan is the one shown in Fig. 112. Both the

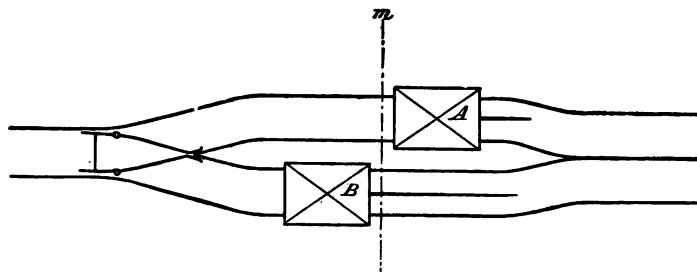


FIG. 110.

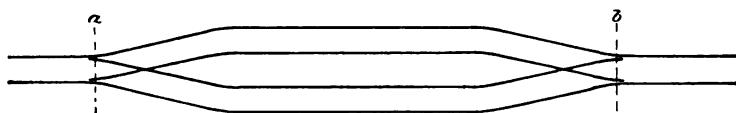


FIG. 111.

skeleton trucks have very broad smooth inside wheels, the outer ones being fitted with double flanges. The rope is guided so as to lie between the rails at *A* and *B*, whilst the second truck passes over it. In the upper half of the road the rope is guided on two sets of rollers, one for the up and the other for the down rope.

**Setting-on Places.**—For single tubs or short trains a flooring of iron-plates is best. Long trains require crossings and switches, the rope running under the track floor towards the engine. For skeleton trucks and double tracks, either small draw-bridges must be provided, to enable the tub from the one truck to be pushed over the lower track of the other, or else the tracks are run together at

the top, as in Fig. 113. The tubs are taken from or delivered to the track, *m* or *n*. The truck journeying on *A* enters at *a* and

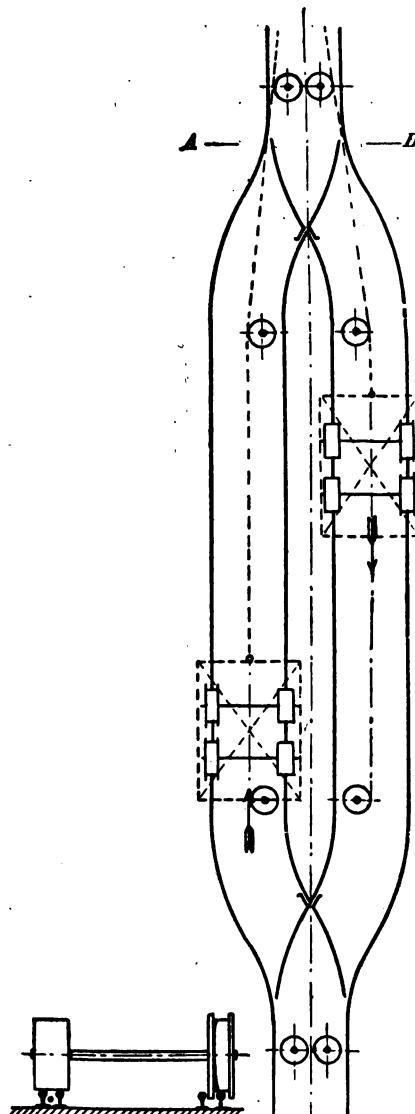


FIG. 112.

must then be displaced further towards *n*, to enable a better connection to be effected with the corresponding track. The same applies to the other trucks, according to their direction.

*2. Haulage with Main and Tail Rope, or with Rope and Counter-rope.*—Single haulage for horizontal roads or slight gradients with few curves.

Fig. 114. The main rope,  $v$ , extends from the drum,  $T$ , to the train of tubs. From the rear of the train the tail rope,  $h$ , passes

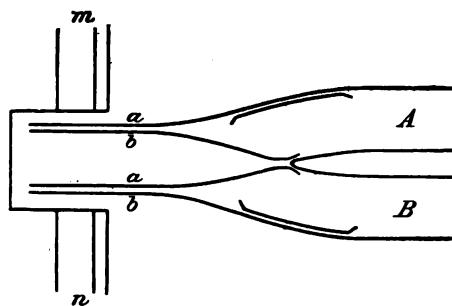


FIG. 113.

over the end pulley,  $S$ , back to the second drum,  $T_1$ . Each drum can be coupled to, or detached from, the engine in turn. When  $T$  is coupled up, the main rope pulls the full tubs in the direction of the arrow, and the tail rope is paid out by the loose pulley,  $T_1$ ,

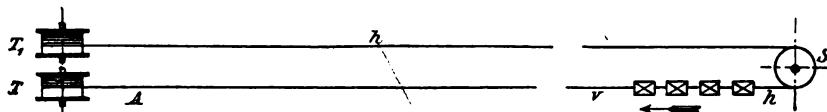


FIG. 114.

which is slightly braked. Arriving at  $A$ , the train is unhooked from both ropes, which are then attached to the waiting train of empties, whereupon  $T$  is disconnected and  $T_1$  coupled to the engine. The tail rope,  $h$ , now draws the train, whilst the main rope runs off

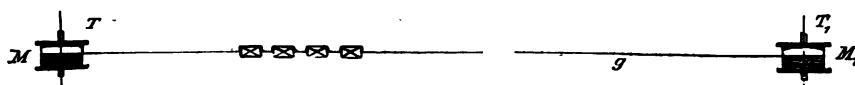


FIG. 115.

from the loose drum,  $T$ , and so forth. The tail rope may be guided near the track, against the walls or roof, or even traverse a separate road.

Fig. 115. The drum,  $T$ , of the engine,  $M$ , pulls the full train by means of the rope,  $s$ , the counter-rope,  $g$ , running off from the

loosened (and braked) drum,  $T_1$ , of engine,  $M_1$ . When the train reaches the pit eye, both ropes are attached to the waiting train of empties,  $T_1$  is coupled up, and the engine,  $M_1$ , started whilst  $T$  is uncoupled from its engine,  $M$ .

Neither of these systems is much in use; that with rope and counter-rope especially, since, although the guiding of the rope is simpler, and the rope resistance lower, than with main and tail ropes, it entails the employment of two engines with their drivers, and some means of signalling from one to the other. Haulage from branch roads is also a troublesome matter with this system.

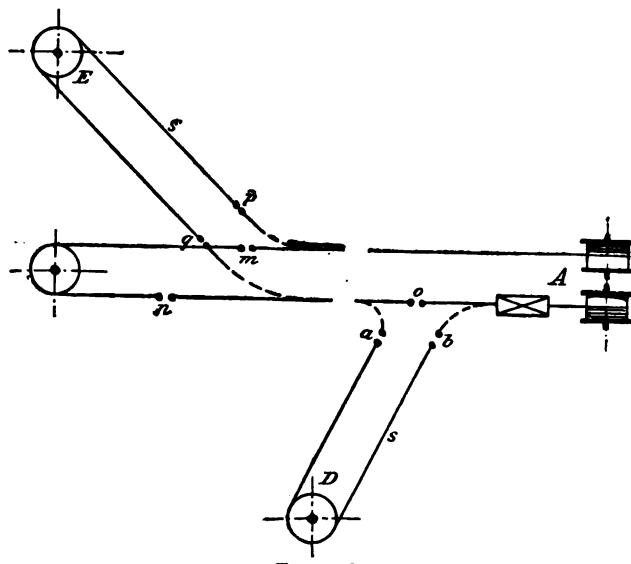


FIG. 116.

The velocity is from 4 to 6 yds., and hence the tracks must be well laid. From 40 to 100 tubs go to a train. Frequently a guard's truck is provided at the end of the train, the guard seeing that the tail rope lies properly on the rollers, especially in curves. He is also able to uncouple the tail or counter-rope quickly.

**Hauling from Branch Roads** (Fig. 116).—The main rope is divided at *o*, the ends, *a* and *b*, being hooked on to the rope, *s*, in the branch road ; or the same procedure is adopted at *m* with regard to the branch rope, *s'*. In either event, the train of empties can be hauled into the branch, without further delay, and the full train

standing at D or E drawn towards A. A rope coupling for this purpose is shown in Fig. 117; but the length of the lashings impedes its passage over the rollers, shorter couplings, such as that in Fig. 117a, being preferable.

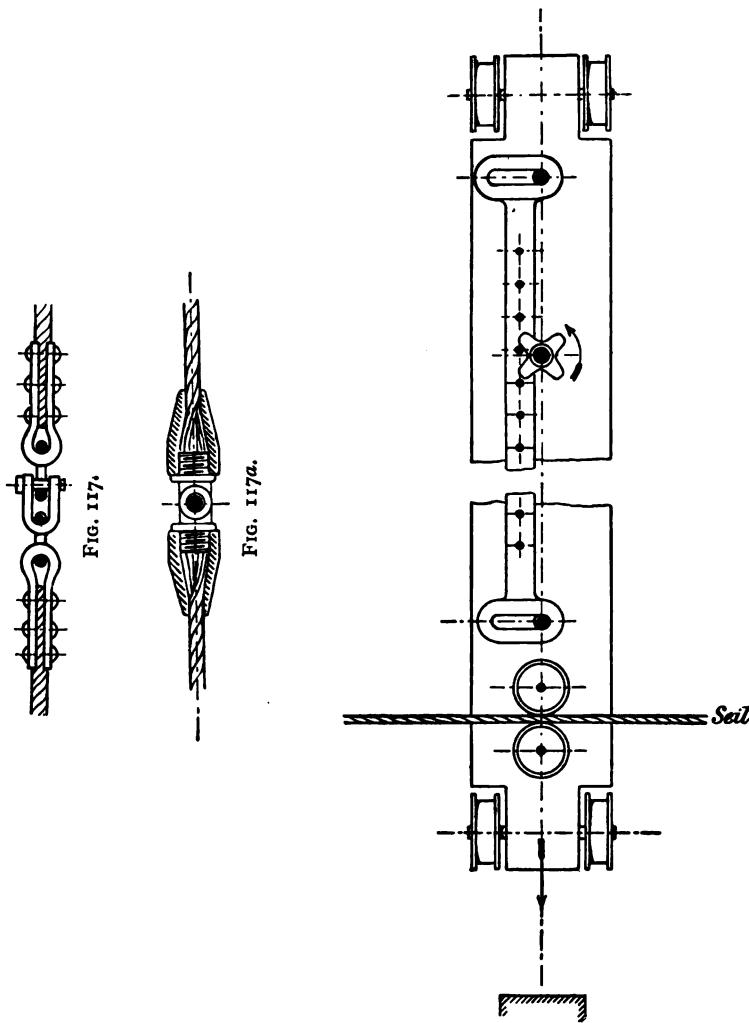


FIG. 118. (Note.—Seil = rope.)

**Engines.**—Single- or double-cylinder engines, driven by steam, compressed air, or water power; electro-motors, etc. Reversing gear, though not essential, is desirable. The drums are mounted on separate shafts, are fitted with brakes, and can be coupled up

or freed by sliding cog wheels or other clutches. The drums, though of small diameter, must be able to take up a great length of rope, and are therefore made broad and provided with attachments for ensuring the proper laying of the superimposed coils of

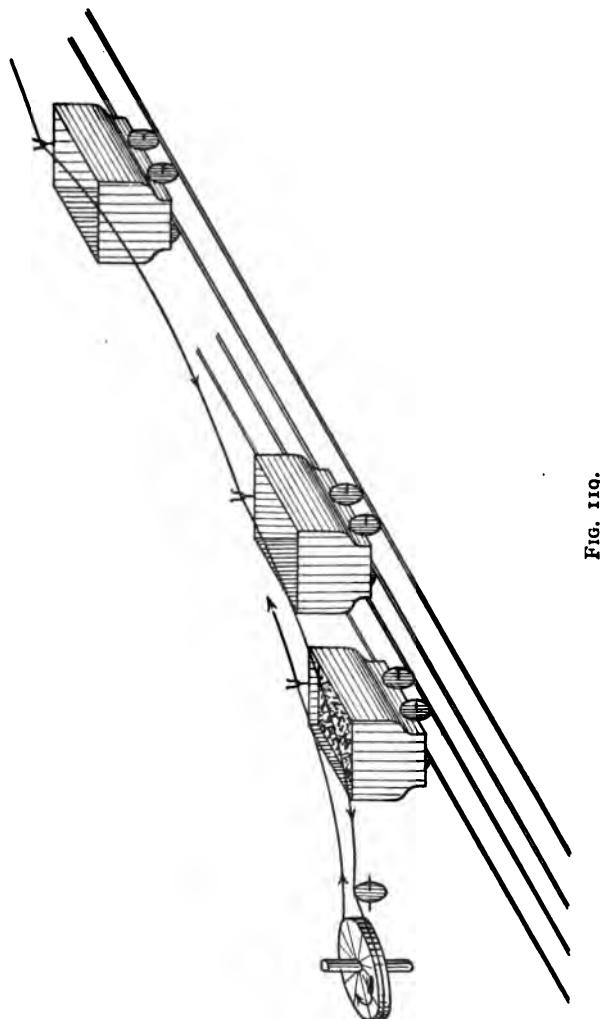


FIG. 119.

rope. These guides consist of slides or small travellers, moving to and fro over the drum and guiding the rope. They are driven in the same manner as the tables on planing machines, or as shown in Fig. 118, the traveller being attached to a vertical shaft driven by the engine. When the guide reaches the end of its travel,

further progress is prevented by an elastic abutment, whilst the traveller forces to the right an adjustable lateral driving bar and then retraces its course.

3. *Endless Overhead Rope* (Fig. 119).—For long horizontal or gently sloping roads with fairly constant gradients. A double track is used and tubs are hauled both ways. The average rate of speed is 40 ins. The interval between the single tubs should be such (15-20 yds.) as to prevent the rope dragging on the floor. The carriers, rope guides and driving gear are the same as those already described.

The direction of movement being constant, no reversing gear is needed, but is desirable in view of accidents. The setting-on places are simple, and the uniform conveyance of single tubs is better adapted to colliery work and cage winding than long trains, which entail an accumulation of tubs at the ends of the roads, and greater danger of derailing. The less powerful engine, running continuously, works more economically and pays for itself off more quickly than the larger engines working under irregular loads in train haulage.

The setting-on places are horizontal or with a gentle slope so that the tubs run down automatically. To facilitate keeping the tubs equidistant, a signal—paint mark, lamp or bell—is set up a certain distance from the setting-on place, and as soon as the last tub has passed this spot, a fresh one can be released, empty tubs being sent on when full ones are lacking. Where tubs are to be set on at intermediate spots, the rope must be raised there by means of rollers to enable this to be done.

**Hauling from Branch Roads.**—The usual system is shown in Fig. 120. A is the chief motor, and at B three pulleys are mounted on the same upright shaft, for the three endless ropes, 1, 2 and 3. C and D are the end pulleys. If the pulleys for 2 and 3 are mounted loose, and fitted with detachable couplings, the work can be stopped in either of the branches, as required. If local circumstances permit, it is preferable to have the chief motor set up at B.

4. *Endless Under Rope*.—This system is employed where the traffic is slack, and the tubs are at irregular distances, so that an

overhead rope would drag on the floor ; it is also useful in roads of variable gradient and curvings. Above-ground it is employed for steep inclines, though in similar cases in the pit winch hoists are preferable.

Single tubs or short trains may be hauled ; in the latter event, only three or even two rails are required. The friction and wear of the rope are greater than with overhead ropes.

*Chain Haulage.*

1. **Overhead Chain.**—Arrangement same as in Fig. 119, but with a chain instead of a rope. Equal or even superior to rope haulage for straight roads with numerous setting-on places, alternat-

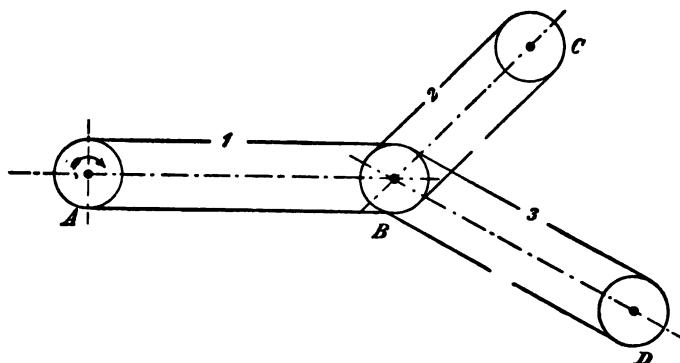


FIG. 120.

ing gradients, and especially hollows. The speed is 40-80 ins., being higher than with ropes, the heavy chain resting on the tubs, increasing their stability and thus lessening the risk of derailing. The higher speed enables an equal amount of haulage to be done with a smaller number of tubs on the line at any one time. The chain costs about three times, and weighs about five to six times as much as a corresponding rope, the greater weight increasing the tub friction and the motive-power required. Chains break suddenly without any previous warning, whereas the damaged portions of ropes are revealed, by projecting ends of wire, long before the rope parts. On the other hand, the broken links of a chain can be quickly replaced by temporary substitutes, whilst the splicing of

ropes entails a prolonged stoppage. True, the substituted links form a source of weakness, and cannot always be replaced by new welded links underground. The life of a chain is two to four times that of a rope.

*Coupling the Tubs.*—  
The chain rests free on the tub top (without

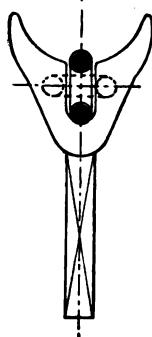


FIG. 121.

carriers), and exerts its tractive force by the friction of the links on the upper frame and contents of the tub. For steep ascents, and in travelling round curves unprovided with guides, chain forks (Fig. 121) are fastened to the front ends of the tubs.

*Method of Driving.*—  
The chain is passed  $\frac{1}{2}$  or

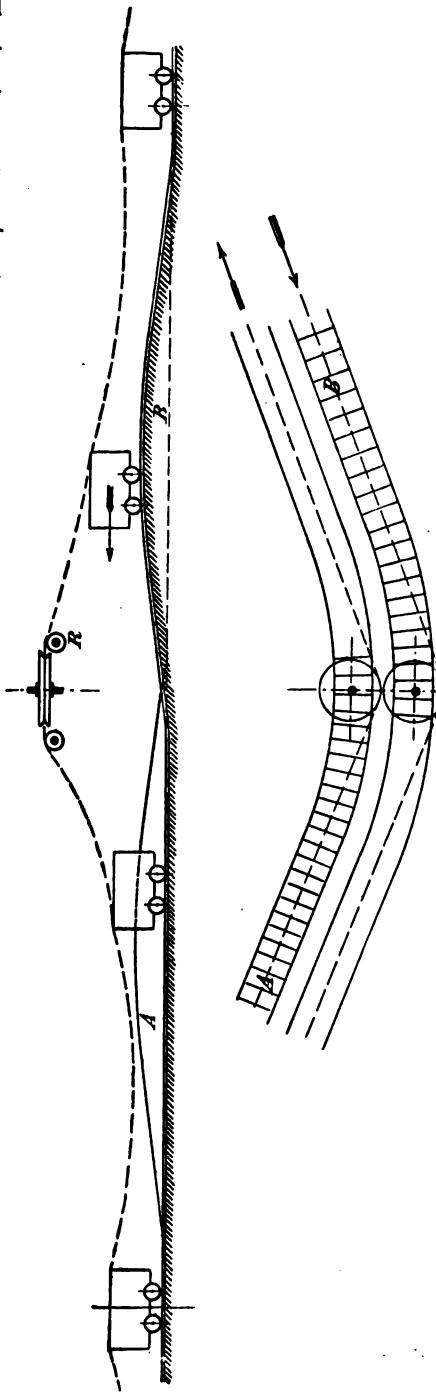
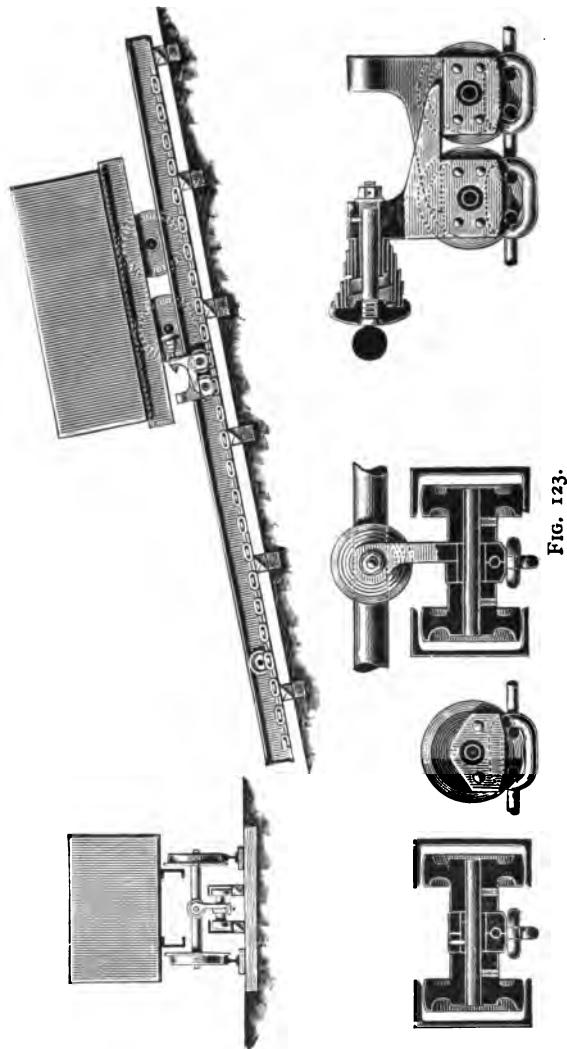


FIG. 122.

$1\frac{1}{2}$  turns round a pulley, with a smooth or wood-lined groove, of slightly conical section to facilitate the displacement of the preceding coil by the on-coming chain. Sickle-shaped guides are provided



for the same purpose. Chain-peg (sprocket) rollers require calibrated chains, and fail to act if the chain stretches and wears unequally. Where the tractive force has to be high, the best plan is to employ a driving pulley and counter-pulley, as in the case of ropes. The

setting-on places and hauling from branch ropes are the same as described under "Rope Haulage".

*Passing Round Curves.*—As shown in Fig. 122 the chain is led over high-mounted pulleys, and the track is graded downhill so that the released tubs may run through the curve of themselves until caught again by the lowered chain. Another method of traversing curves has been described on p. 99.

**2. Under Chain.**—This method is specially adapted for short, steep inclines.

Fig. 123 illustrates the Humboldt system. A pair of channel irons, mounted between the rails, forms the track for the carrier trucks, which are fastened to the chain and press, by means of a small buffer, against the axle of the tub, which therefore does not require any special fittings.

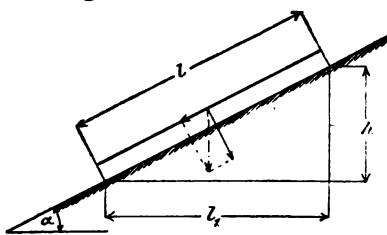


FIG. 124.

The carriers are made of such a shape that they can pass over the chain pulleys.

*Calculations for Rope and Chain Haulage Tracks* (Fig. 124).—The organ of traction and the tubs may be regarded as a load uniformly distributed over the track. If  $g$  represents the weight of rope or chain per unit length (running yard),  $a$  the distance between the tubs, and  $P$  the weight of the latter ( $P$  for full tubs, and  $P_v$  for empties), then the load aforesaid will be  $g + \frac{P}{a}$  per running yard of track. The weight for the whole track,  $l$ , will amount to  $(g + \frac{P}{a})l$ ; and to draw this weight uphill a force  $Z$  will be required, the amount of which is compounded of the relative gravity

$$(g + \frac{P}{a})l \times \sin \alpha = (g + \frac{P}{a})h$$

and the friction

$$\mu \left( g + \frac{P}{a} \right) l \times \cos \alpha = \mu \left( g + \frac{P}{a} \right) l_1.$$

Hence,  $Z = \left( g + \frac{P}{a} \right) (h + \mu \times l_1)$ , wherein  $h$  is positive for uphill gradients and negative for descending tubs,  $l_1$  being positive when the motion is towards the source of power, and negative in the opposite direction. The total coefficient of friction,  $\mu$ , may be taken as 0.01 under favourable circumstances, and 0.02 for bad or greatly curved tracks.

The completed equation enables the rope pull to be determined for any part of the track.

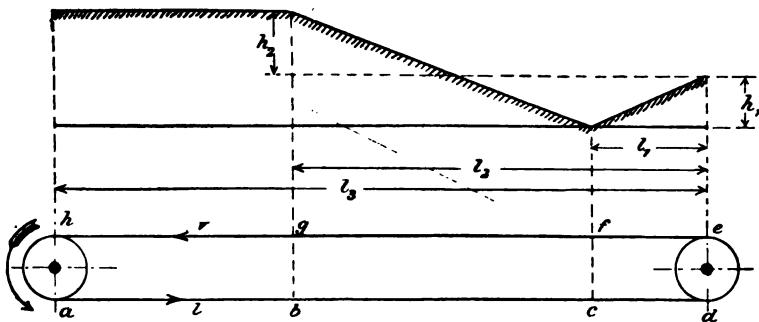


FIG. 124a. (Note.— $v$  = full;  $l$  = empty.)

If the installation be represented by Fig. 124a, and the still unknown tension in  $e$  by  $S$  (for the present), it will be

$$\text{at the point } f = S + Z = S + \left( \frac{P_v}{a} + g \right) (-h_1 + \mu l_1),$$

$$\text{,, , } g = S + \left( \frac{P_v}{a} + g \right) (h_2 + \mu l_2),$$

$$\text{,, , } h = S + \left( \frac{P_v}{a} + g \right) (h_2 + \mu l_3),$$

and for the return track (empties)

$$\text{in } c = S + \left( \frac{P_e}{a} + g \right) (-h_1 - \mu l_1),$$

$$\text{,, } b = S + \left( \frac{P_e}{a} + g \right) (h_2 - \mu l_2),$$

$$\text{,, } a = S + \left( \frac{P_e}{a} + g \right) (h_2 - \mu l_3).$$

Of these strains that at  $f$  will presumably have the lowest value;

but even here it should not fall so low as to allow the chain or rope to drag on the floor. For ropes a "dead" tension,  $S_0$ , of 4-6 cwt. will be sufficient; for chains it should be about equal to the weight of 50-60 yds. of chain. By setting down the tension in  $f = S_0$ , i.e.,

$$S_0 = S + \left( \frac{P_v}{a} + g \right) (-h_1 + \mu l_1),$$

and estimating  $g$  approximately for the present, we obtain the value of  $S$ , whence the value of the maximum tension ( $S_{\max}$ ) in  $h$  can be determined. This amount is increased by the friction of the rollers. In preliminary calculations it is sufficient to allow for this factor an extra 5-15 per cent., according to the number of curves in the road. For exact calculations the pull required to move a roller of radius  $R$  may be assumed as  $0.1 \times K \times \frac{r}{R}$ , wherein  $K$  implies the normal pressure on journals of radius  $r$ . In the case of driving and guide pulleys,  $R$  is the resultant of the rope tension; for carrier rollers the weight of the superincumbent portion must be substituted. A small extra allowance must be made for the resistance of the chain or rope to flexion. From the useful tension  $S_n$ —difference between the maximum and minimum pull of the rope—is found the engine-power required, for a haulage speed  $= v$  and efficiency  $\eta$ , by the formula  $N = \frac{S_n \times v}{\eta \times 75}$ . The engine must, however, be capable of exerting a momentary force, at least  $1\frac{1}{2}$  times this, for starting, etc.

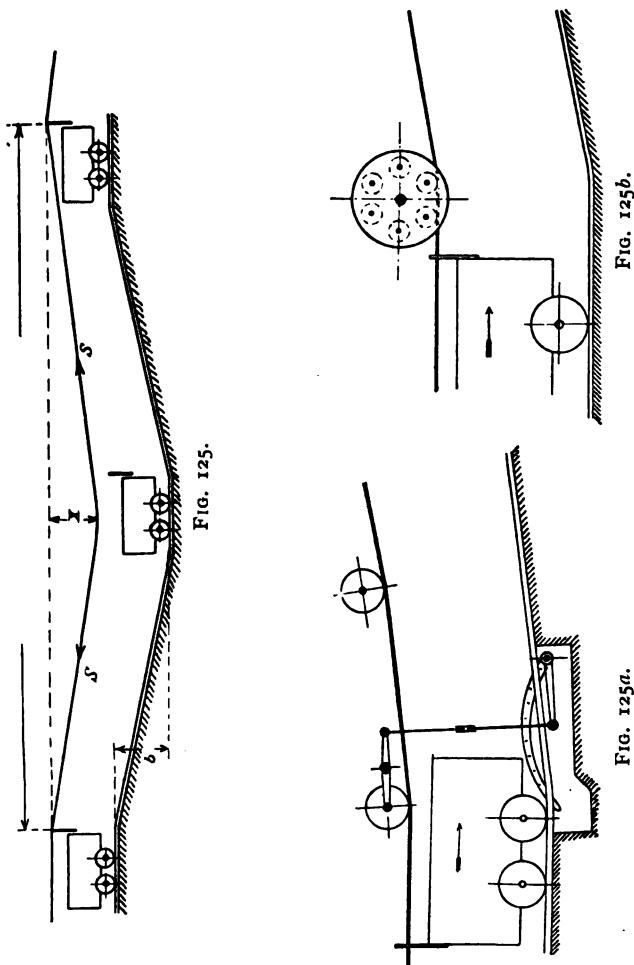
The tensions in  $a$  and  $b$  being known, the requisite number of turns to give the rope on the driving pulley can be ascertained. The strength of rope or chain is selected in accordance with  $S_{\max}$ .

If the full tubs run from a higher to a much lower plane, the engine is replaced by a brake.

*Traversing Hollows.*—Fig. 125 shows that, in hollows, the rope is raised out of the forks in the event of  $x$  being less than  $b$ ,  $x$  itself being calculated from the equation of the arc described by the hanging rope, and taken as  $x = \frac{(2a)^2 \times g}{8 S}$ , wherein  $g$  is the weight of the rope, or chain, per running yard, and  $S$  the tension at this

portion of the track. To ensure safety  $x$  may be required to be  $1\frac{1}{2}$ -2 times greater than  $b$ ; and if this be impracticable, the curve of the rope must be increased by artificial means.

According to Fig. 125a a number of heavy rollers are laid on the rope, which must be eased a little from the tubs every time, by the



aid of a suitable lever, in order to ensure the passage of the carrier; or Forster rollers (Fig. 125b) may be used. These consist of two side shields with small interposed rollers, against which the carrier strikes, turns the pulley round a little, and then proceeds on its way.

*Traversing Curves without Guides.*—By raising the inner rail the tubs are tilted outwards, tipping over being prevented by the resultant of the rope pull in the direction of the centre of curvature. This mean force,  $M$ , must be determined, and then a calculation made to ascertain whether the (empty) tubs still possess sufficient stability. Curves with a radius exceeding about 160 yds. can be safely traversed in this manner.

*Wire-rope Tramways.*

The track consists of two parallel wire ropes — line ropes — firmly anchored at one end, kept taut by weights at the other, and supported at intervals by a row of wooden or iron frames or pillars. The travellers of the skips run on the line rope, and the traction is effected by an endless draught rope.

*Details.*—The line ropes are of circular section and made of thick wires, patent locked ropes being also used of late. The diameter of the rope varies according to the strain, 0·8-1·6 ins. being the usual limits for the one supporting the full skips, and 0·6-1·2 ins. for the return line (empties). The various lengths of rope are connected by coupling sleeves. The usual arrangement in the Pohlig simplex rope is shown in Fig. 127, the rope ends, which are widened by means of conical wedges and covered with composition, being tightly encased by steel sleeves which are screwed together by means of a pin.

The line rope should be supported every 50-60 yds., but in crossing rivers or valleys the span may measure as much as 500 yds. The supports consist of pillars or lattice derricks surmounted by

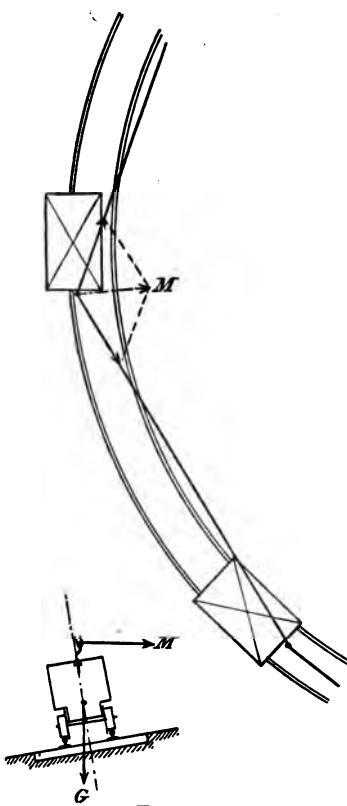


FIG. 126.

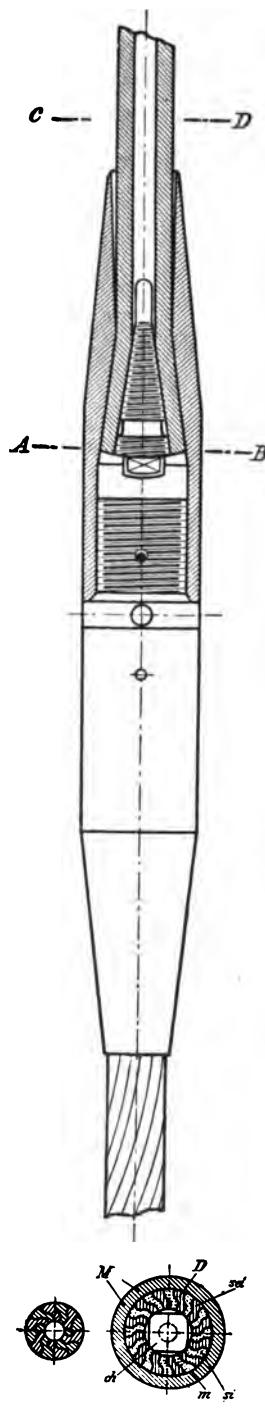


FIG. 127. (Note.—M = sleeve; D = wire of rope; ch = conical screw wedge.)

carrier rollers, or by grooved iron shoes into which the rope fits without any fastening. To rapidly and effectually compensate differences in tension, and in fact impart the requisite tension to the rope as a whole, the one end is anchored, whilst the other is connected to a chain which is led over rollers and carries a heavily weighted chest. By this means a rope tramway of over 1,000 yds. in length may be kept in tension; but for greater distances intermediate tension appliances are necessary. The form of the skips is shown in Fig. 128, consisting of a traveller, a supporting stirrup, with clutch, and the skip proper—generally arranged to tip. The load carried ranges from four to fourteen cwt.

The clutch, connecting the skip with the draught rope, is a particularly important appliance, being the factor deciding the life of the rope and the simplicity and security of the haulage. For slight gradients (1:7) eccentric clamping blocks, which are closed by the pull on the rope, so that the pressure is automatically adjusted to the gradient, are sufficient. A better grip is afforded by plates, pressed against the rope by means of screws. In the new Pohlig clutch (Fig. 129) the screw spindle in the one block has a very quick right-hand thread, that in the other having a very slow left-hand thread, the former serving for rapid coupling and detaching, whilst the other is used for applying the pressure. When the gradient exceeds 1:3, knotted ropes are often used, though this entails an expensive and troublesome dis-

placing and renewing of the knots, and is attended with a good deal of wear on the rope.

An endless draught rope is used. The driving and tension gear resemble those in rope haulage, except that the pulleys are as large as possible (up to 10 ft. diameter). The velocity attained is one to two yards per second.



FIG. 128.

*Stations*.—In addition to the terminal stations, others have to be provided at points where the direction of the line deviates from a direct course; and in very long lines, intermediate stations are erected about every 6,000 yds. At the stations the line rope terminates in rails mounted on shoes at the one side. Switches,

points, turn-tables and shunting platforms enable the traffic to be adequately dealt with. As the skips are pushed forward by hand

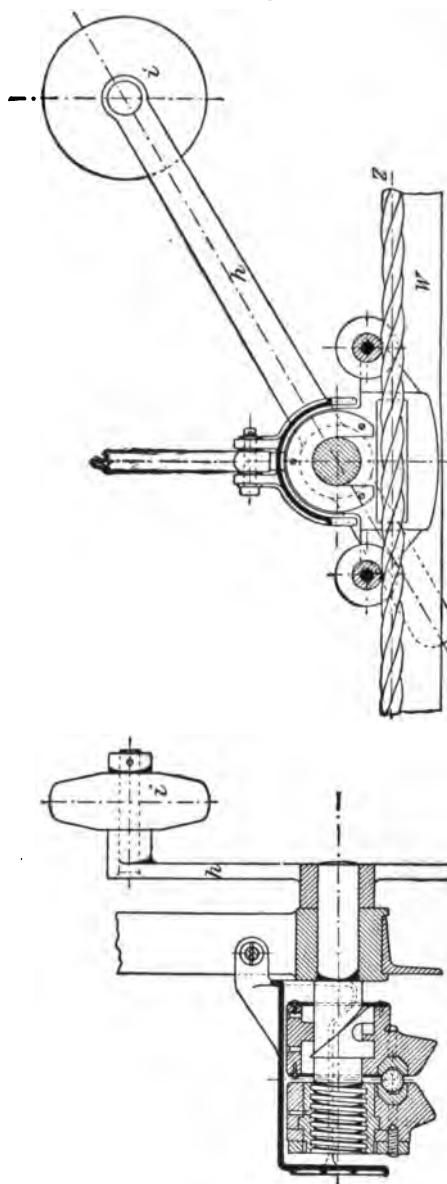


FIG. 129. (Note.—Z = draught rope; W = skip strut.)

on arriving at the station rails, they require to be previously (automatically) detached from the draught rope. In the case of the Pohlig clutch, all that is necessary to free the rope is to turn the

loaded lever, *h*, attached to the screw spindle, from right to left, an operation easily performed (see Fig. 130) by the aid of a suitably bent iron bar, *r*, whilst the recoupling is effected by a guide rail and a fixed striker, *g*.

When the arrival station is on a much lower level than the starting-point, *i.e.*, the loaded skips run downhill, no motor is required, the driving pulley being fitted with a brake instead.

Wire tramways are suitable where materials have to be conveyed over long distances and the contour of the surface is unsuitable for laying a fixed track, or difficulties are encountered in acquiring the land; also when mountain gorges, water-courses, streets or railways have to be crossed, an elevated track is some-

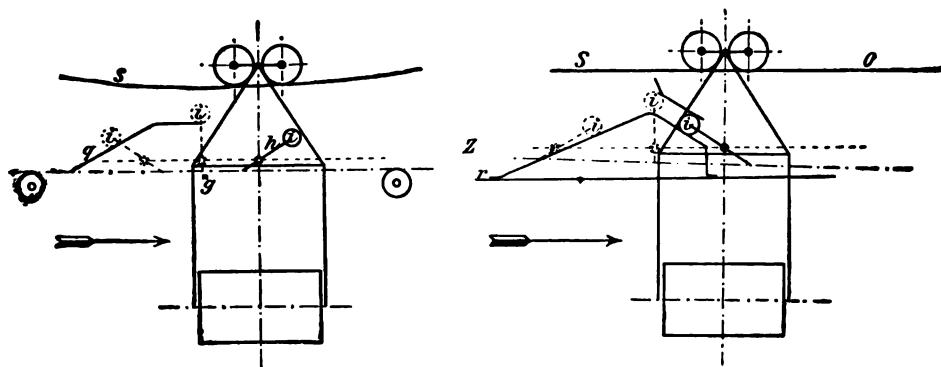


FIG. 130. (Note.—O = top edge of rail; Z = draught rope.)

times desirable owing to the frequency of floods, snowdrifts, etc. About one to three skips can be conveyed per minute, the maximum carrying capacity being some 80 tons an hour. Where the traffic is greater two tracks must be constructed.

Now and again endeavours have been made to directly connect underground haulage with wire-rope tramways, the hanging rails being extended into the haulage road, or by constructing the skips in such a manner that they can be placed on tub frames, and thus transported on the fixed tracks.

## II. LOCOMOTIVE HAULAGE.

Locomotives are used :—

1. In drift work for hauling trains of tubs to the outcrop.
2. To replace horse traction where the erection of rope haulage plant is impracticable owing to the road being too narrow for more than a single track, or containing too many turns, or because the traffic is too small.

The track should be nearly horizontal, otherwise the weight of the engine will have to be excessive, or the train shortened. The engine should be as compact as possible, in order not to unduly impede ventilation.

Care must be exercised in starting and shunting the trains, the component tubs being unprovided with buffers or elastic couplings. Mention has already been made of another disadvantage of train haulage, *viz.*, the accumulation of tubs at the road ends.

*Engine-power.*—Tractive force, 4-60 cwt.

Weight of load, 2-18 tons.

Speed of haulage, 30-120 ins. per second.

*Motive-power.*—Steam, gas, benzine, compressed air, electricity.

Ordinary locomotive engines heated by direct fire are used only in ore mines (return airways) and drifts.

The hot-water locomotive and Honigmann's soda locomotive are only used here and there. The first named has no fire-box but carries a tank filled with water superheated, *e.g.*, by means of high pressure steam blown in. From this tank the supply of steam for the engine is drawn; but of course the steam pressure is a progressively diminishing quantity, as also the water temperature, and hence the engine must be recharged after a short time. The steam is very wet, the consumption high, and the refilling troublesome and time-wasting; but there is no smoke and no risk of ignition.

Honigmann conducts the escape steam of the hot-water locomotive into a tank charged with concentrated caustic soda and immersed in the superheated water tank. The chemical reaction between the steam and the caustic soda generates heat, which retards the cooling of the water in the outer tank.

Gas engines carrying a store of compressed gas are not used in mines, though benzine locomotives have recently been introduced for this work.

According to Mekaski, in compressed air locomotives the wrought-iron air tanks are charged with air under a pressure of 40-60 atmospheres, and this air on its way to the cylinders is passed through superheated water (at 160° C.), whereby it becomes warmed and saturated with water vapour. This enables the air to act with considerable expansion and work in a very favourable manner. The provision of the necessary mains and charging stations in the pit is, however, difficult.

*Electric Haulage.*—All the above-mentioned systems are insignificant in comparison with electric haulage.

The continuous current is generally employed; more rarely polyphase current or accumulators. The current is supplied through a naked line wire fastened to the roof of the haulage road, or through a contact rail, the return current flowing through the track rails or a separate cable. The current is collected by rollers, pulleys or arched slides.

Line wires must be well insulated and placed at such a height as to be out of accidental contact by the workmen.

Brick-lined galleries or rock roads are specially adapted for electric haulage; but in very damp galleries, or where the rock pressure is high, constant supervision and repair are necessary.

## CHAPTER VII.

### THE WORKING OF UNDERGROUND ENGINES.

IT is only in exceptional cases that power generated above-ground is transmitted to the pit by means of shafts, rods or wire ropes, the motive-power for underground haulage engines being mostly supplied by steam, compressed air, hydraulics or electricity.

The three last named are almost always generated by the aid of steam, and the total efficiency in plant with transformed energy is naturally lower than where steam is employed direct. Consequently, where the latter method is practicable, and the peculiar properties of the steam are not injurious to the service of the mine, steam is superior to any of the others for the transmission of power.

#### (a) STEAM.

Boilers are nearly always erected at the surface, the steam being conveyed to the engines by pipes in the shaft. This method is unsuitable for separate driving, but cheap and economical for large engines near the shaft. The carefully insulated pipes must be laid, in such a manner as to be easy of access, in the upcast shaft, and condensation must be provided for. Pipe dimensions must be selected with a view to minimising the cost of steam ; narrow pipes with considerable fall in pressure, but little loss by condensation, are preferable to wide pipes. Where extra power is occasionally required, it is better to provide a double set of pipes, keeping only one in use under normal circumstances. A water separator must be provided between the main and the engine. The escape steam must be condensed, a spray condenser being kept in reserve for use in the event of a breakdown in the air pump ; or else provision must be made for discharging the waste steam into old workings, an upcast ventilating shaft or special upcast pipe. The underground

engine-room must be spacious, well lighted and well ventilated, or the management of the engine will be attended with difficulty and its life and efficiency will be prejudiced.

(b) COMPRESSED AIR.

Unlike steam, compressed air does not conduct troublesome quantities of heat into the shaft and workings, and the waste air instead of being a burden is useful for ventilation. There is no loss by condensation in the pipes ; and if the latter be carefully laid, the waste by diminution of pressure and by leakage is inconsiderable. Any steam engine may be employed as an air motor ; but since air cools considerably in expanding, it is necessary to either work with a small expansion or else warm the air before it enters the cylinders (slight incrustations of ice may be prevented by spraying ordinary pit water into the escape pipe). Heating the air—which is accompanied by a considerable increase in the total efficiency—is best effected by direct fire ; but this is seldom practicable in mines, owing to the smoke evolved and the presence of fire-damp and coal-dust in the pit air. Warming by injected superheated steam or clean hot water entails the provision of special pipes.

The working efficiency of the usual compressed air plant—single-stage compression, no preliminary heating or expansion—is very low, and the system is therefore restricted to places where compressed air is already in use for separate ventilation, driving coal-cutting machines, drills, etc.

(c) HYDRAULIC.

Unlike steam and air, water is inelastic, and permits the attainment of merely a low speed ; hence, wide pipes are required for low pressures, and, for high pressures, the mains are expensive and difficult to keep watertight. Moreover, economical working entails, in large hydraulic engines, pressures of 100 atmos. and more. Low pressure motors may be installed when the water can be derived from the delivery pipe of the pumping plant,<sup>1</sup> or from an

<sup>1</sup> Good pumping engines consume 2½ lb. of best coal in lifting 50,000—60,000—70,000 gallons a height of 3 ft. If 4,000 gallons an hour be drawn from a delivery pipe

existing main supplying, for example, the sprinkling service or sprays for separate ventilation, etc. The efficiency is fairly high. Provision must be made for carrying away the tail water.

Hydraulic power deserves most attention in fiery and dusty pits with firm floors.

Plunger machines are employed for high pressures ; turbines or Pelton wheels (pressure 5-50 atmos.) for small or medium tasks.

A haulage winch working with endless overhead rope and driven by a Pelton wheel is shown in Figs. 131, 132 (Plate VI.). The original was designed by H. Breuer of Höchst-on-Main.

#### (d) ELECTRICITY.

The chief advantage of this form of power resides in the cables, which can be easily laid down anywhere, take up little room, and are not so readily damaged as pipes where the rock is exposed to pressure. Only in fiery pits is the danger of the cable breaking to be feared, and all parts liable to spark—switches and rheostats as well—must be in gas-tight casings. The motors in such cases should be erected in the intake air current, polyphase brushless motors being preferred. The insulation must be carefully seen to, and all wooden linings avoided. Where a cable comes in contact with wood, an underlay of asbestos must be inserted, to prevent ignition. In damp pits iron-shod cables are best ; the motors must be mounted on insulated foundations, and the switch-levers be provided with ebonite handles, etc.

In this system the attendance on the motors is easy, and the efficiency high even in small motors ; and there is no loss of energy when the machinery is at rest.

In choosing motors and kind of current, points to be considered are: whether the starting will be under a full or a small load ; whether the tractive force is constant or greatly fluctuating, the speed constant or variable ; whether, in the event of an accident,

500 ft. high, the effective water-power thus obtained will be about 10 h.-p., whereas the increased consumption of coal by the pumping engine will not exceed about 22 lb., or  $2\frac{1}{2}$  lb. for each 1 h.-p. utilised in the pit. This figure is almost inappreciable in augmenting the working expenses of the pumping plant, since the latter has to bear nearly the whole of the charges for attendance, depreciation, etc.

the load can be suddenly thrown off, or a sudden overload produce complete stoppage,<sup>1</sup> such as may happen through the breaking of

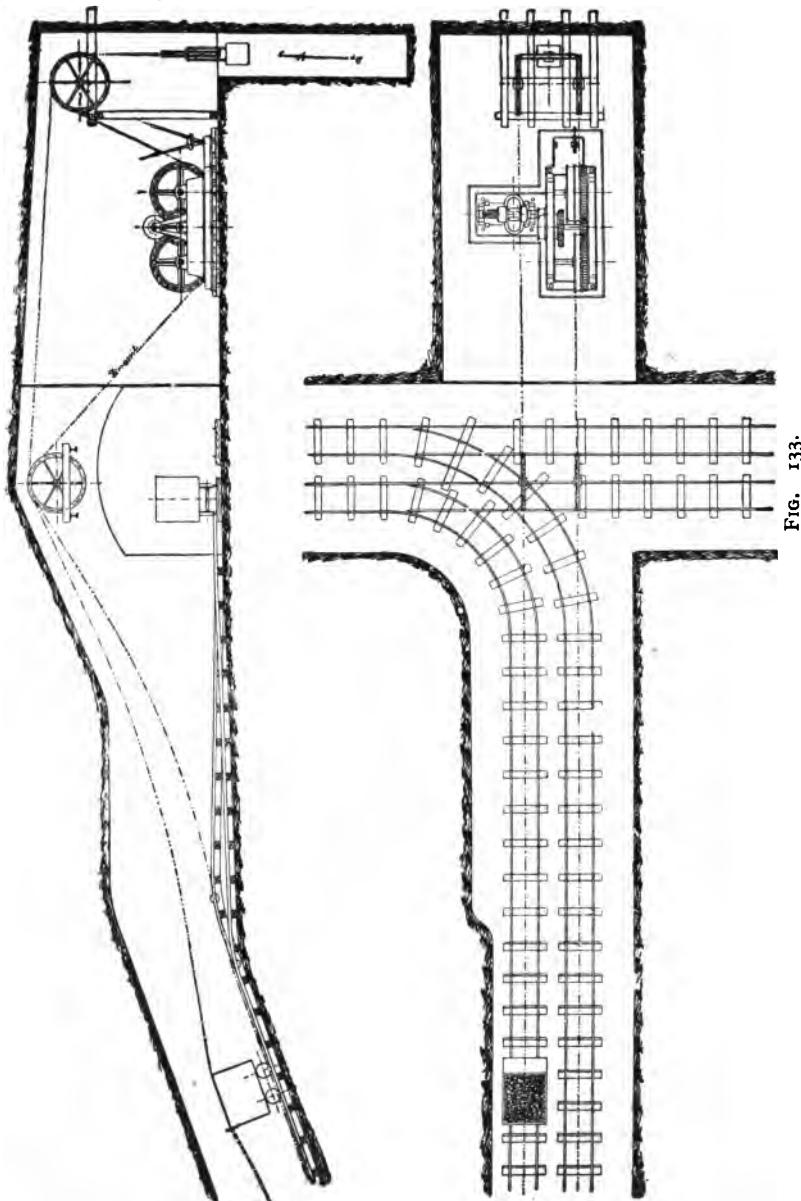


FIG. 133.

<sup>1</sup> Apart from electrical safety appliances, the motor can be protected from overloading by the insertion of a friction clutch or gear between the shafts of the motor and drum. When the strain becomes excessive the coupling slips. The racing of continuous-current motors when running empty can be prevented by means of a centrifugal governor acting on the cut-off switch.

the rope or derailing of a tub in hauling with overhead ropes; whether sparking at the motor and switches can be obviated; and whether the motor is to run continuously or only for short periods, mostly under full load or light loads; and so forth.

Electric winding engines are often fitted with a special emer-

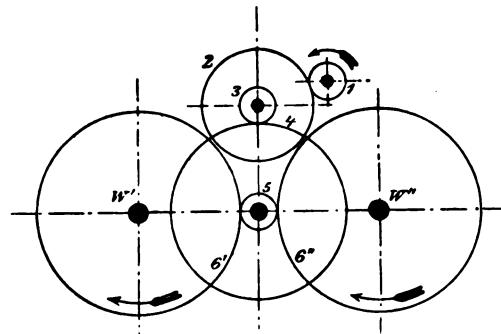


FIG. 134.

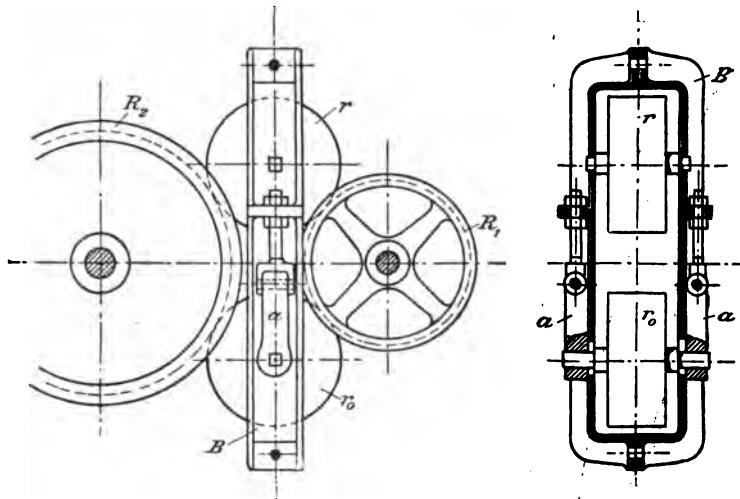


FIG. 135.

gency brake coming into action on the cessation of the current from any cause while the miners are being conveyed to or from the pit. The brake-lever is loaded with a heavy weight, but sustained by a powerful electro-magnet, so that, if the current fails, the lever drops and the brake stops the drum.

Fig. 133 shows the arrangement of an electric haulage road

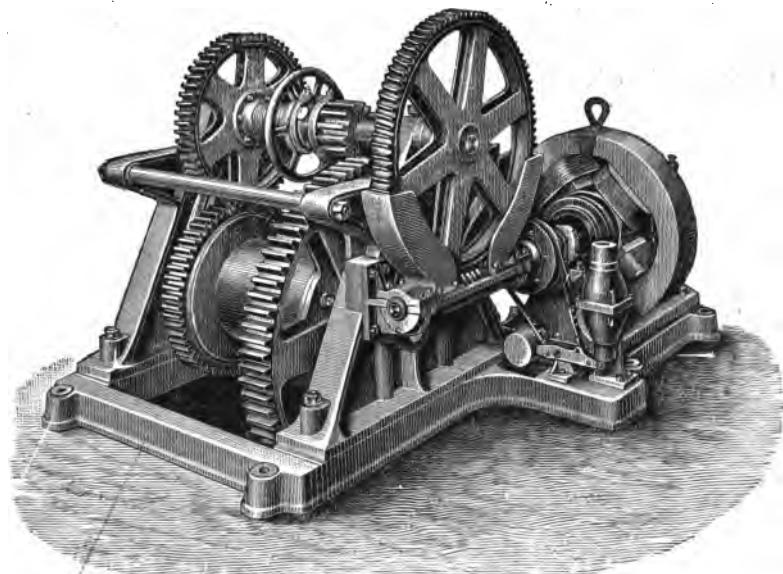


FIG. 136.

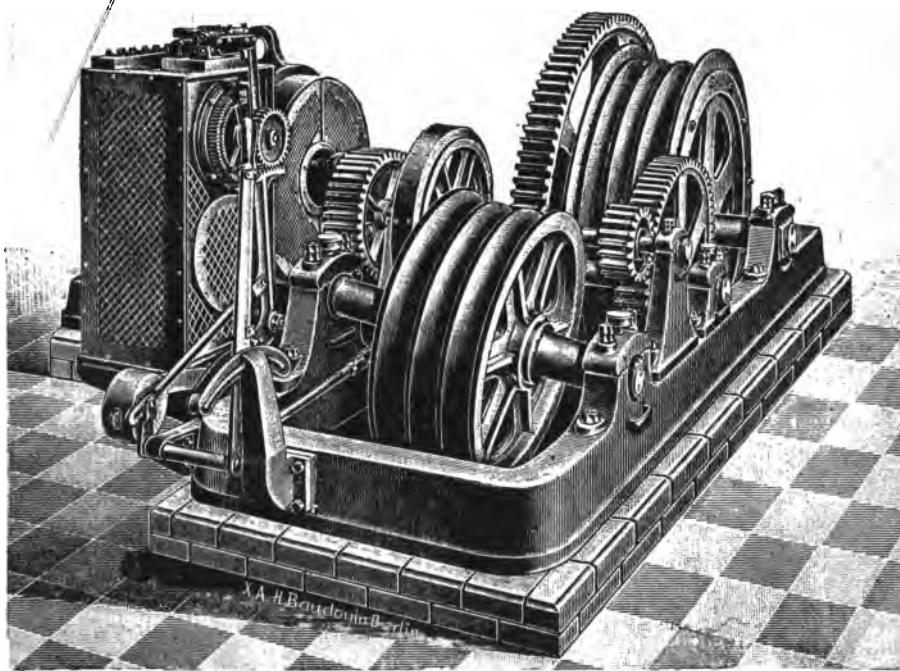


FIG. 137.

according to Hoppe. The method of guiding and tightening the rope needs no further description ; and the mode of driving can be seen from Fig. 134. The motor shaft carries a toothed wheel, 1,

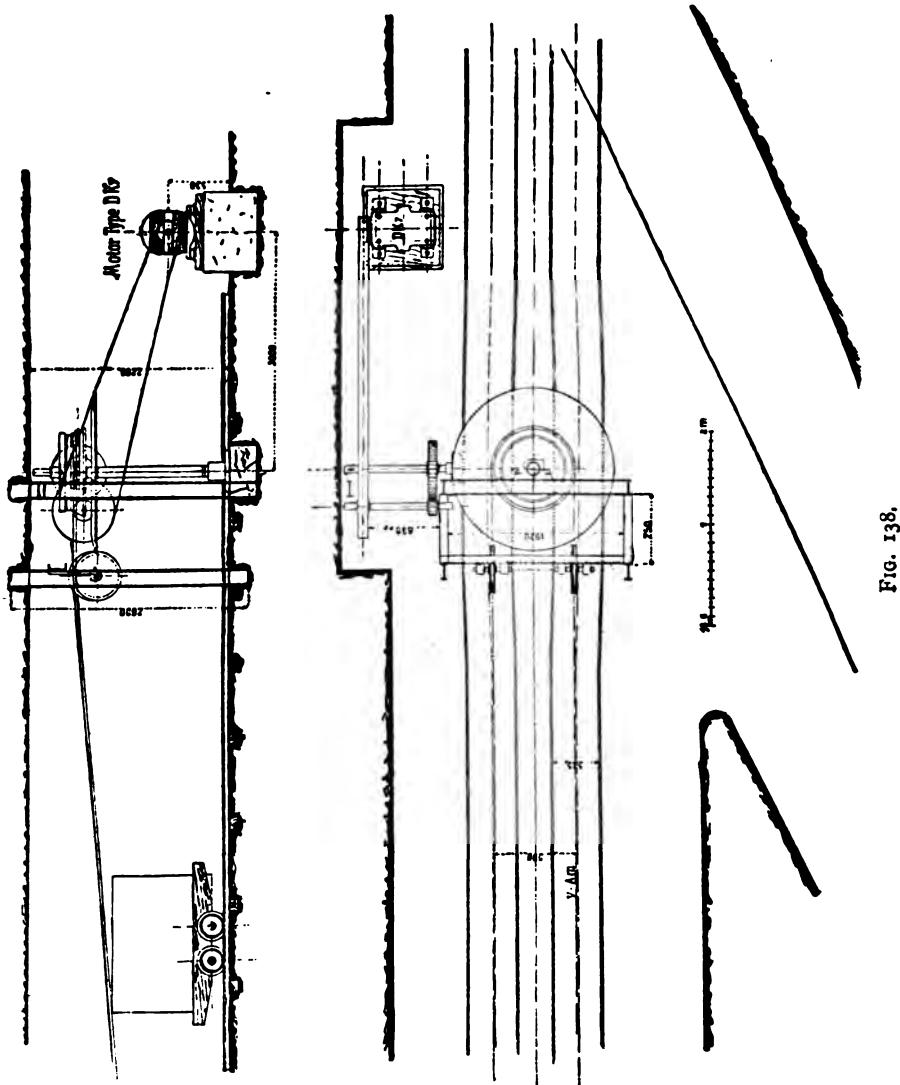


FIG. 138.

and the driving and counter-pulleys are mounted at  $w'$  and  $w''$ . If, as in this case, both pulleys are actuated, then, when three turns of the rope are given, the effective arc embraced is  $= 6\pi$ , but only  $3 = \pi$  when the one pulley is used merely as a guide. Thus the

tractive force can be doubled for the same number of rope turns, but the strain on the rope is unfavourable. In place of the cog gearing,

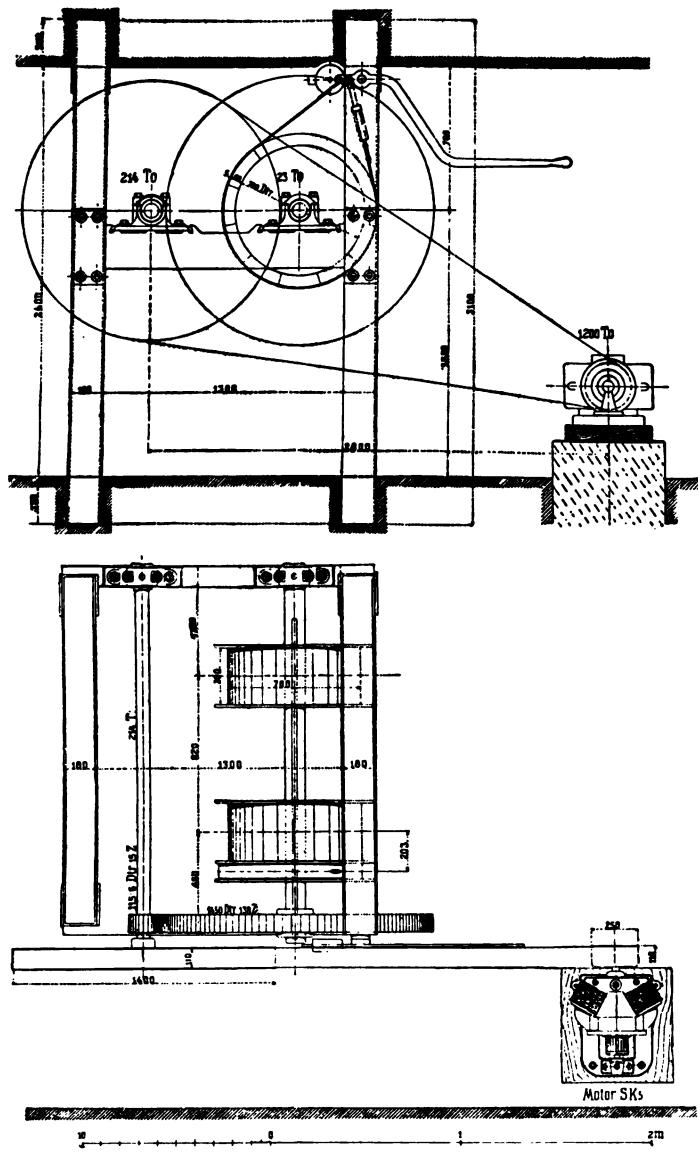


FIG. 139. (Note.—To = revolutions; Z = teeth.)

I-2 (I being usually a raw-hide spur wheel or a phosphor bronze cone wheel), Hoppe often uses friction wheel gear, as in Fig. 135,  $R_1$  being mounted on the motor shaft;  $r$  and  $r_0$ , friction rollers of

leather, raw-hide or millboard, mounted in the bow, B. The axis of  $r_0$  is adjustable in a longitudinal slot. The two rollers can be drawn together, and pressed against the friction wheels,  $R_1$ ,  $R_2$ , by means of set screws and a rubber block,  $\alpha$ .

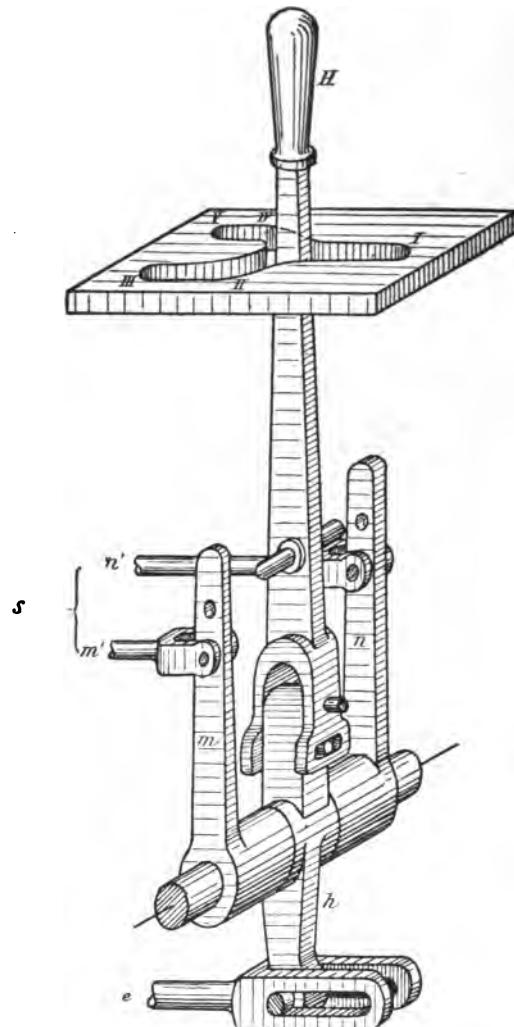


FIG. 136. (Note.—S = to the switch-levers; e = to the brake.)

Fig. 136 shows a worm-gear'd haulage winch made by the Allgemeine Elektrizitäts-Gesellschaft, Berlin, fitted with an electric brake and two-speed gear. The worm-wheel shaft carries two

detachable cog wheels, enabling the drum to be driven at a higher or lower speed.

Figs. 137 and 138 represent electrical systems of chain haulage, the former being by Hoppe, and the latter by Siemens & Halske of Berlin. This firm also makes the winch shown in Fig. 139.

Fig. 140 is the Siemens & Halske reversing gear. The lever, *h*, articulated on the hand-lever, *H*, acts on the brake, and sets it on when *H* is pushed up to I. (the end of the Y-shaped slot). On pulling forward the lever, the brake is gradually released; and by pushing *H* into the branch slots II. III., or IV. V., the levers, *m* or *n*, respectively, are set in motion. These latter are connected with the starting-switch and the rheostat, so that, when *H* is moved from II. to III., or from IV. to V., the circuit is completed for forward or backward running, and the resistances are shut out *seriatum*. The motor cannot be started while the brake is on; and the resistances being gradually shut off before the coils receive the full current, a sudden reversal is impossible. In this way a single lever is sufficient for the brake, starting and reversing gear.

The controlling switches used in electric street cars are also suitable for hoist winches; and the same applies to various other details (spring bearings for the motor, brushes, and so forth).

## CHAPTER VIII.

### MACHINERY FOR DOWNSHILL HAULAGE.

MACHINERY for lowering loads down inclines, etc., is employed for delivering packing waste, lowering coal, etc., from higher workings to the main haulage roads (especially in open cast workings), in unloading, in preparatory plant, etc. Gravity is the motive power, the excess of energy being necessarily taken up by means of brakes.

#### BRAKE INCLINES.

The arrangements are identical with those for haulage through ascending inclines, except that the driving mechanism is replaced by a brake winch, consisting mainly of the driving drum or pulley and a brake. The methods of laying the track, coupling the tubs or trucks, guiding the rope, and constructing the drums, pulleys and brakes, differ but slightly from those already described.

The haulage may be single- or double-acting, the latter being more frequently used in open workings, with open rope, or endless rope or chain; whilst the single method is more in use for underground work, as taking up less room. The tub is attached to one end of the rope, the other carrying a counterpoise, which is drawn up by the descending full tub and afterwards raises the empty. The usual weight for this counterpoise is equal to the empty tub, plus half the net load. In double-acting brake inclines the excess weight generating motion is therefore equal the load, but in single inclines equal only half the load. Hence it follows that the single method is inapplicable for inclines of low gradient (below  $8^{\circ}$ ), whereas the double-acting system may be used on gradients down to  $3^{\circ}$ , in proportion as the trains are lengthened and the tubs easy running.

Overhead rope or chain is recommended for slight gradients

and long roads. The rate of haulage is  $2\frac{1}{2}$ - $5\frac{1}{2}$  yds. In single tracks, the rails for the counterpoise are generally laid inside the main track, and in such case the weight, having to pass under the tubs, must be as flat as possible. It usually consists of a shallow

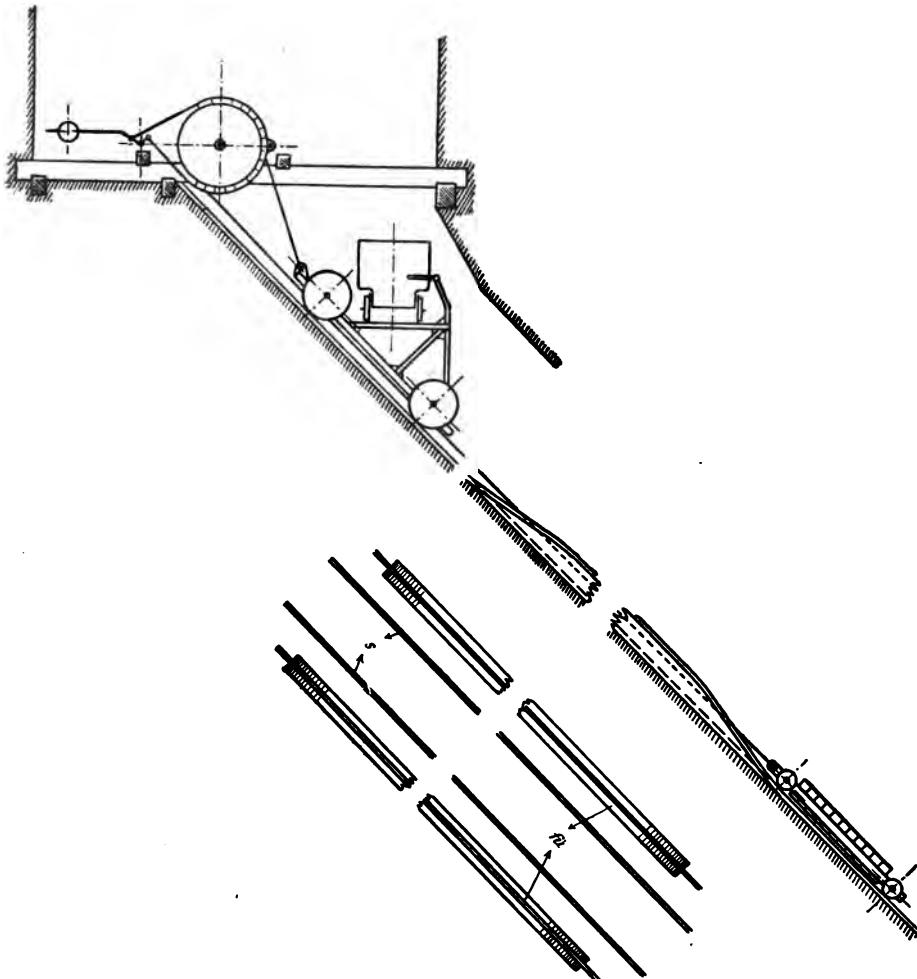


FIG. 141. (Note.—*s* = track for counterpoise; *fū* = main track.)

truck mounted on four wheels, and loaded with stones, fragments of iron, or water, according to requirements. In view of easy conveyance, it is better, however, to form the counterpoise of a number of plates bolted together, and surmounted with rollers, to keep the rope from chafing against the edges of the weight. If the main

track be raised at the meeting-point, as shown in Fig. 141, then the dimensions of the counterpoise need not be so restricted. The elevated rails are carried on longitudinal sleepers cut to the proper shape.

The brake engine consists of the rope drum or pulley, and the brake. Pulley brakes are lighter, easier to mount and dismount, and occupy less room than drum brakes, and are therefore better adapted for pit work. In order to prevent the slipping of the rope in the pulley groove, the conditions already laid down must be fulfilled. The friction is increased by wedge-shaped grooves or by giving several turns to the rope. The pulley shaft is mounted horizontally for single track work, but vertically for double tracks. Rope pulley and brake rim are mostly cast in one piece, or the brake is applied to the outer rim or sides of the pulley, though in this event the heat generated is injurious to the rope. Drum brakes are fitted either with two drums, or with only a single one round which the rope is wound three or four times (Fig. 142). This saves room and rope, but, to ensure the rope coiling evenly on the drum, guides have to be provided, and thus the advantages are counterbalanced. Coiling guides are also required when the first guide pulley is mounted very close to the drum. The rope is gripped by two rollers which are mounted on a small truck or slot receiving motion, like a lathe tool-rest, from a screw spindle actuated from the drum shaft. A simpler plan (Fig. 143) is to provide the hub of the guide pulley with a female thread and mount it on a fixed screw spindle, on which it revolves and travels by the influence of the rope. The pitch of the thread must correspond to the thickness of the rope.

Large brake winches, unless fixtures, are usually mounted on a wooden frame. Fig. 144 shows a means of rapidly fixing up iron pillars (for mounting the drum journals) tight against roof and floor. Large winches should be also fitted with a hand-crank, and where necessary, with detachable gear, for turning the drum shaft, in order to lift the empty tub in case of breakdown, adjust the rope, etc.

Band brakes are generally used, and must be "self-acting," *i.e.*, normally kept pressed against the drum, etc., by weights or springs,

and eased by a foot-lever when haulage is proceeding. Emergency brakes, to enable the load to be arrested instantly, in case of need, are also fitted in the same way, the lever being loaded by a heavy weight but prevented from applying the brake, by a nose or cam, until the latter is withdrawn.

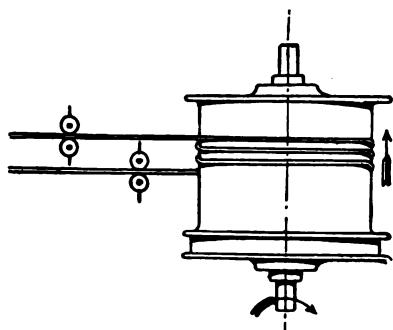


FIG. 142.

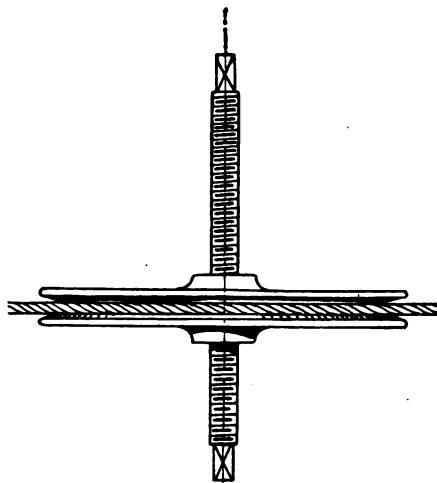


FIG. 143.

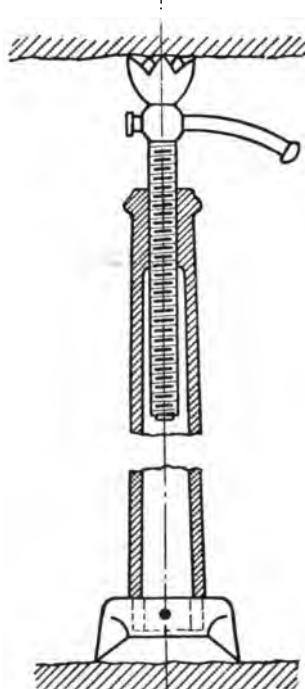


FIG. 144.

In very long brake inclines, especially with continuous endless rope haulage, declivities in wire-rope tramways, etc., the band brake is occasionally supplemented by vane brakes for keeping the velocity within given maximum limits. These brakes consist of large air vanes or smaller water paddles, driven from the shaft of

the drum or pulley. The resistance opposed by air or water to the movement of these vanes takes up the greater part of the excess

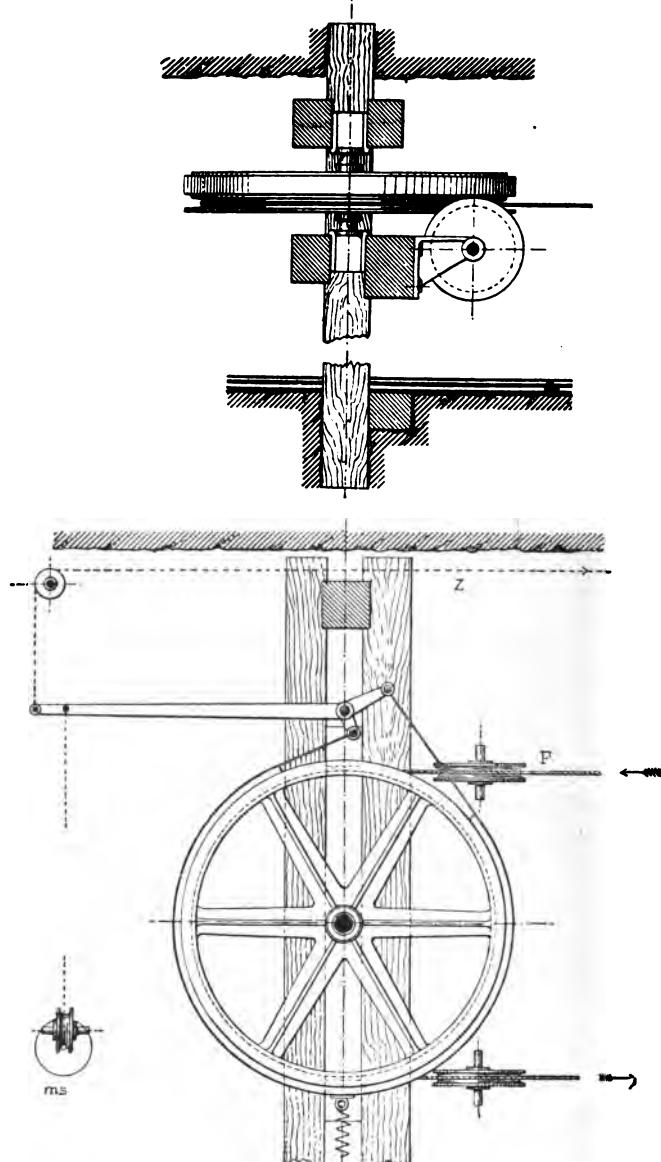
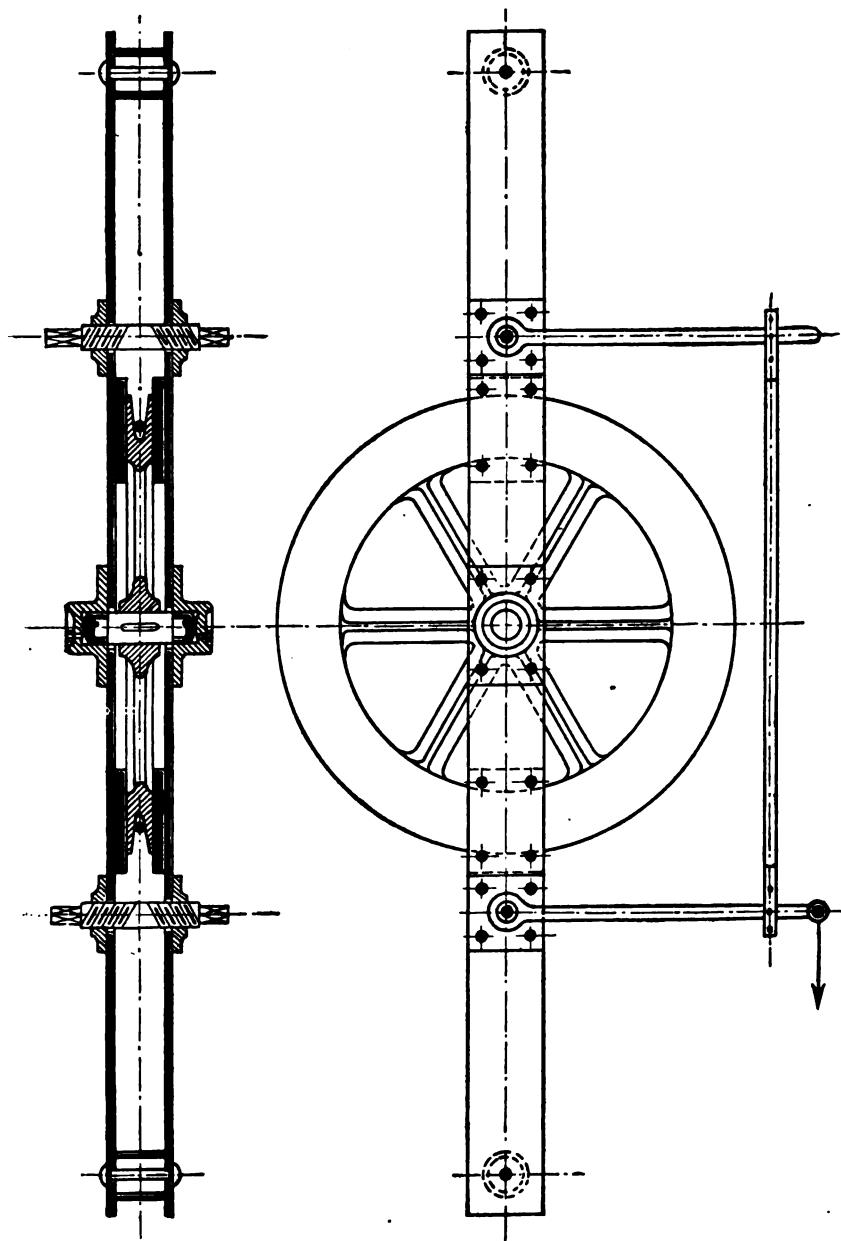


FIG. 145. (Note.—Z = brake cord; F = haulage rope; ms = brake weight.)

of gravitation, thus facilitating the management of the winch and securing uniform velocity.

Fig. 145 represents the station at the head of a brake incline



with endless overhead rope. The dotted brake cord reaches to the bottom of the incline and serves to ease the brake.

The Vanhassel pulley brake is shown in Fig. 146, the frame of two flat iron bars being utilised as a brake, by screwing up the brake blocks against the sides of the pulley with the aid of right- and left-handed screws.

*Hauling from Different Levels.*—Fast-and-loose-drum brakes

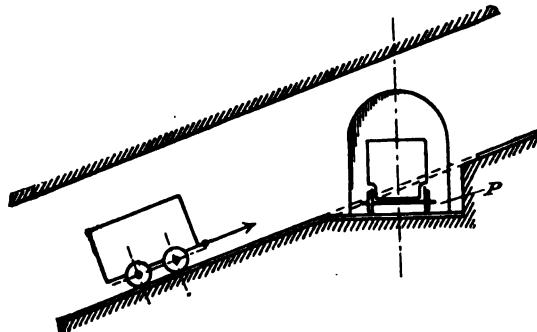


FIG. 147.

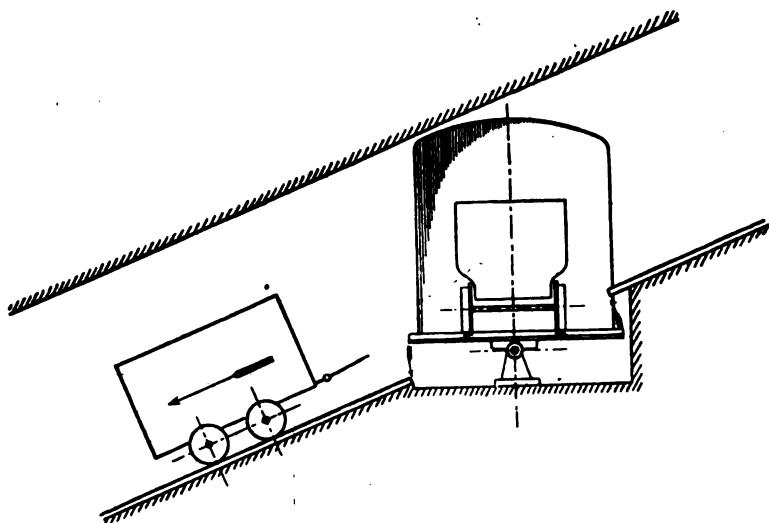


FIG. 148.

are used, the rope being coiled as in winding drums; or where pulley brakes are employed, extra lengths are attached to the rope. A simpler plan than hooking the tub, truck or counter-weight to the rope end is to wind the lower end of the rope round a small drum as reserve, and attach this drum to the tub, etc., in such a manner as to prevent the unwinding of the rope.

Where tubs are delivered to the brake incline from branch roads, the main track must be interrupted (Fig. 147), the tub being turned on the turn-table, P, and hooked on to the rope. In lowering from higher levels, the brake is bridged over by short lengths of rail. Turn-tables of the kind shown in Fig. 148 are also used, the tub

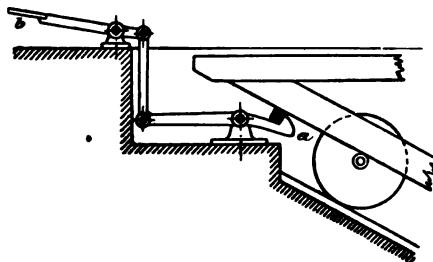


FIG. 149.

from the branch road being run on to the horizontal table, turned and hooked on to the rope, the table being then tilted to the same angle as the main track. The table can be fixed in both positions.

*Taking up Rope Stretch.*—The rope is liable to stretch in use, a source of trouble, especially in double-track haulage, since the

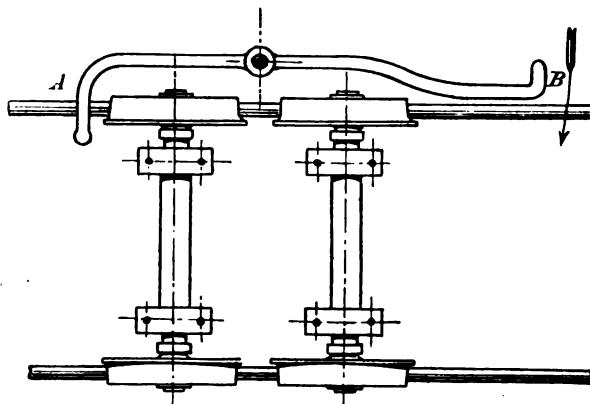


FIG. 150.

truck then does not draw up far enough and the changing of the tubs becomes difficult. The extra length can be taken up by turning the loose drum, shortening the bridle chain, or adjusting a screw between the rope cap and the tub hook.

*Safety Appliances.*—While the tubs are being changed the truck is held fast, the simplest device for this purpose consisting of a hook,

*a* (Fig. 149), which engages with a bar under the ascending truck. When the full tub has been pushed on, the attendant presses down the lever, *b*, and then first eases the brake. If the tubs are hooked direct on to the rope, some means must be provided for pre-

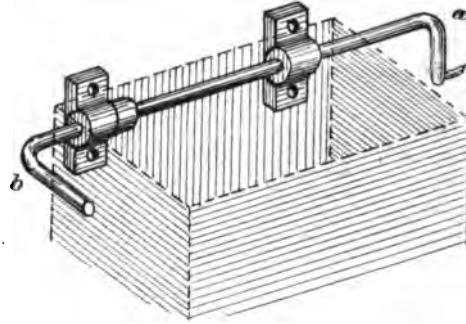


FIG. 151.

venting them running away before they are properly coupled. In Fig. 150 a curved iron bar is pivoted near the rail, a lug, *A*, stopping the tub from running away. On turning the lever in the direction of the arrow the tub is released, *B* at the same time closing the track to

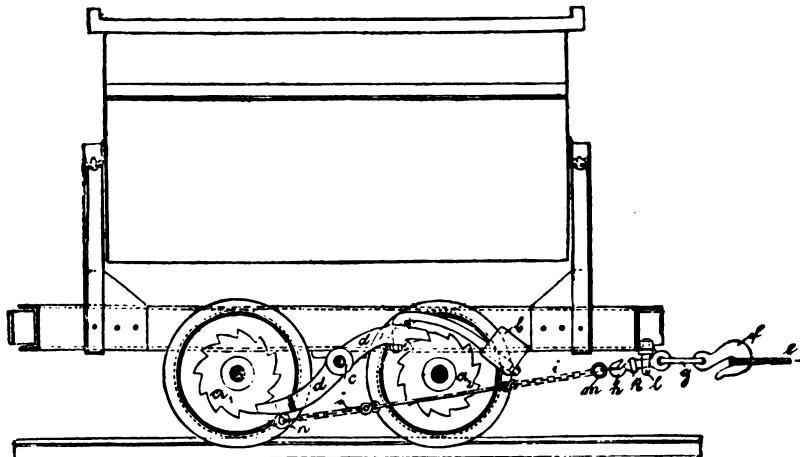


FIG. 152.

any other tubs. The reascending truck pushes *B* aside and returns the stop, *A*, to its original position. Another stop, also used for branches opening on inclines, is shown in Fig. 151. Here a rotatable bar with bent ends, *a* and *b*, is mounted in two staples. The

heavier end, *a*, hangs down, whilst *b* bars the track. The obstacle is removed by turning *a* in the direction of the arrow.

Stops for trucks have already been mentioned (p. 20), and there only remain to be dealt with such appliances as are fitted on the track. These include strong protective walls at the bottom of the incline, for catching the descending truck if the rope breaks, and preventing injury to workmen there. (Particularly necessary when the incline opens into a sloping road.) In long inclines, it is often the practice to set up, at intervals of 40-50 yds., crossbars that lie flat between the rails, but can be raised by pulling a cord,

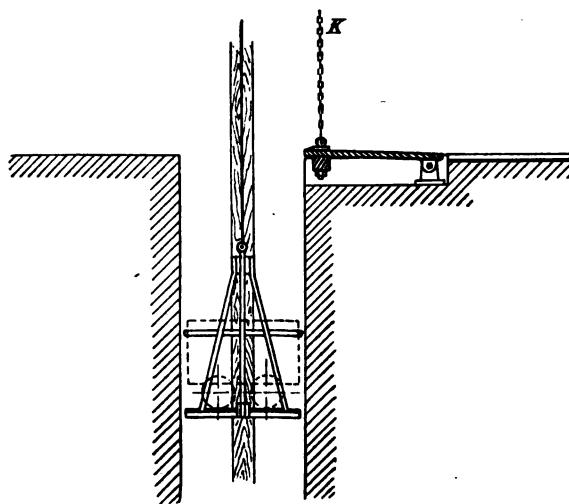


FIG. 153.

and then stop the tubs. The same effect can be produced automatically in endless rope or chain haulage, should an ascending tub break loose and run away downhill, pivoted barriers being provided that are opened by the ascending tubs but bar any progress in the opposite direction.

Safety catches have been devised for acting in the event of a tub running downhill very fast. To this class belongs a lever that is pushed aside by tubs descending at normal speed, but when one runs away the sudden impact on the levers releases stops which bar the track. Finally, mention may be made of the new tub brake designed by Neitsch (Fig. 152) for gradients up to 15 per cent.

Should the rope break, the counterpoise, *b*, releases the double pawl, *d* (which is normally kept raised by the pull of the rope), thus stopping the tub.

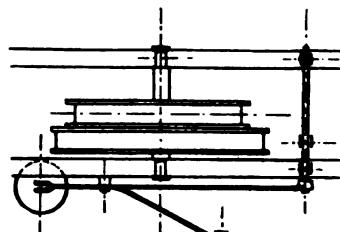
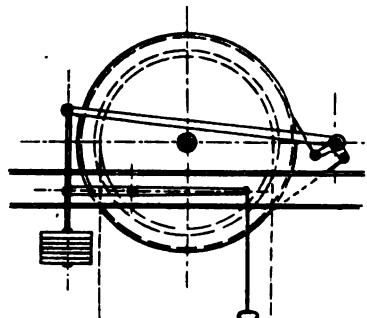


FIG. 154.

#### BRAKE ENGINES FOR WINDING.

These machines, mostly arranged for double action, consist of drums and brakes. In confined spaces driving pulleys are chosen; and for short lifts, above-ground, the rope may be replaced by a chain.

The tubs to be lowered are placed on cages, fitted with guides, and lattice doors to the shaft, as in upward winding. Keps are recommended for safety, though

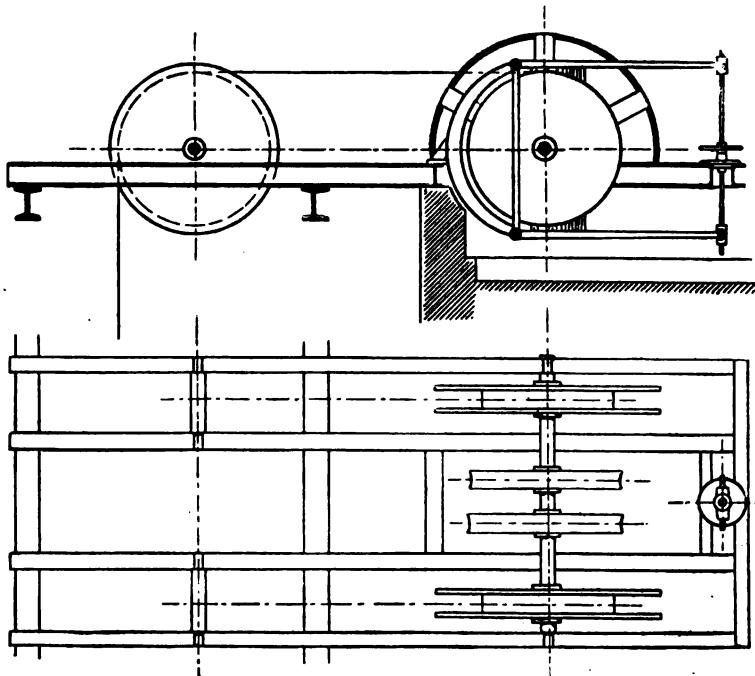


FIG. 155.

not essential ; besides, the rope is strained if the cage is slung while the tubs are being changed. Since, unless a hand crank and detachable gear be provided at the drum shaft, the cage cannot be raised off the keps before lowering, the latter if used at all must be pushed under the cage and withdrawn laterally. Or hooks (Fig. 149) engaging under a bar at the head of the cage may be used. The stretch of the rope is taken up in the manner already described, or by mounting the drum in adjustable bearings. In Fig. 153 the edge of the delivery floor is pivoted, and can be set to the proper height by the chain, K, and a pulley block.

Fig. 154 is a brake for derrick use, and Fig. 155 is a large brake engine fitted with flanged pulleys and powerful brake blocks.

#### UTILISING THE FORCE OF GRAVITY.

In ordinary brake inclines, etc., the excess energy due to gravitation is nullified by brakes ; but under special local conditions this energy can be utilised for raising loads, by connecting the brake engine shaft to a hoist or haulage-road pulley.

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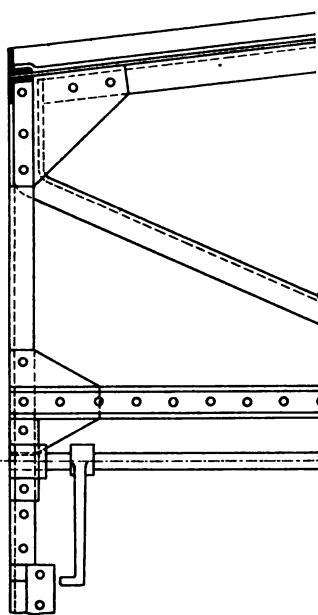
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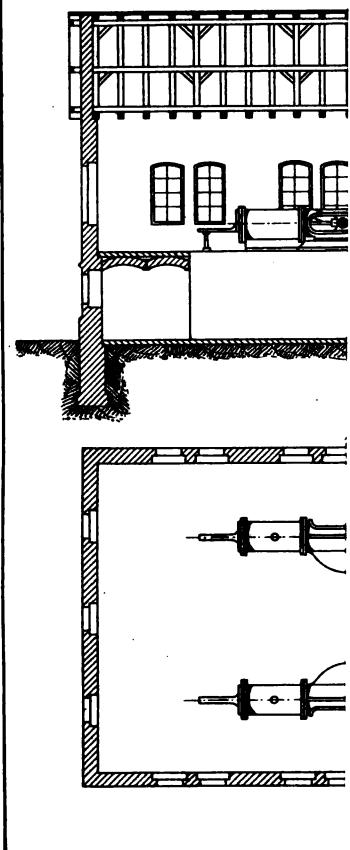
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**Fig. 34.**





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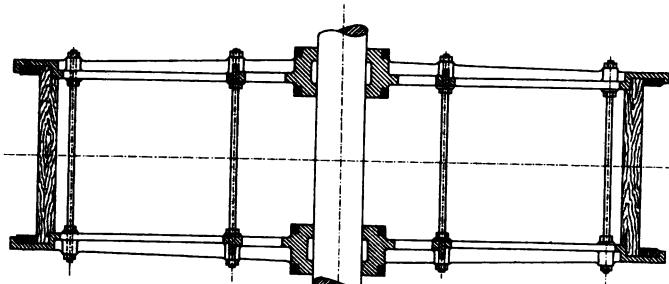


Fig. 59.

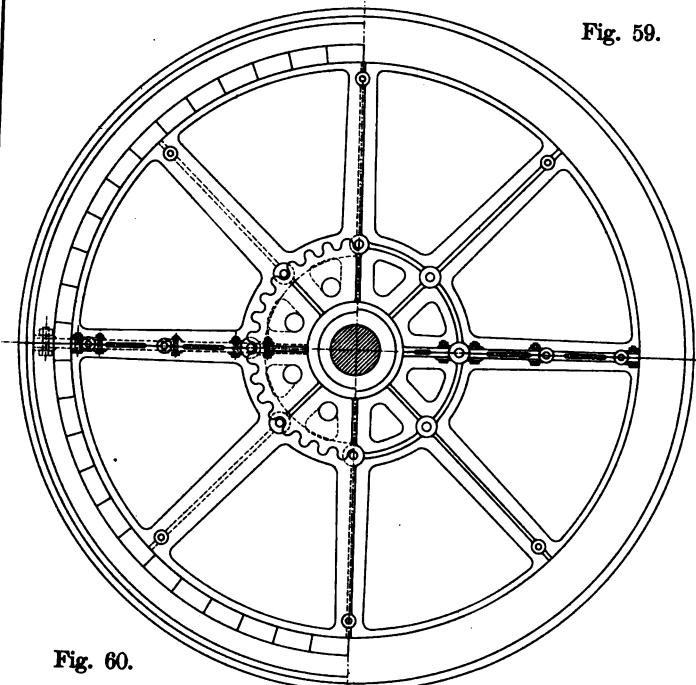


Fig. 60.

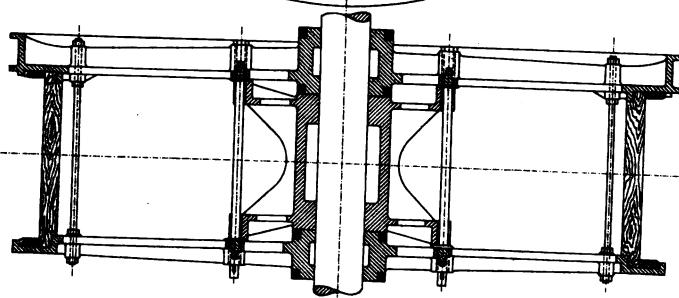
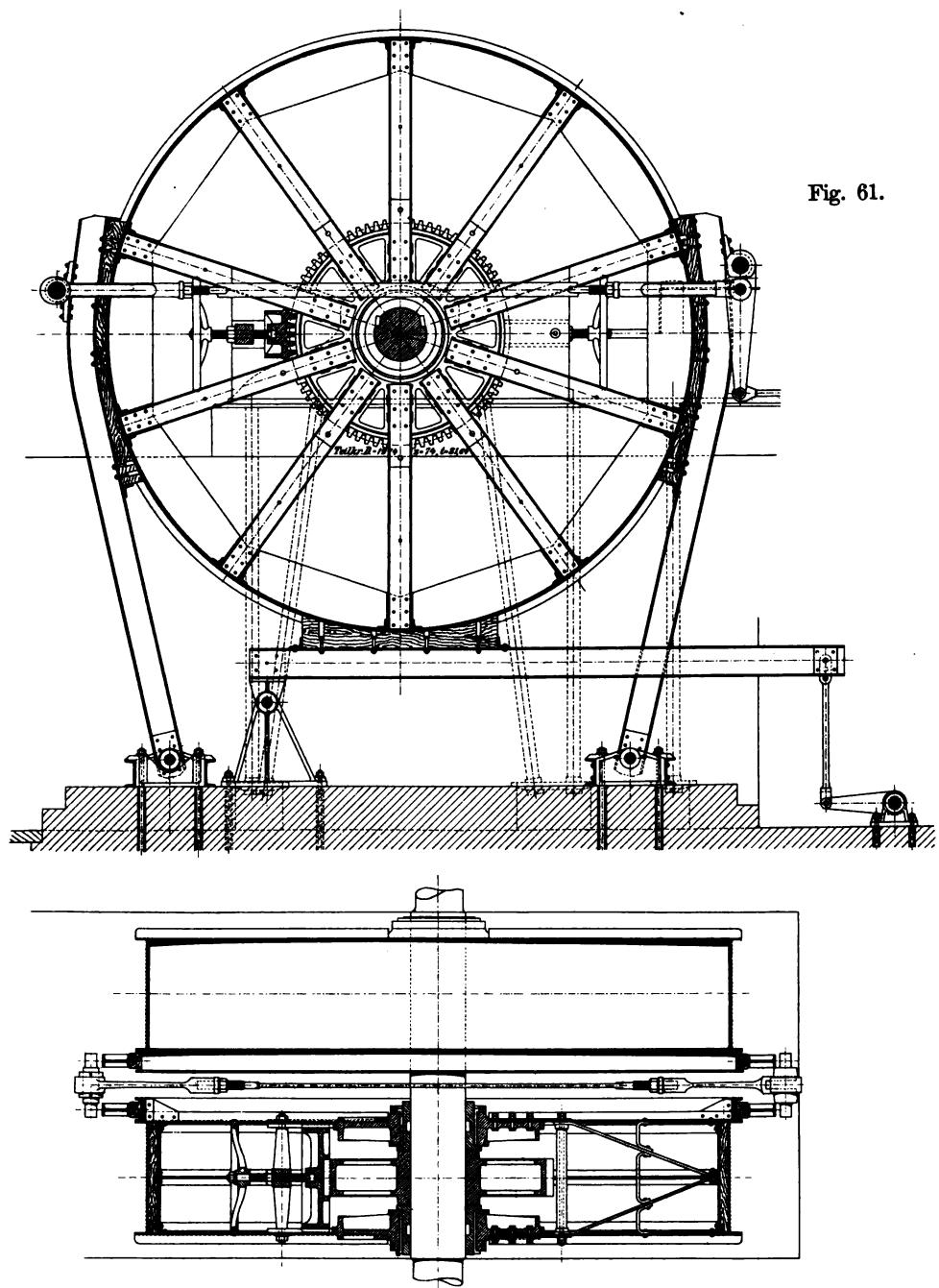
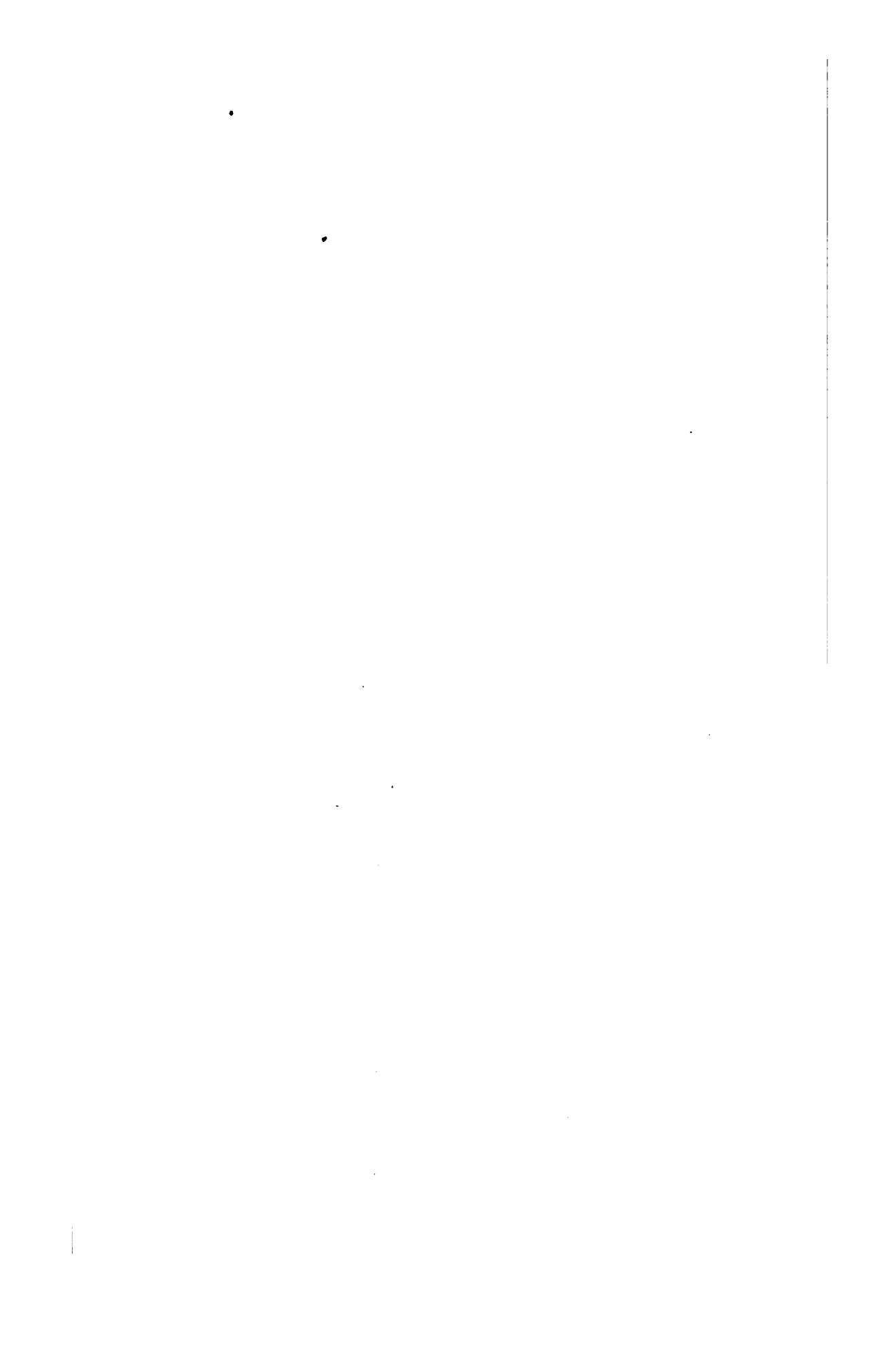


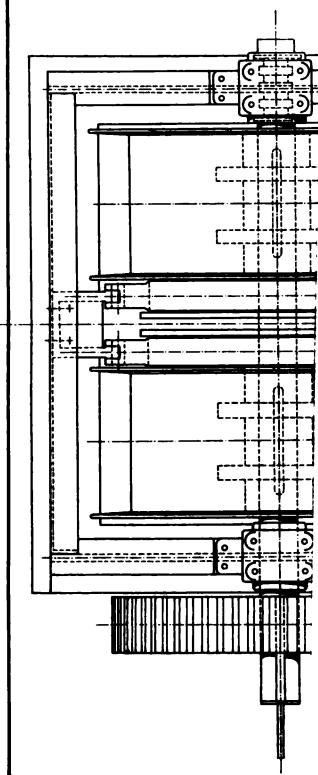
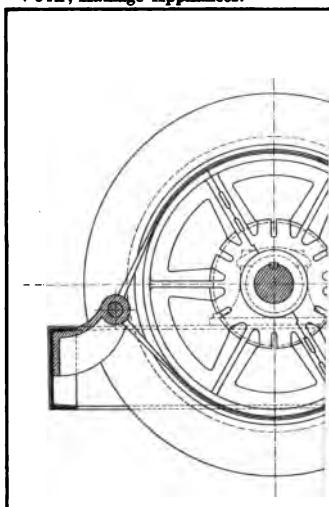


Fig. 61.





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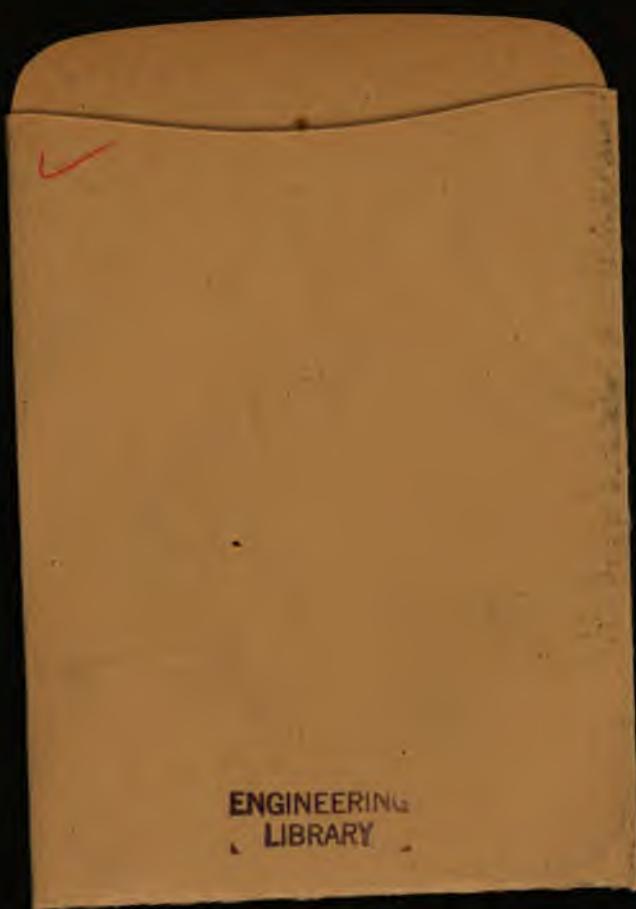
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